

MINERALS & CHEMICAL GROUP

Received

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January 31, 1991

SUPERFUND BRANCH

CERTIFIED MAIL

Bill Adams
U.S. Environmental Protection Agency
M/S HW-113, 11th Floor
1200 Sixth Avenue
Seattle, WA 98101

Re: J.R. Simplot Company

Response to Request for Information

Eastern Michaud Superfund Site

Dear Mr. Adams:

The J.R. Simplot Company, hereinafter referred to as "Simplot", hereby responds to a letter received on November 7, 1990 from the United States Environmental Protection Agency. The letter was directed to John Cochrane of the J.R. Simplot Company, requesting information on the Eastern Michaud Superfund Site located in Pocatello, Idaho. The EPA and Simplot agreed that Simplot's response to this Request for Information was due on or before January 30, 1991.

RESPONSES TO REQUEST FOR INFORMATION

Request No. 1:

A description of the specific size, location and status of the gypsum decant pond and the east overflow pond including dates of installation and lining.

Response:

- A. Gypsum Decant Pond:
 - 1. Size:
 Length at top = 300 feet
 Width at top = 200 feet
 Working depth = 4 feet
 Volume = 2,000,000 gallons



7837 5.2.1 0002 Volume 1 9f2

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- 2. Location: Exhibit #1, which is attached hereto and incorporated herein by reference, depicts the Gypsum Decant Pond.
- 3. Date Operational: 1972.
- 4. Liner:
 - a. Material: "Griffolyn" Type 65 black reinforced plastic.
 - b. Date Installed: 1972.
- 5. Status: Active.
- B. East Overflow Pond:
 - 1. Size:
 Length at top = 272 feet
 Width at top = 132 feet
 Depth = 8 feet
 Volume = 2,150,000 gallons
 - 2. Location: See Exhibit #1 which depicts the East Overflow Pond.
 - 3. Date Pond was Operational: Unknown.
 - 4. Date Pond was Lined: Unlined.
 - 5. Status: Active.

Request No. 2:

The effects of leaching from the two waste gypsum piles and the phosphate ore pile and results of any environmental investigations performed.

Response:

A. PEI Associates prepared a study for the EPA titled, EVALUATION OF WASTE MANAGEMENT FOR PHOSPHATE PROCESSING, which included Simplot gypsum system in the presurvey sampling. PEI Associates placed six monitoring wells around the gypsum stacks and collected samples. Ford Chemical Laboratory, Inc. analyzed split samples collected by PEI Associates. Ford Chemical Laboratory, Inc. results were included as Appendix F of the PEI Associates report.

Simplot has continued to sample four of the PEI constructed wells. These samples have been analyzed by Ford Chemical. (See response to Request No. 8). Two of the six well casings constructed by PEI have been damaged by underground movement and do not allow sample equipment to be lowered into the casings.

- B. Exhibit #2, which is attached hereto and incorporated herein by reference, is a copy of a study conducted by Dames & Moore for Simplot, titled PERMEABILITY OF SOILS AND MINERALOGICAL INVESTIGATION OF "SIMCRETE" FOR J.R. SIMPLOT COMPANY, POCATELLO, IDAHO.
- C. Exhibit #3, which is attached hereto and incorporated herein by reference, is a copy of a report titled HUNDRED FOLD REDUCTION IN PERMEABILITY UNDER A GYPSUM STACK, and was presented at the 1980 Environmental Symposium sponsored by The Fertilizer Institute.
- D. Simplot has attached portions of reports prepared by Dames & Moore which contain information about permeability of gypsum and soil. The titles of the reports are:

Exhibit #4, which is attached hereto and incorporated herein by reference, is a copy of a REPORT OF SOIL STUDIES, GYPSUM TAILINGS POND, POCATELLO, IDAHO, FOR THE J.R. SIMPLOT COMPANY, July, 1962.

Exhibit #5, [Confidential Business Information], which is attached hereto and incorporated herein by reference, is a copy of a report titled RECOMMENDATIONS FOR PRESENT POND CONTROL PROGRAM, TAILINGS POND DEVELOPMENT, SIMPLOT PLANT, POCATELLO, IDAHO, FOR THE J.R. SIMPLOT COMPANY, May, 1963.

Exhibit #6, [Confidential Business Information], which is attached hereto and incorporated herein by reference, is a copy of a REPORT OF PROJECT PLANNING, PROPOSED TAILINGS POND (TP-K 2.1), POCATELLO, IDAHO, FOR THE J.R. SIMPLOT COMPANY, January, 1966.

Exhibit #7, [Confidential Business Information], which is attached hereto and incorporated herein by reference, is a copy of a REPORT OF INVESTIGATION AND DESIGN, PROPOSED EARTHFILL DIKES, TAILINGS POND (TP-K2.1) EXPANSION, NEAR POCATELLO, IDAHO, FOR THE J.R. SIMPLOT COMPANY, Dec. 1974.

Exhibit #8, which is attached hereto and incorporated herein by reference, is a copy of a REPORT OF LABORATORY INVESTIGATION ON EXISTING GYPSUM TAILINGS IMPOUNDMENT FACILITY, POCATELLO, IDAHO, FOR THE J.R. SIMPLOT COMPANY, April, 1987.

Exhibit #9, which is attached hereto and incorporated herein by reference, is a copy of a report titled INVESTIGATION AND STABILITY ANALYSIS OF TAILINGS POND NO.2, J.R. SIMPLOT COMPANY'S POCATELLO, IDAHO OPERATIONS, FOR THE J.R. SIMPLOT COMPANY, Jan. 1988.

Exhibit #10, which is attached hereto and incorporated herein by reference, is a copy of a SUMMARY REPORT, FOLLOW-UP INVESTIGATION AND LABORATORY TESTING, GYPSUM TAILINGS POND NO.2, J.R. SIMPLOT COMPANY'S POCATELLO OPERATIONS, FOR J.R. SIMPLOT COMPANY, March, 1988.

E. Simplot has no studies which have analyzed leaching from the phosphate ore pile. However, Simplot has analyzed water used to transport phosphate ore through a 26-mile pipeline. The phosphate ore and water mixture slurry has analyzed for hazardous waste characteristics according to procedure SW846; the dry phosphate ore has analyzed for hazardous waste characteristics according to the TCLP procedure; the liquid portion of slurry has been analyzed for drinking water parameters. Exhibit #11, which is attached hereto and incorporated herein by reference, contains the analyses for one slurry sample, one dry ore sample and two liquid portions of the slurry.

Exhibit #12, which is attached hereto and incorporated herein by reference, are copies of information generated by the U.S. Geological Survey on water which had been slurried with western phosphate ore.

F. Exhibit #13, which is attached hereto and incorporated herein by reference, is a copy of a report titled, GEOLOGIC INVESTIGATION OF THE DON COMPLEX, SPRING 1976.

Request No. 3:

A complete history of on-site landfill operations including:

- A. Exact location and operation dates of each landfill.
- B. The type, volume, and containers for each hazardous substance disposed in each landfill.

C. Design specifications of each landfill, this is, liners, caps, leachate collection systems, and so forth.

Response:

- A. Active Solid Waste Landfill:
 - 1. Location: See Exhibit #14, which is attached hereto and incorporated herein by reference, which is Simplot drawing 130-6480-105, Tailing Pond #2, Topographic, Current Lift Details, New Proposed Access Road/8% Grade, Revision "A", 12-09-82, Ralph Petrie.
 - 2. Date Operational: Unknown.
 - 3. Type, volume, and containers for each hazardous substance: Simplot has no records to determine whether any hazardous substances were ever disposed of in the Active Solid Waste Landfill. Simplot presently has a policy which prohibits the disposal of hazardous substances in the active solid waste landfill.
 - 4. Design Specifications: The solid waste landfill is constructed partly on virgin earth and the No. 1 phosphogypsum tailings stack.
 - a. Liner: None.
 - b. Cap: Earth.
 - c. Leachate collection system: None.
- B. Original Trash Landfill (Abandoned):
 - 1. Location: See Exhibit #14, which depicts the original Trash Landfill.
 - 2. Date Operational: Unknown.
 - 3. Type, volume, and containers for each hazardous substance: Simplot has no records to determine whether any hazardous substances were ever disposed of in the Original Trash Landfill.

- 4. Design Specifications: The landfill was constructed on virgin earth.
 - a. Liner: None.
 - b. Cap: Earth.
 - c. Leachate collection system: None.

Request No. 4:

A complete history of spills of feedstocks, intermediate and final products and hazardous materials on-site.

Response:

Simplot has no records which provide a complete history of spills of feedstocks, intermediate and final products and hazardous materials on-site. Exhibit #15, which is attached hereto and incorporated herein by reference, are copies of Simplot Spill Release/Report Forms. Two spills not covered by the Simplot Release/Report forms that we have knowledge of are as follows:

- A) Collapse of Tank #26 on Oct. 26, 1974, which also broke the valve off Tank #23, caused a spill of approximately 500 tons (as P2O5) of phosphoric acid. The majority of the phosphoric acid spilled was recovered on site and the NPDES discharge permit limit was not exceeded.
- B) 80 ton spill of sulfuric acid from a railcar occurred on Sept. 28, 1974. This spill was contained in the waste treatment system and the NPDES discharge permit limit was not exceeded.

Request No. 5:

Complete descriptions of hazardous substance handling and disposal practices on-site including operations at the hazardous waste storage area and a description of any hazardous substances disposed in the waste gypsum piles.

Response:

- A. Hazardous Waste Storage Area. Simplot withdrew their permit for a Treatment Storage and Disposal Facility.
- B. Hazardous Substance Handling & Disposal. The description of various plant processes are contained in the pamphlet titled PRODUCT FLOW CHARTS & INFORMATION SHEETS, which is

> attached hereto and incorporated herein by reference as Exhibit #16. Spills of acids are:

- (1) Recovered at the originating plant.
- (2) Recovered at another plant using the material.
- (3) Recovered for sale as dilute liquid fertilizer.
- (4) Neutralized and the solid waste disposed of at the solid waste landfill.
- C. Hazardous Substances to Gypsum Pile. Simplot has no records to determine whether any hazardous substances were ever disposed of in the Gypsum Pile. Simplot presently has a policy which prohibits the disposal of hazardous substances in the gypsum pile.

Request No. 6:

A description of the handling and disposal practices for spent oil and solvents on-site.

Response:

Spent oil is accumulated in a tank and transported by Cowboy Oil to the Ashgrove Cement Plant where it is burned as supplemental fuel. Solvents are collected and returned to Safety-Kleen for reprocessing.

Request No. 7:

A description and a copy of the agreement between FMC and Simplot for the shared use of a drainage ditch from the respective plant properties to the Portneuf River including:

- A. What the ditch was used for.
- B. The length of time it was used by each company.
- C. The types and quantities of wastewater discharged via the ditch.

Response:

A. Exhibit #17, which is attached hereto and incorporated herein by reference, is copy of the original easement agreement, recorded May 11, 1949, instrument number 67527.

Exhibit #18, which is attached hereto and incorporated herein by reference, is copy of the easement recorded August 1, 1973, instrument number 101967.

- B. Exhibit #19, which is attached hereto and incorporated herein by reference, is a letter dated November 7, 1956 which indicated the "reclaimed Westvaco (now FMC) waste water" flow was estimated to be about 3000 g.p.m. The ditch was used by Simplot for process water and any water left over was used to irrigate 36 acres of farm land adjacent to the plant. Plant expansions utilized water previously used to irrigate farm land.
- C. FMC discontinued use of the ditch on October 26, 1973. Simplot discontinued discharge to the Portneuf river via this ditch on April 1, 1974 by routing a small drainage flow into the water treatment system. Portions of the FMC ditch location on Simplot property are utilized for storm runoff control. This stormwater is not discharged to the Portneuf River. A portion of the FMC ditch serves as an emergency overflow between the east overflow pond and the holding pond, and does not discharge to the Portneuf River.
- D. Exhibit #20, which is attached hereto and incorporated herein by reference, is Simplot wastewater data.

Request No. 8:

A summary of analytical results for all soil and ground-water samples taken on-site by Simplot and maps showing all sample locations.

Response:

A. Soil Sample Locations and Results. The location and results of soil samples are included with the reports referenced in Response 2E.

- B. Groundwater Sample Locations. Exhibit #1 depicts the location of wells known as #4, #5, #6 & Frontier. Wells known as #1, #2, & #3 were taken out of service many years ago and were plugged with concrete. Exhibit #21, which is attached hereto and incorporated herein by reference, is a copy of Figure 6-4 from EVALUATION OF WASTE MANAGEMENT FOR PHOSPHATE PROCESSING, by PEI Associates for EPA, and depicts the location of wells known as PEI-1, PEI-2, PEI-3, PEI-4, PEI-5, & PEI-6.
- C. Groundwater Analysis Summary. Simplot has utilized many different laboratories for groundwater analysis. These laboratories include but are not limited to Simplot labs, Betz labs, State of Idaho labs, Ford Chemical and USGS.

The most extensive laboratory work has been done by the Ford Chemical laboratory. Ford Chemical data has been compared on split samples with the EPA contract lab utilized in the study conducted by PEI Associates and with the USGS lab. Ford Chemical data is the most complete data set available. Exhibit #22, which is attached hereto and incorporated herein by reference, is a copy of Simplot's computer data base for the Ford Chemical Laboratory data. The Simplot computer data base does not contain all of the historical Ford Chemical Laboratory data.

Request No. 9:

A discussion of individual and corporate histories and relation- ships between J. R. Simplot, the Simplot-Muir Company, the Ruby Company, Simplot Industries, Inc., the J. R. Simplot Company, the Inland Terminal Warehouse Company, and the Pocatello Corporation including dates of activities, incorporations and acquisitions.

Response:

It is believed that the J. R. Simplot Company corporate history commences February 28, 1946 with the incorporation of J. R. Simplot Processing Company, an Idaho corporation. On March 7, 1946, the name of the Company was changed to J. R. Simplot Company. Early shareholder information with regard to this Company is unavailable. On September 28, 1948, Simplot Investment Company, an Idaho corporation, was formed and it is believed that J. R. Simplot held 34% of the outstanding stock of the Company. On February 24, 1953, the Articles of Incorporation were amended to provide for two classes of stock, Class A and Class B, and upon the cancellation of the old certificates, J. R. Simplot was issued 34% of the Class A stock and 34% of the Class B stock. On March 1, 1952, J. R. Simplot

Company, an Idaho corporation was merged into Simplot Investment Company, and on March 7, 1952, Simplot Investment Company changed its name to J. R. Simplot Company.

On June 28, 1955, J. R. Simplot Company, a Nevada corporation was formed and on March 1, 1956, J. R. Simplot Company, an Idaho corporation was merged into J. R. Simplot Company, a Nevada corporation which remains the present J. R. Simplot Company.

The Simplot Muir Company was incorporated in the State of Utah on March 2, 1946, changed its name to Ruby Company on April 18, 1950. J. R. Simplot was a 25% shareholder of Ruby Company from March 6, 1946 to March 22, 1951, when his 25% interest was conveyed to Simplot Investment Co., the predecessor of J. R. Simplot Company which at the same time obtained another 25.1% interest in Ruby Company from other parties.

Simplot Investment Co., and its successor J. R. Simplot company remained a shareholder of 50.1% of the voting stock of Ruby Co. until January 25, 1956 when a second class of stock was created and its interest was reduced to 49.9% of the Class A voting stock. J. R. Simplot company remained a shareholder of 49.9% of the voting stock of Simplot Industries, Inc. from that date. In 1978, SI, Inc. a Utah corporation was formed as a wholly owned subsidiary of J. R. Simplot Company (Nevada) and on May 1, 1978, Simplot Industries, Inc. was merged into SII, Inc. and its name changed to Simplot Industries, Inc. Simplot Industries, Inc. was then subsequently merged into J. R. Simplot Company (Nevada) on February 28, 1985.

Pocatello Chemical Corporation, a Delaware corporation was formed on the 10th day of December, 1973. All of the issued and outstanding stock of Pocatello Chemical Corporation was owned by Bessemer Securities Corporation from March 9, 1964 until December of 1969 at which time all of said stock was assigned to Simplot Industries, Inc. Pocatello Chemical Corporation remained a wholly owned subsidiary of Simplot Industries, Inc. until December 21, 1977 when it was merged into Simplot Industries, Inc. as the survivor.

J. R. Simplot was a minority shareholder of J. R. Simplot Company from its incorporation until 1990. Mr. Simplot was originally President of J. R. Simplot Company, and at all times has remained a Director of that corporation. On October 1, 1973, J. R. Simplot became Chairman of the Board of J. R. Simplot Company which position he hold as of this date.

Inland Terminal Warehouse Company (Inland), an Idaho corporation was incorporated January 24, 1947, and was solely owned by Gay S. Otter. In 1985, the assets of Inland Terminal Warehouse Company were sold to Simplot Leasing Corporation, a wholly owned

second tier subsidiary of J. R. Simplot Company, and Inland Terminal Warehouse Company was subsequently liquidated. J. R. Simplot was not an officer, director or shareholder of Inland.

The acquisitions at the site by the above corporations are as follows:

All properties at the site which are under the control of J. R. Simplot Company were acquired either directly by J. R. Simplot Company or through Simplot Industries, Inc. (formerly Ruby Company) which was eventually merged into J. R. Simplot Company as the survivor with the exception of two relatively small parcels. A property acquired by Inland Terminal Warehouse company located adjacent to the plant site was used for parking motor vehicles, and a small 10 acre site within the plant site was conveyed to Pocatello Chemical Corporation on which a portion of a chemical plant was constructed, financed and leased to J. R. Simplot Company for operation until the construction was completed and paid for. At which time Simplot Industries, Inc. acquired all of the outstanding stock of Pocatello Chemical Corporation and Pocatello Chemical Corporation was eventually merged into Simplot Industries, Inc.

If you need to discuss any aspects of the Simplot response or need further information from Simplot please feel free to contact Terry T. Uhling, P.O. Box 912, Pocatello, Idaho, 83202, telephone No. (208) 238-2801. Thank you for your cooperation and assistance in this matter.

Sincerely yours,

TERRY T. UHLANG

Assistant General Counsel

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c: Ron Graves

CERTIFICATE OF MAILING

I HEREBY CERTIFY that a true, correct and complete copy of the foregoing document was mailed on this 31st day of January, 1991, postage prepaid, to the following:

Dean Nygard
IDAHO DEPT. OF HEALTH & WELFARE
Dept. of Environmental Quality
1410 N. Hilton
Boise, ID 83720

TERRY T. UHLENG

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- Exhibit #1 Map which depicts the Gypsum Decant Pond.
- Exhibit #2 Copy of a study conducted by Dames & Moore for Simplot, titled PERMEABILITY OF SOILS AND MINERALOGICAL INVESTIGATION OF "SIMCRETE" FOR J.R. SIMPLOT COMPANY, POCATELLO, IDAHO.
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PERMEABILITY OF SOILS AND MINERALOGICAL INVESTIGATION OF "SIMCRETE" FOR J. R. SIMPLOT COMPANY, POCATELLO, IDAHO

Dames & Moore Job No. 4048-024-06

PERMEABILITY OF SOILS AND MINERALOGICAL INVESTIGATION OF "SIMCRETE"

INTRODUCTION

Observations made during preparation of the Environmental Analysis Record indicated that when gypsum slurry from the J. R. Simplot Company phosphate fertilizer plant interacted with the native silt loess soil underlying the gypsum storage area, a chemical reaction occurred which greatly reduced permeability of the soil. In addition, at the soil-gypsum interface, an indurated material, informally designated "Simcrete," was formed. This report presents the results of investigations designed to provide further insight into these reactions and their significance in relation to inhibiting potential seepage from the gypsum storage area.

The investigations reported here are the results of the modified scope of work outlined in our proposal of September 18, 1975, "Analysis and Identification Study of 'Simcrete' Substance." The scope of work authorized by Mr. Jack Smith, J. R. Simplot Company, during telephone conversations with Dr. Peter Olsen of Dames & Moore during November, 1975, consisted of conducting a series of five laboratory permeability tests utilizing native silt loess soils and water from the gypsum tailings slurry as well as optical examination of thin sections of the Simcrete substance to determine the nature of the cementing material.

MINERALOGICAL INVESTIGATION OF SIMCRETE

Samples of the indurated material collected by personnel of the J. R. Simplot Company in November, 1975, were submitted to Professor William T. Parry, Department of Geology and Geophysics, University of Utah for examination. Two types of samples were examined. One consisted of older material taken from a stratum approximately one foot in thickness located about 50 feet below the surface of the abandoned gypsum storage area. The other sample was younger material taken at the gypsum-soil interface near the leading edge of the active gypsum storage area; at this site the gypsum covered the soil surface to a depth of only 2 to 5 feet and had been in place for about 6 months.

Optical examination of petrographic thin-sections made of the samples revealed the presence of two distinct types of secondary material which decrease porosity and permeability and increase cohesive strength. The first, noted in the older Simcrete, is isotropic and has a refractive index below 1.54. The second, observed in the younger material, is anisotropic, is composed of radiating crystals with refractive indices below 1.54 and has low birefringence, and parallel extinction under polarized light. Neither of these materials could be identified as to chemical species within the scope of work authorized.

The complete report of Professor Parry's optical investigation, including photomicrographs, is included in the appendix.

Samples of the older Simcrete as well as a sample of the native silt loess soil had previously been supplied to Dr. Parry for comparative

X-ray diffraction and X-ray emission studies. These studies were not conclusive other than to note that while quartz, calcite and dolomite were present in the native soil, calcite and dolomite were absent in the Simcrete, and that the latter contained an additional component which could not be identified. In addition, it was determined that the Simcrete contained more sulphur, phosphorous and calcium and less aluminum than the silt loess soil. Dr. Parry's complete letter report is contained in the appendix.

Air permeability tests were performed by Core Laboratories,

Dallas, Texas, on four cores of older Simcrete. Porosities of the various
samples were found to be 16.0, 29.7, 36.0, and 36.3 percent. Respective
vertical permeabilities in millidarcys were 1.7, 2.7, 104 and 25, corresponding to vertical permeabilities to water of 1.5, 2.4, 93 and 22 feet/year.

PERMEABILITY

METHODS:

Soil samples were taken using thin wall samplers from the top six inches of soil at five locations during November, 1975 by J. R. Simplot Company personnel. Locations of the samples are shown on Plate 1. All sample sites were at locations which will eventually be covered by gypsum.

Permeability tests were performed in the Salt Lake City Dames & Moore laboratory as described in Plate 2, "Method of Performing Percolation tests," under a confining pressure of 100 pounds per square foot. All samples were disturbed during sampling and had to be recompacted. A two-inch long core from each sample was selected for the actual permeability tests.

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Two of the soil samples ("A" and "B") were subjected to permeability testing utilizing tap water for six days followed by 14 days of testing utilizing water from the gypsum slurry.

Three of the soil samples ("C," "D" and "E") were tested for 15 days utilizing only water from the gypsum slurry.

Data on the results of permeability testing of another sample ("F") are also included. This testing was performed in August 1975 and provided the basis for the observation that the gypsum slurry water reacted chemically with the native silt loess soil resulting in greatly reduced permeability. Sample "F" was taken at a depth of six feet from a boring ("D3") completed November 2, 1974 in conjunction with a job previously performed for the J. R. Simplot Company (Dames & Moore Job 4048-020-06, dated December 22, 1974). Permeability of the sample was tested for 13 days utilizing gypsum slurry water only.

In addition to the permeability tests, the pH of the gypsum slurry water was determined before application to the soil samples. A sample of the same water collected after percolation through Samples "C," "D" and "E" was also analyzed for pH. Mechanical and hydrometer analysis of Sample "A" for textural classification was also made.

RESULTS:

The results of the permeability tests are shown in Tables 1 through 6.

Samples "A" and "B" yielded permeability values with tap water of about 65 and 140 ft/year, respectively. Within approximately 5 hours of

tions on the same

changing to gypsum slurry water, permeability had decreased to about 20 and 9 feet/year, respectively. In less than one week, permeability rates of both samples were less than one foot/year. At the end of the 14 day test period both samples showed permeability rates of about 0.85 feet/year.

The initial permeability rates of the other three soil samples ("C," "D" and "E") tested only with gypsum slurry water averaged about 45, 85 and 250 feet/year, respectively. (Sample "C" was severely disturbed by sampling; this may be responsible for the low initial permeability value). Within 24 hours, these samples showed permeability rates of about 3, 10 and 4 feet/year. By the end of the 15 day test period, permeability rates of the 3 samples ranged from 1.2 to 1.5 feet/year.

Initial permeability rates of the subsurface sample ("F") averaged about 215 feet/year. This decreased to about 9 feet/year within 24 hours and by the end of the 13 day test period, permeability was less than 0.5 feet/year.

The initial pH of the gypsum slurry water used in these tests was 1.7. Following percolation through soil samples "C," "D" and "E" a composite sample showed a pH of 3.6.

Mechanical analysis of sample "A" for particle size revealed 85.2% passing a No. 200 U. S. Standard Sieve (0.075 mm). Hydrometer analysis showed the following particle size distribution for the total sample:

Sand (>0.05 mm), 39.5 percent; Silt (0.05-0.002 mm), 49.2 percent;

Clay (<0.002 mm), 11.3 percent.

DISCUSSION

These investigations have verified that the gypsum slurry reacts chemically with the native silt loess soils underlying the operating gypsum

storage area to significantly reduce permeability. The original permeabilities of these soils were about 50 to 250 feet per year. These were reduced through reaction with the percolation of the slurry water to about one foot, per year or less. This represents a reduction in permeability of 97 to 99 percent.

Permeabilities of this order are generally quite acceptable for clay or bentonite liners constructed for industrial waste ponds and for sewage lagoons. The Utah Code of Waste Disposal Regulations allow a maximum seepage through the bottoms of sewage lagoons of 0.25 inches per day or 7.6 feet per year. The Idaho Department of Environmental and Community Services (personal communication, January 5, 1976) has used this same figure for a number of years but now considers additional factors in determining allowable seepage in a given case.

Formation of the Simcrete substance did not occur under the laboratory conditions of testing during the short term of the tests. However, the samples, when examined following the tests, showed positive indications that such induration was commencing with definite cementation having taken place, particularly in the upper portion of the samples.

The cementing material which is formed and which contributed to the decreased permeability could not be chemically identified although two definite types were differentiated by optical examination. The chemical reaction producing Simcrete is unknown but involves a change from a calcareous to non-calcareous state with replacement of calcite and dolomite. The cementing substances are probably compounds of calcium, phosphate and/or sulfate possibly containing iron and magnesium.

Whatever the chemical nature of the soil-gypsum slurry reaction may be, the practical significance is that, in essence, a liner of very low permeability is created under the storage area in a short period of time, wherever this reaction occurs. This reaction, with its reduced permeability, may be expected to occur wherever similar reactive soil underlies the gypsum storage area.

Respectfully submitted,

DAMES & MOORE

Richard Chojnacki

Associate

Peter F. Olsen Project Manager

RC/PFO:ab

TABLE 1 PERMEABILITY RATES - SOIL SAMPLE "A"

Wet Density

Moisture Content

Before Test

98.1 lbs/cu ft

Before Test

13.2%

After Test

111.1 lbs/cu ft

After Test

28.1%

Dry Density

After Test

86.7 lbs/cu ft

| Water Source | Elap Days | sed Time Minutes | Observation Time (Minutes) | Number of Observations | Permeability Range | Mean |
|-----------------|--------------|---------------------|----------------------------|---------------------------|--------------------|--------------------------|
| Tap Water | . 0 | | 118 | 3 | 76.7-85.5 | 79.9 25 10 rd |
| ^ H | 2 | | 45 | 9 | 54.4-89.4 | 70.0 |
| 11 | 5 | | 25 | 5 | 62.2-77.8 | 68.4 |
| tt | 6 | | 49 | 11 | 58.3-68.0 | 62.3 |
| Gypsum | | | | | | |
| Slurry | | 15 | | 1 | | 58.3 |
| " | | 53 | | 1 | | 55.2 |
| 11 | | 70 | | 1 | | 52.6 |
| 11 | | 82 | | 1 | | 43.7 |
| 11 | | 113 | | 1 | | 33.8 |
| 11 | | 125 | | 1 | | 43.7 |
| 11 | | 235 | | ī | | 28.1 |
| II. | | 315 | | 1 | | 19.7 |
| 11 | 1 | • | 538 | 12 | 4.6-13.9 | 7.2 |
| 11 | 2 | | 476 | 4 | 5.2-11.7 | 6.6 |
| 11 | 3 | | 1489 | 5 | 3.4- 4.2 | 4.0 |
| 11 | 4 | • | 349 | 3 | 0.49- 3.1 | 1.7 |
| 11 | 7 | | 541 | 3 | 0.07- 0.27 | 0.13 |
| u . | 8 | | 1431 | 3 | 1.1- 1.3 | 1.3 |
| *** | 9 | | 1241 | 2 | 1.2- 1.3 | 1.2 |
| 11 | 10 | | 1626 | 2 | 0.89- 0.95 | 0.93 |
| *** | 11 | | 1265 | 2 | 0.55- 0.97 | 0.86 |
| 11 | 14 | | 42 35 | 2 | 0.82- 0.85 | 0.85 |

TABLE 2 PERMEABILITY RATES - SOIL SAMPLE "B"

Wet Density

Moisture Content

Before Test 98.1 lbs/cu ft

Before Test 11.6%

After Test

114.1 lbs/cu ft

After Test 28.7%

Dry Density

After Test 88.6 lbs/cu ft

| | | | Observation | | | 4 |
|-----------|-------------|-----------------|-------------|---------------------|------------------------|-------------|
| Water | Elaps | <u>sed Time</u> | Time | Number of | <u>Permeability In</u> | |
| Source | <u>Days</u> | <u>Minutes</u> | (Minutes) | <u>Observations</u> | Range | <u>Mean</u> |
| Tap Water | 0 | | 81 | 3 | 289.7-408.7 | 352.5 |
| 11 | 2 | | 45 | 9 | 116.6-182.7 | 144.7 |
| 11 | 3 | | 25 | 5 | 116.6-186.6 | 147.0 |
| 11 | 6 | | 49 | 11 | 132.2-145.8 | 137.6 |
| Gypsum | | | | | | |
| Slurry | | 15 | | 1 | | 114.0 |
| 11 | | 53 | | 1 | | 115.1 |
| 11 | | 90 | | 1 | | 33.6 |
| 11 | | 102 | | 1 | | 50.2 |
| 11 | | 133 | | 1 | • | 29.4 |
| 11 | | 145 | | . 1 | | 22.7 |
| 11 | | 250 | | 1 | | 10.0 |
| 11 | | 333 | | 1 | | 9.1 |
| 11 | 1 | 222 | 477 | 12 | 1.2- 11.0 | 4.7 |
| 11 | 2 | | 477 476 | 5 | 2.1- 7.0 | 3.7 |
| ŧf | 3 | • | 1489 | 5 | 1.9- 2.6 | 2.5 |
| 11 | 4 | | 1273 | 4 | 0.46- 2.1 | 2.0 |
| 11 | 7 | | 4323 | 4 | 0.02- 1.3 | 1.4 |
| ti | | | | 3 | 0.50- 1.2 | 1.1 |
| 11 | 8 | | 1429 | 2 | | |
| - 11 | 9 | | 1241 | | 0.50- 1.0 | 0.63 |
| | 10 | | 1626 | 2 | 0.77- 0.87 | 0.80 |
| 11 | 11 | | 1470 | 2 | 0.25- 1.0 | 0.75 |
| 11 | 14 | | 4235 | 2 | 0.69- 0.95 | 0.84 |

TABLE 3 PERMEABILITY RATES - SOIL SAMPLE "C"

Wet Density

Moisture Content

Before Test 97.6 lbs/cu ft

Before Test 11.3%

After Test 113.3 lbs/cu ft

After Test 29.2%

Dry Density

After Test 87.7 lbs/cu ft

| Water | Elapsed Time | Observation Time | Number of | Permeability | In Ft/Yr |
|--------|--------------|---------------------|---------------------|--------------|-------------------|
| Source | (Days) | (Minutes) | <u>Observations</u> | Range | Mean |
| Gypsum | | | | | |
| Slurry | 0 | 442 | 33 | 0-51.8 | 7.8 |
| 11 | 1 | 1675 | 5 | 1.3- 7.0 | 2.6 |
| 11 | 4 | 660 | 3 | 2.9- 5.2 | 3.4 |
| 11 | 5 | 1380 | 1 | 2.1 | 2.1 |
| 11 | 6 | 1456 | 2 | 1.3- 1.7 | 1.6 |
| 11 | 7 | 300 | 1 | 2.9 | 2.9 |
| 11 | 11 | 4843 | . 4 | 1.2- 2.2 | 2.2 |
| 11 | 12 | 1410 | 3 | 1.2- 1.6 | 1.3 |
| 11 | 13 | 1073 | 1 . | 1.3 | 1.3 |
| ** | 15 | 3101 | 2 | 1 2- 2.4 | 1 3 ⁽⁴ |

TABLE 4 PERMEABILITY RATES - SOIL SAMPLE "D"

Wet Density

Moisture Content

Before Test 98.5 lbs/cu ft Before Test 13.2%

After Test 109.5 lbs/cu ft After Test 25.4%

Dry Density

After Test 87.0 lbs/cu ft

| Water Source | Elapsed Time(Days) | Observation Time (Minutes) | Number of Observations | Permeability i | n Ft/Yr Mean |
|-----------------|--------------------|----------------------------------|---------------------------|---------------------|-----------------|
| | J | | | | |
| Gypsum | | | | | |
| Slurry | 0 | 189 | 34 | 38.9-103.7 | 63.2 |
| 11 | 1 | 1470 | 4 | 5.1- 10.1 | 8.6 |
| 11 | 4 | 660 | 3 | 4.5- 6.3 | 5.2 |
| 11 | 5 | 1380 | 1 | 2.7 | 2.7 |
| ** | 6 | . 887 | 1 . | 1.8 | 1.8 |
| 11 | 7 | 1430 | 2 | $2.2_{\bar{a}}$ 3.1 | 2.9 |
| 11 | 8 | 919 | 1 | 1.9 | 1.9 |
| 11 | 11 | 460 | 3 | 2.8- 3.3 | 3.0 |
| . 11 | 12 | 1410 | 3 | 1.3- 2.2 | 2.0 |
| 11 | 13 | 1073 | 1 | 1.4 | 1.4 |
| 11 | 15 | 3101 | 2 | 0.97- 3.8 | 1.2 |

TABLE 5 PERMEABILITY RATES - SOIL SAMPLE "E"

Wet Density

Moisture Content

Before Test 89.7 1bs/cu ft

Before Test 12.2%

After Test 105.6 lbs/cu ft

After Test

32.1%

Dry Density

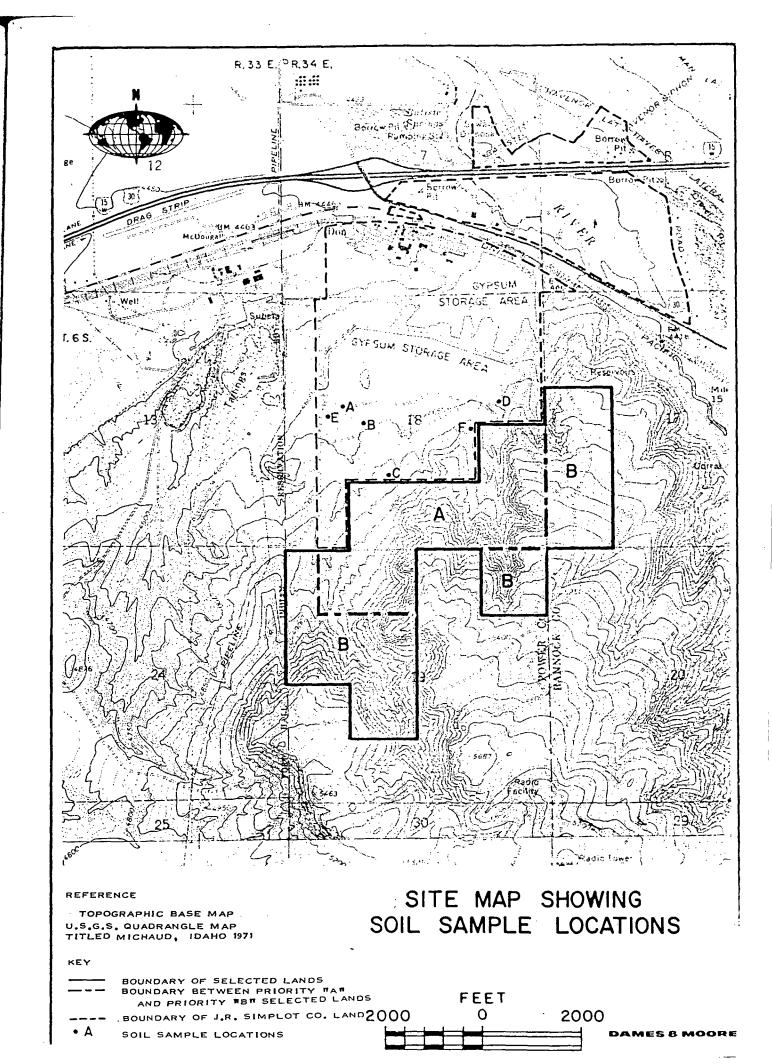
After Test

80.0 lbs/cu ft

| Water Source | Elapsed Time (Days) | Observation Time (Minutes) | Number of Observations | Permeability Range | In Ft/Yr Mean |
|-----------------|------------------------|----------------------------------|---------------------------|--------------------|------------------|
| Gypsum | | | | | |
| Slurry | 0 | 171 | 31 | 71.3-259.2 | 122.0 |
| ** | 1 | 755 | 3 | 4.0- 7.6 | 4.9 |
| 11 | 4 | 660 | 3 | 1.5- 2.7 | 2.4 |
| 11 | 5 | 1380 | 1 | 2.2 | 2.2 |
| 71 | 6 | 1425 | 2 | 2.2- 2.4 | 2.3 |
| 11 | 7 | 300 | 1 | 1.2 | 1.2 |
| 11 | 8 | 919 | 1 | 2.2 | 2.2 |
| 11 | 11 | 460 | 3 | 0.86- 1.7 | 1.2 |
| 11 | 12 | 1410 | 3 | 1.6- 1.9 | 1.8 |
| 11 | 13 | 1073 | 1 | 1.7 | 1.7 |
| 11 | 15 | 3101 | 2 | 0.50- 1.6 | 1.5 |

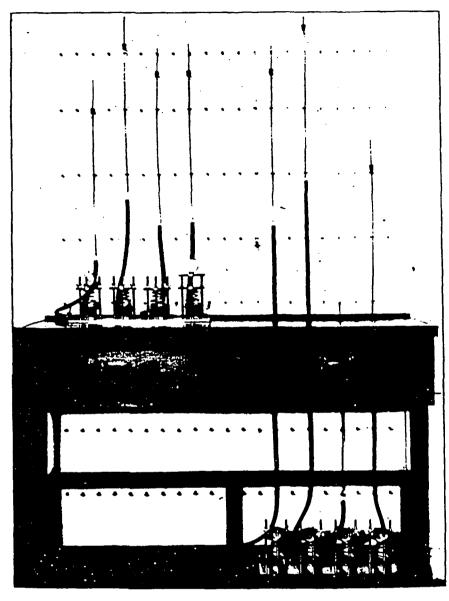
TABLE 6 PERMEABILITY RATES - SOIL SAMPLE "F"

| Water | Elapsed Time | Observation Time | Number of | Permeability in | n Ft/Yr |
|--------|--------------|---------------------|--------------|-----------------|---------|
| Source | (Days) | (Minutes) | Observations | Range | Mean |
| Gypsum | | | | • | |
| Slurry | . 0 | 36 | 3 | 168.5-231.2 | 215.4 |
| + 11 | 1 | 500 | 2 | 8.7- 37.3 | 10.8 |
| 11 | . 4 | 4045 | 2 | 0.51- 0.07 | 0.10 |
| 11 | 5 | 1660 | 4 | 0.14- 2.8 | 2.0 |
| 11 | 6 | 927 | 2 | 0.00- 0.13 | 0.06 |
| 11 | 7 | 1502 | 2 | 0.00 | 0.00 |
| 11 | 8 | 930 | 1 | 0.44 | 0.44 |
| 11 | 11 | 4875 | 1 | 0.46 | 0.46 |
| 11 | 12 | 1120 | 2 | 0.07- 0.23 | 0.10 |
| 11 | 13 | 1100 | 1 | 0.42 | 0.42 |



The quantity and the velocity of flow of water which will escape through an earth structure or percolate through soil are dependent upon the permeability of the earth structure or soil. The permeability of soil has often been calculated by empirical formulas but is best determined by laboratory tests, especially in the case of compacted soils.

A one-inch length of the core sample is sealed in the percolation apparatus, placed under a confining load, or surcharge pressure, and subjected to the pressure of a known head of water. The percolation rate is computed from the measurements of the volume of water which flows through the sample in a series of time intervals. These rates are usually expressed as the velocity of flow in feet per year under a hydraulic gradient of one and at



APPARATUS FOR PERFORMING PERCOLATIONS TESTS

Shows tests in progress on eight samples simultaneously.

a temperature of 20 degrees Centigrade. The rate so expressed may be adjusted for any set of conditions involving the same soil by employing established physical laws. Generally, the percolation rate varies over a wide range at the beginning of the test and gradually approaches equilibrium as the test progresses.

During the performance of the test, continuous readings of the deflection of the sample are taken by means of micrometer dial gauges. The amount of compression or expansion, expressed as a percentage of the original length of the sample, is a valuable indication of the compression of the soil which will occur under the action of load or the expansion of the soil as saturation takes place.

METHOD OF PERFORMING PERCOLATION TESTS

THE UNIVERSITY OF UTAH COLLEGE OF MINES AND MINERAL INDUSTRIES SALT LAKE CITY 84112

DEPARTMENT OF GEOLOGY
AND GEOPHYSICS

717 MINERAL SCIENCE BUILDING

December 9, 1975

Dr. Peter F. Olsen
Project Ecologist
Dames and Moore
Suite 200
250 East Broadway
Salt Lake City, Utah 84111

Dear Dr. Olsen:

Enclosed is a report of our optical investigation of "simcrete" samples. We have found two distinct types of secondary material which would decrease porosity and permeability and increase cohesive strength. The first, shown in photographs 1, 2, 3, and 4, is isotropic and has a refractive index below 1.54. The second, shown in photographs 5, 6, and 7, is anisotropic radiating crystals with refractive indices below 1.54, low birefringence, and parallel extinction. Neither of these materials could be identified as to chemical species with current information.

Further studies should include microprobe determination of the composition of each phase and an x-ray diffraction study of each phase.

Thank you for the opportunity to be of service.

Sincerely yours,

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Report On The Optical Investigation

The samples of old and young 'simcrete' were examined under a low power binocular microscope to determine the appearance of the cementing material. Two types of secondary material were identified. Some of the old 'simcrete' had discontinuous, parallel partings which contained a vitreous coating. These partings were well developed in a number of samples but in general, both the old and young 'simcrete' is dense and without the partings. Both old and young 'simcrete' had small, soft, white spots of material that appeared secondary in nature.

Four samples were chosen for their good development of the two unknown materials. These were cut into slices and cemented to glass slides. The cemented slices were then polished to a thickness of about 0.03mm, and a cover glass epoxied to each mount.

These petrographic slides were examined and photographed under plane polarized light. The following photographs and their accompanying explainations demonstrate the maximum amount of information that can economically be obtained from this material by optical methods.



Photo 1

Two open partings, partially filled with an isotropic, high relief, low RI, crystalline material that's apparently a cement. The detrital grains are quartz and feld-spar with a brown matrix of clay and organic material. The cement completely fills the parting in the upper right corner of the frame. The sample is of the old simcrete. The bar scale represents 0.5mm. The box encloses the field of photo 2.



Photo 2

A close-up of photo 1. The unknown material stands out in high relief against the epoxy filled parting. The obvious crystalline nature is readily apparent. The circular feature in the upper left corner is a bubble in the epoxy. The bar scale represents 0.1mm.



Photo 3

A void, nearly filled with the cementing material. The angular boundary of the cement with the central part of the cavity may indicate the maximum growth of the crysalline cement. This might demonstrate the reduction of the primary porosity by the cement. The bar scale represents 0.5mm.



Photo 4

A parting, completely filled with the unknown material runs diagonally across the frame. A dark, linear feature seems to bisect the parting lengthwise, and may be due to the growth of the cement crystals from either side of the parting. The sample is of the old 'simcrete'. The bar scale represents 0.5mm.



Photo 5

A low magnification frame of a sample of the younger 'simcrete'. The high apparent porosity is due to the plucking of this soft rock in rolishing. The previously mentioned cement is present plus another unknown material which occurs as dark spots in this frame. In the hand specimens, these spots are white and very soft. These spots are also visible in the old 'simcrete'. The bar scale represents 0.5mm.



Photo 6

A higher magnification view of part of frame ⁵. The spots are seen as radiating, crystalline material. The radiating crystals have high relief, low RI, low birefringence, and parallel extinction. All of the spots are mantled by a dark amorphous material. Note that the crystals seem to mantle the detrital grains with no apparent interaction. The bar scale represents 0.1mm.



Photo 7

A high magnification view of one of the spots, showing the lack of reaction between the radiating crystals and the detital grains. The very fine fabric of the spots and their mantling amorphous covering prevents further optical investigation of this still unknown material. The bar scale represents 0.1mm.

ATTACHMENT 4

HUNDRED FOLD REDUCTION IN PERMEABILITY UNDER A GYPSUM STACK

by

J. F. COCHRANE
J. R. Simplot Company
Pocatello, Idaho

recycled paper

ecology and environment

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SUMMARY:

Laboratory investigations have verified field observations that gypsum slurry water reacts chemically with native silt loess soils underlying an operating gypsum storage area to significantly reduce permeability. The original soil permeabilities were about 50 to 250 feet per year. These were reduced through reaction between the soil and the percolating gypsum slurry water to about one foot per year or less during a 15-day test. The soil at the gypsum storage area in Southeastern Idaho is a calcareous silt loess and ranges in depth from a few feet to in excess of 60 feet.

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The chemical species causing the reduced permeability were not positively identified. Optical examination of field samples revealed the presence of two distinct types of secondary material which decreased porosity and permeability and increased cohesive strength. Comparative studies of the native silt loess soil and the resulting soil after treatment with gypsum slurry water were conducted by X-ray diffraction and X-ray emission. These studies indicated the presence of quartz, calcite and dolomite in the native soils; calcite and dolomite were absent in the treated soil. In addition, the treated soil contained an additional component which was not identified. The treated soil contained more sulfur, phosphorus, calcium and less aluminum than the native soil. To the extent that these reactions occur at various gypsum storage sites, they should contribute significantly to the minimization of seepage rates.

BACKGROUND:

The J. R. Simplot Company has operated a phosphate fertilizer complex in Southeastern Idaho near Pocatello for approximately 34 years. Gypsum has been produced as a byproduct of wet process phosphoric acid (WPA) production for 27 years. The original gypsum storage area was abandoned in 1966. A new gypsum disposal area was constructed on a 100-foot high bench South of the plant. Because of the distance and elevation involved to reach the new storage area, it was decided to install gypsum thickeners to concentrate the material to about 35 to 40 weight percent solids before pumping the material to the storage area. The new gypsum storage area receives a small volume of water in comparison to conventional gypsum storage areas which do not use a thickener. Nevertheless, it was noticed by plant personnel that water tended to accumulate in a relatively short time after gypsum was pumped onto previously uncovered soil.

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Observations by personnel from a consulting engineering firm during preparation of an Environmental Analysis Record confirmed observations by plant personnel that gypsum slurry water reacted with the native soil to greatly reduce permeability. Subsequent to this the consulting firm was hired to perform laboratory studies for the purpose of determining if the observed reduction in permeability could be reproduced in the laboratory and if the mechanism and chemistry causing the reduced permeability could be identified.

The byproduct gypsum is a di-hydrated calcium sulfate produced by reacting sulfuric acid with ground phosphate ore to produce phosphoric acid. The phosphoric acid is separated and used to make various grades of phosphate fertilizers. Approximately five tons of gypsum is produced for each ton of phosphate (P205) produced by the WPA plant. In the storage pile, the gypsum exhibits bands and layers of different coloration, alternating generally from light gray to dark gray. The darker layers result from organic impurities in the phosphate ore, but do not produce any measurable difference in the engineering properties of the gypsum. This layered structure results in a highly anisotropic permeability; that is, the permeability in the horizontal direction is many times greater than that in the vertical direction. Chemically, the gypsum tailings are composed of calcium sulfate (CaSO4.2H2O) with various impurities. Chemical analyses of the solid and liquid fractions will vary on a daily basis. The composition of a one-day composite for the two fractions is shown in Table 1.

The general soil cover in this area is described as calcareous silt. This soil, having been deposited by wind, is commonly characterized as loess or silt loess. The soil ranges in depth from a few feet to in excess of 60 feet at the gypsum storage area as determined by previous field investigations. Hydrometer analysis of a soil sample showed the following particle size distribution for the total sample: sand (greater than 0.05 mm), 39.5%; silt (0.05-0.002 mm), 49.2%; clay (less than 0.002 mm), 11.3%.

Wind blown soils of this type are found in portions of most of the Midwestern and Northwestern states; beginning near the Great Lakes and extending to Washington and Oregon. _ 4 N º

Soil samples were taken using thin wall samplers from the top six inches of soil at five locations. All of these locations will eventually be covered by by-product gypsum. All samples were disturbed during sampling and had to be recompacted. A two-inch long core from each sample was selected for the actual permeability tests. The permeability tests were performed under a confining pressure of 100 pounds per square foot.

Two of the soil samples were subjected to permeability tests utilizing tap water for six days followed by 14 days of testing utilizing water from the gypsum slurry. Three of the soil samples were tested for 15 days utilizing only water from the gypsum slurry. Permeability of another sample taken at a depth of six feet was tested for 13 days utilizing only water from the gypsum slurry.

Two samples of soil located under the gypsum storage area were collected for optical and X-ray examination. Optical examination of thin sections made from the samples was done to measure refractive index, etc., and to make photomicrographs. Samples of the native silt loess soil and treated samples were compared by X-ray diffraction and X-ray emission studies.

RESULTS:

Results of the permeability tests are shown in Tables 2 through 7. The change in soil permeability is especially dramatic for samples "A" and "B" because these samples were first tested with tap water and then tested with water from the gypsum slurry. The initial permeability of the samples was about 80 and 350 feet per year respectively. After exposure to tap water for six days the permeability had decreased to 62 and 140 feet per year respectively. After exposure to water from the gypsum slurry for one day, the permeability had decreased to seven and five feet per year respectively. Permeability of both samples decreased to less than one foot per year before completion of the 14-day exposure to water from the gypsum slurry.

It was noted that sample "E" shows the greatest permeability (1.5 feet per year) and also the lowest density before and after the tests. This suggests that this particular sample may not have been recompacted is much as the other soil samples. In any event, the results are consistent with field experience which indicates that a soil with greater density will have a lower permeability.

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The optical investigation of the treated samples indicated two distinct types of secondary material had formed that would decrease the porosity and permeability and increase the cohesive strength. The chemical species of these materials was not identified. The first chemical specie is isotropic and has a refractive index below 1.54. The second chemical specie is anisotropic radiating crystals with a refractive index below 1.54; the crystals exhibit bi-refringence and parallel extinction. The photomicrographs show the first chemical specie to be of obvious crystalline nature. This material was observed to partially or completely fill voids in the original soil. This crystalline material was observed in an older soil material taken from a stratum approximately one foot in thickness located about 50 feet below the surface of the abandoned gypsum storage area. A younger material taken at the gypsum-soil interface where gypsum had been in place for about six months and covered the soil to a depth of only two to five feet did not contain the above mentioned crystalline material. It did, however, contain a second chemical specie. This second material was observed to consist of radiating crystals having high relief, a low refractive index, low bi-refringence, and parallel extinction. This material showed no apparent interaction with the adjacent soil particles. These crystals had grown to a size in excess of 100 microns. This chemical specie would be expected to reduce porosity but not create the cementing action observed by the first chemical specie.

The initial pH of the water from the gypsum slurry used in these permeability tests was 1.7. Following percolation, through soil samples, a composite sample showed a pH of 3.6.

Neutralization of the water from the gypsum slurry with calcium precipitates a large percentage of the soluble fluoride and silica at a final pH of 3.6.

The unidentified compounds which cause soil cementing and reduced permeability resulted in the material being referred to as "Simcrete" in reference to Simplot concrete. Formation of the "Simcrete" substance did not occur under the laboratory conditions of testing during the short-term permeability tests. However, these samples, when examined following the tests, showed positive indications that such induration was commencing with definite cementation having taken place in the upper portion of the samples. The chemical reaction or reactions producing "Simcrete" is unknown at the present time, but involves a change from a calcareous to non-calcareous state

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with replacement of calcite and dolomite. The cementing substances are probably compounds of calcium phosphate, sulfate, and/or fluoride and possibly containing iron and magnesium. The X-ray diffraction and X-ray emission studies indicate the presence of quartz, calcite and dolomite in the native soil; calcite and dolomite were absent in the "Simcrete". In addition, it was determined that the "Simcrete" contained more sulfur, phosphorus, and calcium and less aluminum than the silt loess soil. The older "Simcrete" sample showed components which were not present in the native soil. These components had X-ray diffraction d-spacings of 9.61, 5.91, 5.07, 4.19, 3.23, 2.83, 2.72, 2.56, 2.34, and 2.18 angstrom units.

CONCLUSION:

The practical significance of the soil-gypsum slurry water reaction is that a liner of very low permeability is created under the gypsum storage area in a short period of time, wherever this reaction occurs. This reaction, with its reduced permeability, may be expected to occur wherever similar reactive soil underlies the gypsum storage area. Hydraulic studies in the laboratory showed that soil having original permeabilities of 50 to 250 feet per year were reduced by the unidentified chemical reactions to permeabilities ranging from .85 to 1.5 feet per year within 15 days. The laboratory soils tested for permeability were also measured for density. Those samples which had the greatest density showed the lowest permeability.

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A cementing action was noted on the surface of these samples during the laboratory testing.

The X-ray studies indicated the presence of quartz, calcite, and dolomite in the native soil. The soil samples which had been exposed to water from the gypsum slurry did not contain calcite or dolomite. The optical examination revealed the presence of two yet unidentified crystalline materials. One of the crystalline materials did not fully occupy voids in the soil because of the radial characteristic of the crystalline material. The second compound appeared to be attached to the soil matrix and progressively grew into the void in a solid mass until, in some cases, the void was entirely filled with the crystalline material. In summary, although the chemical reactions remain unknown at the present time, the soil-gypsum slurry water reaction has been shown to reduce soil permeability in both field and laboratory conditions by amounts ranging from 97 to 99% in about two weeks of exposure.

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CHEMICAL CHARACTERISTICS OF SOLID AND LIQUID FRACTIONS

OF GYPSUM SLURRY

(Daily composite sample taken from influent to operating gypsum storage area at J. R. Simplot Company plant)

| Constituent | Solids (%) | Liquid (mg/1) |
|--|-------------|---------------|
| Sulfate as SO ₄ | 53.500 | 3020.0 |
| Calcium as Ca ⁴ | 20.350 | 320.0 |
| Silicon Dioxide | 7.150 | 133.30 |
| Phosphoric acid as P ₂ O ₅ | 1.450 | 4800.0 |
| Aluminum as Al | 0.985 | 175.70 |
| Sodium as Na | 0.745 | 27.63 |
| Fluoride as F | 0.560 | 3200.0 |
| Strontium as Sr | 0.025 | ND |
| Iron as Fe | 0.025 | 6.898 |
| Magnesium as Mg | 0.015 | 360.0 |
| Zinc as Zn | 0.006 | 15.0 |
| Chromium as Cr | 0.004 | 0.703 |
| Manganese as Mn | 0.004 | 4.943 |
| Vanadium as V | 0.003 | 17.231 |
| Copper as Cu | 0.002 | 3.862 |
| Cadmium as Cd | 0.001 | 1.585 |
| Lead as Pb | 0.001 | 0.174 |
| Uranium as U | < 0.001 | 1.350 |
| Molybdenum as Mo | 0.000 | 0.328 |
| Antimony as Sb | 0.000 | 0.30 |
| Selenium as Se | 0.000 | 0.260 |
| Silver as Ag | 0.000 | 0.029 |
| Arsenic as As | 0.000 | 0.013 |
| Mercury as Hg | 0.000 | 0.005 |
| Cyanide as Cn | 0.000 | < 0.01 |
| Water of Hydration | 18.170 | |
| То | tal 102.996 | 12089.311 |

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PERMEABILITY RATES - SOIL SAMPLE "A"

Wet Density

Moisture Content

1.1 - 1.3

1.2 - 1.3

0.89- 0.95

0.55- 0.97

0.82- 0.85

1.3

1.2

0.93

0.86

0.85

3

2

2

2

| Before Test | 98.1 lbs/cu ft | Before Test | 13.2% |
|-------------|-----------------|-------------|-------|
| After Test | 111.1 lbs/cu ft | After Test | 28.1% |

Dry Density

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After Test 86.7 lbs/cu ft

8

9

10

11

14

| oility in Ft/Y | | Number of Observa- | Observation Time | sed Time | Elaps | Water |
|--|------------|-----------------------|---------------------|------------------------------------|-------|---------------------------------|
| ge Mean | Range | <u>tions</u> | (Minutes) | Minutes | Days | Source |
| 85.5 79.9 | 76.7-85.5 | 3 | 118 | | 0 | Tap Water |
| 89.4 70.0 | 54.4-89.4 | 9 | 45 | • | 2 | Tap Water |
| 77.8 68.4 | 62.2-77.8 | 5 | 25 | | 5 | Tap Water |
| 68.0 62.3 | 58.3-68.0 | 11 | 49 | | 6 | Tap Water |
| 58.3 55.2 52.6 43.7 33.8 43.7 | | 1 1 1 1 1 | | 15 53 70 82 113 125 | | Gypsum Slurry " " " |
| 28.1 | | 1 | | 235 | | tt |
| 19.7 | | 1 | | 315 | | ** |
| | 4.6 -13.9 | 12 | 538 | | 1 | 17 |
| | 5.2 - 11.7 | 4 | 476 | | 2 | 11 |
| | 3.4 - 4.2 | 5 | 1489 | | 3 | :+ |
| | 0.49- 3.1 | 3 | 349 | | 4 | 11 |
| 0.27 0.1 | 0.07- 0.27 | 3 | 541 | | 7 | ** |
| | | 3 | | | 7 | 11 |

1431

1241

1626

1265

4235

PERMEABILITY RATES - SOIL SAMPLE "B"

| Wet | Density | |
|-----|---------|--|
|-----|---------|--|

Moisture Content

| Before Test | 98.1 lbs/cu ft | Before Test | 11.6% |
|-------------|-----------------|-------------|-------|
| After Test | 114.1 lbs/cu ft | After Test | 28.7% |

Dry Density

After Test 88.6 lbs/cu ft

| Water Source | Elap: Days | sed Time <u>Minutes</u> | Observation Time (Minutes) | Number of Observa- tions | Permeability in Range | n Ft/Yr Mean |
|------------------|---------------|----------------------------|----------------------------|--------------------------------|-----------------------|-----------------|
| Tap Wate | | | 81 | 3 | 289.7-408.7 | 352.5 |
| Tap Wate | | | 45 | 9 | 116.6-182.7 | 144.7 |
| Tap Wate | | | 25 | 5 | 116.6-186.6 | 147.0 |
| Tap Wate | r 6 | | 49 | 11 | 132.2-145.8 | 137.6 |
| Gypsum Slurry | , | 15 | | 1 | | 114.0 |
| 11 | | 53 | | 1 | | 115.1 |
| 11 | | 90 | | 1 | | 33.6 |
| 11 | | 102 | | 1 | | 50.2 |
| 11 | | 133 | | 1 | | 29.4 |
| 11 | | 145 | | 1 | | 22.7 |
| 11 | | 250 | | 1 | | 10.0 |
| it | | 333 | | 1 | | 9.1 |
| 11 | 1 | | 477 | 12 | 1.2 -11.0 | 4.7 |
| 11 | 2 | | 476 | 5 | 2.1 - 7.0 | 3.7 |
| 11 | 3 | | 1489 | 5 | 1.9 - 2.6 | 2.5 |
| 11 | - 4 | | 1273 | 4 | 0.46 - 2.1 | 2.0 |
| *1 | 7 | | 4323 | 4 | 0.02 - 1.3 | 1.4 |
| 11 | 8 | | 1429 | 3 | 0.50 - 1.2 | 1.1 |
| 11 | 9 | | 1241 | 2 | 0.50- 1.0 | 0.63 |
| 11 | 10 | | 1626 | 2 | 0.77- 0.87 | 0.80 |
| 11 | 11 | | 1470 | 2 | 0.25- 1.0 | 0.75 |
| . 11 | 14 | | 4235 | 2 | 0.69- 0.95 | 0.84 |

-415

TABLE 4

PERMEABILITY RATES - SOIL SAMPLE "C"

| Wet Density | • | Moisture Conten | t |
|-------------|-----------------|-----------------|-------|
| | 97.6 lbs/cu ft | Before Test | 11.3% |
| | 113.3 lbs/cu ft | After Test | 29.2% |

Dry Density

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After Test 87.7 lbs/cu ft

| Water Source | Elapsed Time (Days) | Observation Time (Minutes) | Number of Observations | Permeability Range | in Ft/Yr Mean |
|-----------------|------------------------|----------------------------|---------------------------|-----------------------|------------------|
| Gypsum | | • | | | |
| Slurry | 0 | 442 | 33 | 0-51.8 | 7.8 |
| 11 | 1 | 1675 | 5 | 1.3- 7.0 | 2.6 |
| 11 | 4 | 660 | 3 | 2.9- 5.2 | 3.4 |
| . 11 | 5 | 1380 | 1 | 2.1 | 2.1 |
| ** | 6 | 1455 | 2 | 1.3- 1.7 | 1.6 |
| tı | 7 | 300 | ī | 2.9 | 2.9 |
| 11 | 11 | 4843 | 4 | 1.2- 2.2 | 2.2 |
| tt | 12 | 1410 | 3 | 1.2- 1.6 | 1.3 |
| 11 | 13 | 1073 | i | 1.3 | 1.3 |
| 11 | 15 | 3101 | 2 | 1.2- 2.4 | 1.3 |

PERMEABILITY RATES - SOIL SAMPLE "D"

Wet Density

Moisture Content

Before Test 98.5 lbs/cu ft After Test 109.5 lbs/cu ft Before Test 13.2% After Test 25.4%

Dry Density

After Test

87.0 lbs/cu ft

Observation Water Elapsed Time Time Number of Permeability in Ft/Yr Source (Days) (Minutes) Observations Range Mean Gypsum Slurry 0 189 34 38.9-103.7 63.2 1 1470 4 5.1- 10.1 8.6 660 4.5- 6.3 5.2 5 1380 2.7 1 2.7 6 887 1.8 1 1.8 7 1430 2 2.2- 3.1 2.9 8 919 1 1.9 1.9 11 460 3 2.8-3.0 3.3 12 1410 3 1.3-2.2 2.0 13 1073 1 1.4 1.4 15 3101 0.97-3.8 1.2

-417 .

PERMEABILITY RATES - SOIL SAMPLE "E"

Wet Density

Moisture Content

Before Test 89.7 lbs/cu ft Before Test 12.2% After Test 105.6 lbs/cu ft After Test 32.1%

Dry Density

After Test 80.0 lbs/cu ft

| | Water | Elapsed Time | Observation Time | Number of | Permeability | in Ft/Yr |
|---|--------|--------------|---------------------|---------------------|--------------|----------|
| • | Source | (Days) | (Minutes) | <u>Observations</u> | Range | Mean |
| | Gypsum | | | | | |
| | Slurry | 0 | 171 | 31 | 71.3 -259.2 | 122.0 |
| | 11 | 1 | 755 | 3 | 4.0 - 7.6 | 4.9 |
| | 61 | 4 | 660 | 3 | 1.5 - 2.7 | 2.4 |
| | ** | 5 | 1380 | 1 | 2.2 | 2.2 |
| | *1 | 6 | 1425 | 2 | 2.2 - 2.4 | 2.3 |
| | 11 | 7 | 300 | 1 | 1.2 | 1.2 |
| | ** | 8 | 919 | 1 | 2.2 | 2.2 |
| | ** | 11 | 460 | 3 | 0.86- 1.7 | 1.2 |
| | 11 | 12 | 1410 | 3 | 1.6 - 1.9 | 1.8 |
| | 11 | 13 | 1073 | 1 | 1.7 | 1.7 |
| | 11 | 15 | 3101 | 2 | 0.50- 1.6 | 1.5 |

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TABLE 7

PERMEABILITY RATES - SOIL SAMPLE "F"

| Water | Elapsed Time | Observation Time | Number of | Permeability i | n Ft/Yr |
|--------|--------------|---------------------|---------------------|----------------|---------|
| Source | (Days) | (Minutes) | <u>Observations</u> | Range | Mean |
| Gypsum | | · | | | |
| Slurry | 0 | 36 | 3 | 168.5 -231.2 | 215.4 |
| 41 | 1 | 500 | 2 | 8.7 - 37.3 | 10.8 |
| .11 | 4 | 4045 | 2 | 0.51- 0.07 | 0.10 |
| 11 | 5 | 1660 | 4 | 0.14- 2.8 | 2.0 |
| 17 | . 6 | 927 | 2 | 0.00- 0.13 | 0.06 |
| 11 | 7 | 1502 | 2 | 0.00 | 0.00 |
| . 11 | 8 | 930 | . 1 | 0.44 | 0.44 |
| 11 | 11 | 4875 | . ī | 0.46 | 0.46 |
| 1f | 12 | 1120 | 2 | 0.07- 0.23 | 0.10 |
| 11 | 13 | 1100 | ī | 0.42 | 0.42 |

DEFINITIONS

- 1. Anisotropic Minerals. The minerals which do not crystallize in an isometric system such as diamond, garnet, fluorite, etc., but contain a definite crystalline system of internal structure.
- 2. Anisotropic Permeability. The permeability varies with direction; i.e., horizontal versus vertical.
- 3. Bi-refringence. Light passing through a transparent mineral creates a double refraction and creates double images.
- 4. Parallel extinction. The wave motion of light has been limited to a single plane of vibration by absorption by certain crystals. When vibration is thus restricted, light is said to be polarized. Light transmitted through two plates of the material is eliminated where the plates overlap when the planes of vibration are 90° apart.

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THE UNIVERSITY OF UTAH COLLEGE OF MINES AND MINERAL INDUSTRIES SALT LAKE CITY 84112

DEPARTMENT OF GEOLOGY
AND GEOPHYSICS

August 15, 1975

717 MINERAL SCIENCE BUILDING

Mr. Dennis J. Paulsen Dames and Moore, Eng. 250 East Broadway Salt Lake City, Utah

Dear Mr. Paulsen:

Two samples, designated Sample 1, silt loess-calcareous and Sample 2, indurated silt loess-noncalcareous, submitted to me on August 11, 1975 were subjected to x-ray analysis with the following results:

- 1. X-ray diffraction. A powder-pack mount of each sample was analyzed using Copper K-alpha radiation to determine differences between samples 1 and 2. Components identified in sample 1 are quartz, calcite, and dolomite. Quartz was identified in sample 2. Calcite and dolomite are missing from sample 2. An additional component or components is present in sample 2 with x-ray diffraction d-spacings of 9.61, 5.91, 5.07, 4.19, 3.23, 2.83, 2.72, 2.56, 2.34, and 2.18 angstrom units. A thorough and careful search of our powder diffraction file has failed to produce a firm identification of this material.
- 2. X-ray emission. Phosphorous, sulfur, calcium, and aluminum contents of samples 1 and 2 were compared using 1-1/4 inch diameter pellets of the samples and a chromium target x-ray tube. Sample 2 contains more S, P, Ca and less Al than sample 1.

The unidentified substance in sample 2 is probably a compound or compounds of calcium, phosphite and/or sulfate possibly containing iron and magnesium. Definite identification will require tedious and time consuming procedures such as heavy liquid separation and purification of the unknown, petrographic analysis of thin sections, or electron microprobe analysis. As a first step complete chemical analysis of samples 1 and 2 for $\mathrm{SO_4}$, $\mathrm{PO_4}$, Na , Mg , Al , Si , P , K , Ca , Mn , Fe , V , etc., is suggested.

The x-ray diffraction and emission analysis charts are enclosed.

Sincerely,

W. T. Parry

Professor

WTP/dl

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REPORT OF SOIL STUDIES

GYPSUM TAILINGS POND

POCATELLO, IDAHO

FOR THE J. R. SIMPLOT COMPANY

DAMES & MOORE

EARTH SCIENCES

REPORT OF SOIL STUDIES

GYPSUM TAILINGS POND

POCATELLO, IDAHO

FOR THE J. R. SIMPLOT COMPANY

DAMES & MOORE

CONSULTANTS IN APPLIED EARTH SCIENCES SOIL MECHANICS - ENGINEERING GEOLOGY - GEOPHYSICS

CHICAGO
HOMOLOCO
HOMO

415 SOUTH SECOND EAST STREET . SALT LAKE CITY II, UTAH . ELGIN 9-8764 PARTNER: WARREN D. CURTIS

July 10, 1962

J. R. Simplot Company P. O. Box 912 Pocatello, Idaho

Attention: Mr. Keith A. Bithell

Gentlemen:

Ten copies of our "Report of Soil Studies, Gypsum Tailings Pond, Pocatello, Idaho, For the J. R. Simplot Company", are herewith submitted.

The scope of these studies was planned in consultation with Mr. Keith A. Bithell of the J. R. Simplot Company. Historical data of the existing tailings embankment and other information pertinent to our studies were provided to us by Mr. Bithell.

The existing dike has a computed safety factor of one. It is therefore concluded that additional construction on top of the existing dike may precipitate a general slide failure. Recommendations for stabilizing the existing dike and construction of additional embankment height are included herewith.

Preliminary recommendations were presented verbally in a conference held with personnel from the J. R. Simplot Company on June 11, 1962. Recommendations for the existing embankment correction were presented in our preliminary letter dated June 13, 1962.

Yours very truly,

DAMES & MOORE

Warren D. Curtis

WDC/KS:ml

REPORT OF SOIL STUDIES

GYPSUM TAILINGS POND

POCATELLO, IDAHO

FOR THE J. R. SIMPLOT COMPANY

SCOPE

Presented in this report are our recommendations, with substantiating data, resulting from our soil studies at the site of the Proposed Gypsum Tailings Pond that is being developed near Pocatello, Idaho, for the J. R. Simplot Company.

The plant site of the Simplot Company is located approximately one mile northwest of the City of Pocatello, Idaho, on U. S. Highway 30 North. The existing tailings pond is bounded on the north by the mainline tracks of the Union Pacific Railroad, and on the west by the Simplot plant. The location of the site with respect to surrounding topographic features is presented on Plate 1, Map of Area. The location and topographic terrain of the existing tailings pond and dike are shown on Plate 2, Plot Plan.

Our studies were undertaken for the following purposes:

- To determine the subsurface soil and ground water conditions
 of the existing tailings pond dike and discharged tailings
 materials.
- 2. To analyze the level of safety from a stability standpoint of the existing tailings pond dike.
- 3. To recommend construction methods that can be employed in increasing the present embankment height.
- 4. To recommend materials which may be utilized in future embankment construction.
- 5. To recommend criteria for the placement of embankment materials.

6. To recommend safe slopes and maximum height for a continued increase in embankment height.

The results of our field explorations and laboratory tests, which provide the basis for our recommendations, are presented in Appendix A, Field Explorations and Laboratory Tests. The dike history is set forth in Appendix B, Historical Sketch of Gypsum Storage Pond.

SITE CONDITIONS

The tailings pond at present occupies a plan area of approximately 700 by 1200 feet. The site lies on the south edge of the river flood plane formed by the Portneuf River. To the south of the site, the terrain rises to form the foothills of the mountain range. The existing pond is bounded on the north by the mainline tracks of the Union Pacific Railroad and on the west by the Simplet plant. The foothills form the southern limits of the pond, and the terrain is slightly rolling to the east of the pond.

The natural riverbed deposits consist predominantly of sand and gravel with a small fraction of silt-sized particles. The natural deposit of the foothills consist predominantly of silts with scattered gravels and boulders.

We understand that a commercial gravel pit at one time occupied the site of the existing tailings pond. In the development of the pond, gypsum tailings were deposited by hydraulic methods into the pit. As the height of the pond was increased, natural soils were imported from the foothills to the south to form the perimeter embankments on the north, west and east sides of the pond. At the present time, the embankment is approximately 50 feet in height adjacent to the railroad right of way.

The subsurface soil conditions at the site were explored by drilling seven exploration borings with truck-mounted rotary wash-boring equipment.

These borings ranged in depths from 20 to 57 feet below the ground surface.

Borings 1, 2, 6 and 7 were drilled through the existing embankment. Borings 3 and 4 were drilled through the gypsum tailings within the embankment and Boring 5 was drilled in the natural soil deposits of the adjoining foothills to the south. In addition to these borings, 11 hand auger borings were drilled to obtain bulk samples of the natural soils and gypsum deposits at various locations. The locations of all of the borings are shown on Plate 2. Detailed descriptions of the soils encountered in the borings are presented in Appendix A of this report.

In general, as revealed by our borings, the natural soils of the adjoining foothills, which were utilized in the perimeter embankments, consist predominantly of silts interspersed with gravel. The gypsum deposits within the embankment also consisted predominantly of silt-sized particles. Due to this similarity in materials, it was extremely difficult to delineate between the natural soils and the gypsum tailings in the borings drilled through the embankment. However, from the results of moisture and density determinations, it is believed that the natural soils may extend as deeply as 30 feet below the top of the embankment at the locations of Borings 1 and 2. At the locations of Borings 6 and 7, the gypsum was encountered at a depth of approximately 12 feet. It is believed that the construction procedure in the past may have resulted in a partial mixing of the two types of materials. All of the borings except Boring 5 were terminated in the natural sand-and-gravel deposit.

At the time of our explorations, standing water was encountered at various depths below the ground surface. The depth at which ground water

was encountered is presented on the detailed logs presented in Appendix A.

DEVELOPMENT OF POND

We have been provided with a brief historical sketch of the procedures employed in the construction of the present embankment. This history is presented in Appendix B of this report.

It is desirous from a Simplot operational standpoint to heighten the present embankment. It is understood that with the present rate of discharge and present area available for storage, the pond will fill at a rate of approximately 10 feet per year. At the time of our exploration, the level of the pond was approximately 10 feet below the existing embankment. Additional embankment height is needed for future plant operations.

Present methods of tailing placement consist of a perimeter discharge along the outer limits of the pond. Free water from the hydraulic discharge system drains to lower ground adjacent to the hillside to the south of the pond. Free water is thereafter removed through a decanting system and is returned to the plant. We understand that this system will be maintained as the pond increases in height.

DISCUSSION AND RECOMMENDATIONS

PRESENT EMBANKMENT:

We have analyzed the level of safety from a stability standpoint of the present tailings pond embankment. Our analyses has been based on a sliding circular type of failure. A failure of this type would result if the actuating forces would exceed the resisting forces of the soil mass. Based on the results of our laboratory test data and engineering analyses, it is concluded that the existing embankment has a factor of safety of one. Such a factor is considered precipitous in normal embankment design. It is thus recommended that no additional construction be undertaken to heighten

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Stability of the embankment also requires that the surface of ponded water be maintained away from the perimeter of the embankment. A minimum distance of 150 feet is recommended. The discussion that follows on corrective measures is based on the assumption that this minimum distance will be maintained in plant operations. Minimum distances are shown on Plates 3-A and 3-B.

RECOMMENDED CORRECTIVE MEASURES FOR PRESENT EMBANKMENT:

It is considered a likely possibility that additional construction on top of the present embankment may precipitate a general slide-type failure. There are numerous methods for correcting a potentially unstable embankment condition. The most feasible in most cases is to flatten the existing slope, thereby reducing the driving forces which tend to cause motion. It is realized that change in the geometric shape of the embankment will present difficult construction problems. However, it is recommended that such a change be made to permit stability in the future embankment.

In our studies, we have analyzed two different methods of slope correction. In our initial plan, it is recommended that the top 17 feet of the outside slope of the present embankment be flattened to a slope of approximately two and one-half horizontal to one vertical. From the data presently available, it is anticipated that such a cut will not penetrate into the underlying gypsum materials. The material taken from the cut may be utilized in building on top or to the inside face of the present embankment. A typical cross section showing the existing embankment and the proposed new configuration is presented on Plate 3-A, Typical Cross Section - Plan A. The embankment, if corrected in accordance with these recommendations, will posses a factor of safety on the order of 1.2 against a sliding-type failure.

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An alternate method of correction is presented on Plate 3-B, Typical Cross Section - Plan B. In this plan, it is recommended that the top 10 feet of the outside slope of the present embankment be flattened to a slope approaching three horizontal to one vertical. The embankment materials resulting from such a cut can be pushed down to the toe of the embankment. The additional weight at the toe will aid materially in the stability of the embankment. However, such a plan will be dependent on the lateral dimension of the property which is available to the J. R. Simplot Company. It is anticipated that a minimum lateral distance of 10 feet from the toe of the present embankment will be required for this plan. It has been computed that this plan will provide for a factor of safety on the order of 1.2 against a sliding-type failure.

Ease of construction will probably necessitate the plan which will be utilized to correct the existing embankment. Either plan recommended will be satisfactory from a stability standpoint.

FUTURE EMBANKMENT DESIGN:

After correction of the present embankment slope is accomplished, it is recommended that a slope of three horizontal to one vertical be utilized for the outside slope of the future embankment. Our studies were directed toward the utilization of either natural soils from the adjacent foothills or gypsum from the existing pond for this construction. However, based on the results of our laboratory tests and engineering analyses, it is concluded that the natural soils exhibit more predictable strength, consolidation, and permeability characteristics, and can be placed more readily than the gypsum. Thus, in our discussions with engineers from the J. R. Simplot Company, it was recommended that the natural soils be utilized for the future perimeter embankment. Our analyses has been directed toward the utilization of the natural soils.

It is recommended that the future embankment be mechanically placed and compacted in layers. The function of compaction is primarily that of making the cover material more stable against wind and rain water erosion than would otherwise develop from loose dumping. With the use of a three-to-one slope, compaction control is not critical to stability. Recommended specifications for the placement of the future embankment materials are outlined in Appendix C of this report. These compaction requirements are not severe and can be readily obtained by reasonable care on the part of the contractor.

We have analyzed the level of safety from the standpoint of a sliding-type failure for an additional 100-foot-high embankment. A computed factor of safety on the order of 1.2 is attainable with a slope of three to one. This factor of safety is dependent upon maintaining the surface of the ponded water at a minimum distance of 150 feet from the edge of the slope. If this distance is maintained, it is anticipated that leakage through the embankment will be inconsequential in amount.

From our discussions, it is understood that the embankment will be constructed in annual stages of approximately 10 feet in height. The gypsum tailings will be discharged until the pond is essentially filled and another embankment stage will be constructed. The possibility of slides into the tailings pond during the construction stage when equipment is operating on the inside edge of the embankment has been investigated. A factor of safety against sliding of 1.5 is maintained if slopes are not steeper than one and one-half horizontal to one vertical for the 10-foot height. It is considered that this slope is the angle of repose of the natural soils. These findings are based on average conditions for gypsum that has been drained. Operators of equipment should be alert for minor pockets of

soft material which can be resolved by use of flatter slopes over soft sections.

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The following Plates and Appendices are attached and complete this report:

Plate 1 - Map of Area

Plate 2 - Plot Plan

Plate 3-A - Typical Cross Section - Plan A

Plate 3-B - Typical Cross Section - Plan B

Appendix A - Field Explorations and Laboratory Tests

Appendix B - Historical Sketch of Gypsum Storage Pond

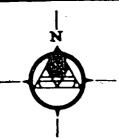
Appendix C - Suggested Specifications for Placing Embankment Fills

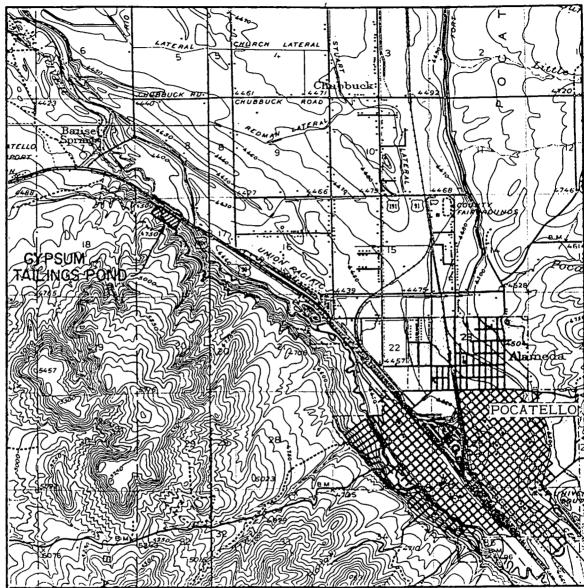
Respectfully submitted,

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DAMES & MOORE

Warren D. Curtis





REFERENCE;

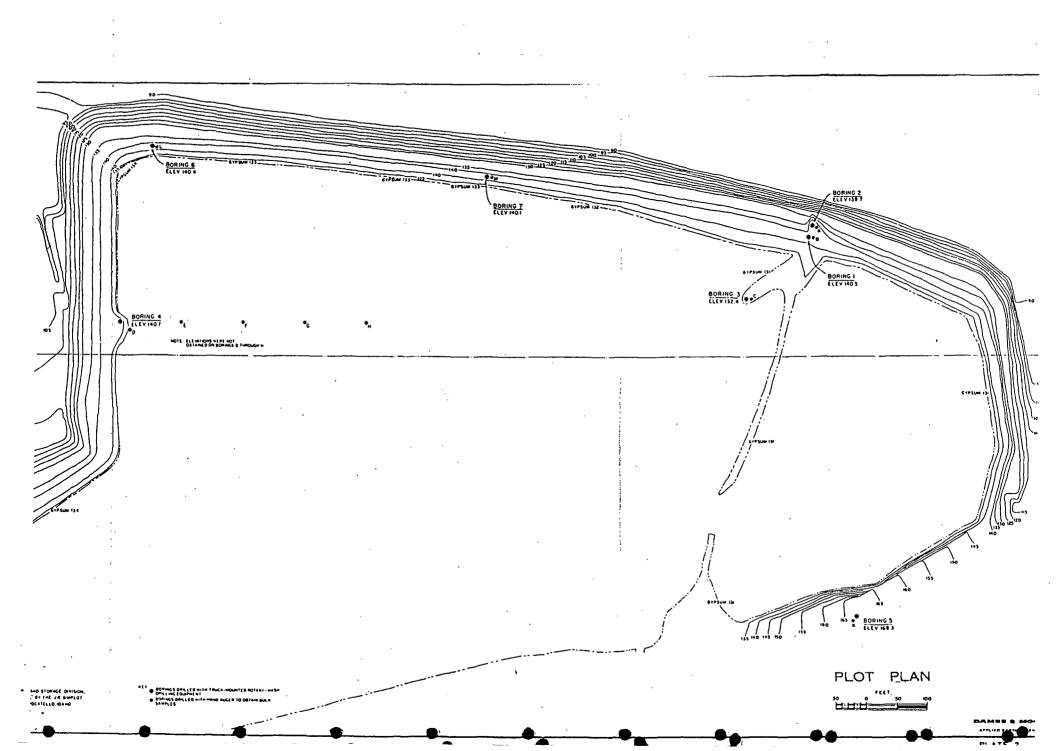
• U.S.G.S. MAPS OF MICHAUD, IDAHO QUADRANGLE AND POCATELLO, IDAHO QUADRANGLE.

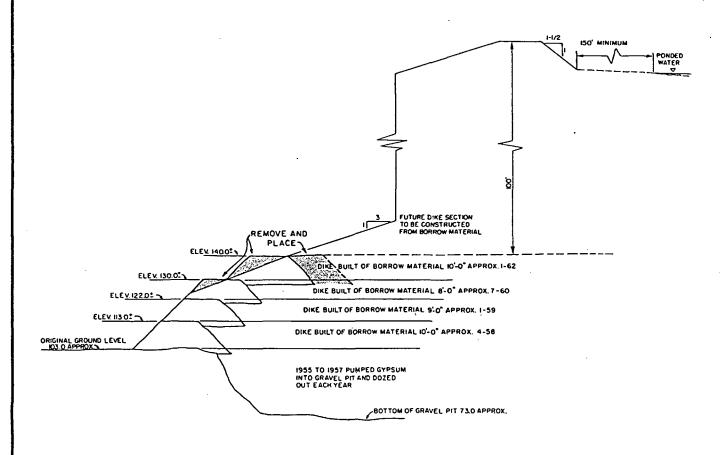
MAP OF AREA



DAMES & MOOR

APPLIED EARTH SCIENCES

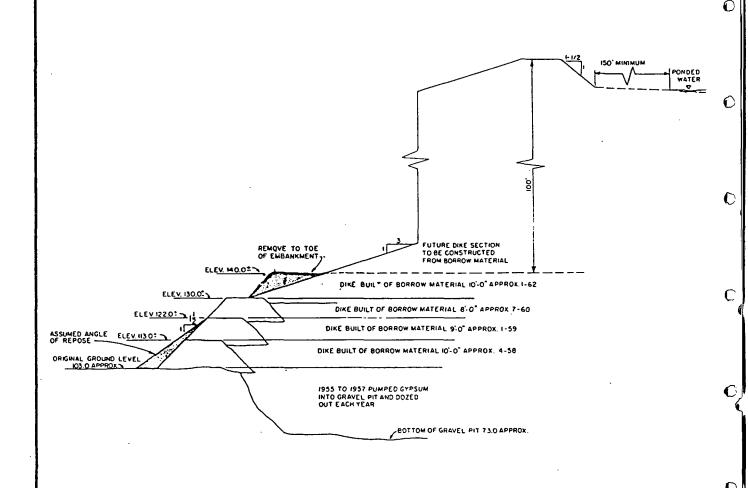




REFERENCE SECTION TITLED, "HISTORICAL CROSS SECTION WEST AND NORTH WALLS GYPSUM POND DIKE 1955 TO 1962", TAKEN FROM PRINT TIO. K-101, BY THE J.R. SIMPLOT CO., DATED 4-29-62, AND TITLED, "CONVEYING AND STORAGE DIVISION SECTIONS GYPSUM STORAGE POND DIKE 1962".

TYPICAL CROSS SECTION PLAN A

FEET 10 5 0 10 20 30 40 50



REFERENCE:
SECTION TITLED, "HISTORICAL CROSS SECTION WEST AND NORTH
WALLS GYPSUM POND DIKE 1955 TO 1962", TAKEN FROM PRINT NO. K-101,
BY THE JR. SIMPLOT CO, DATED 4-29-62, AND TITLED, "CONVEYING
AND STORAGE DIVISION SECTIONS GYPSUM STORAGE POND DIKE 1962".

TYPICAL CROSS SECTION

PLAN B

FEET 10 5 0 10 20 30 40 50

DAMES & MOORE

APPENDIX A

FIELD EXPLORATIONS AND LABORATORY TESTS

FIELD EXPLORATIONS

The subsurface soil conditions at the site were explored by drilling seven test borings to depths ranging from 20 to 57 feet below the ground surface. Six of these borings in the embankment and tailings pond area penetrated into the underlying sand, gravel and boulder formation. In addition, linear borings were also drilled.

Undisturbed samples of the various soils penetrated were obtained utilizing the Dames & Moore Soil Sampler illustrated on Page A-I. In addition, loose bulk samples of the various soils were obtained from the hand auger borings. The soils encountered in the borings were classified in the field by visual and textural examination and the classifications were verified by further inspection and testing of the samples in the laboratory. Graphical representations of the soils encountered in the borings are shown on Plates A-IA through A-IG, log of Borings. The nomenclature utilized to classify the soil types is described on Plate A-2, Soil Classification Chart and Key to Test Data.

Ground surface elevations are presented above the log of each test boring. These elevations were provided to us by the engineering staff of the J. R. Simplot Company.

LABORATORY TESTS

GENERAL:

The physical characteristics of the soils encountered at the site were determined in a series of laboratory tests on samples obtained during our field explorations. These tests include triaxial compression tests, direct shear tests, consolidation tests, compaction tests, percolation tests,

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particle-size determinations, and moisture and density determinations. The test results are presented in the appropriate sections of this Appendix. This Appendix contains information on the methods utilized in performing the various tests.

STRENGTH TESTS:

Triaxial compression tests and direct shear tests were performed on selected soil samples to determine the strength characteristics of the various soil strata encountered in the borings. The results of the strength tests, and the associated moisture and density determinations, are presented to the left of the Log of Borings in the manner described by the Key to Test Data shown on Plate A-2. The tests were performed as follows:

Triaxial Compression Tests: Prior to testing, the samples to be tested were saturated and consolidated at the designated confining pressure. The samples, approximately two and one-half inches in diameter and five to six inches in length, were extruded from the sampling rings and the ends fitted with porous stones. Constant lateral air pressure, known as confining pressure, was maintained around a thin rubber membrane in which the sample The drainage lines connected to the cap and base were sealed was encased. to prevent escape of water during the test. The samples were then subjected to axial deflection at a constant rate, and the resistances to compression in the soil were measured. Stress-strain curves for each test were drawn from which the yield point resistances to compression were obtained. For each type of soil tested, a series of Mohr's Circles, one for each test, were plotted on common axes. The relationship of shear strength to normal pressure was then obtained from the strength envelope of the appropriate Mohr's Circles.

<u>Direct Shear Tests</u>: Direct shear tests were also performed on selected undisturbed soil samples to determine the strength characteristics of the various soil strata. The tests were performed in the manner described on Page A-II, Method of Performing Direct Shear and Friction Tests. The tests were performed at field moisture and at saturated moisture conditions to determine the effect of saturation upon the strength characteristics of the soils. Furthermore, the tests were performed at surcharges (pressure applied normal to the ends of the sample) corresponding to the approximate weight of the overburden pressures encountered in the field. A load-deflection curve was plotted for each test and the shearing strength was determined from this curve.

In addition to the direct shear tests performed on the undisturbed soil samples, tests were also performed on compacted core samples of the various materials. The core samples were compacted to 95 per cent of the maximum density attainable as determined by compaction tests. These tests were performed at optimum and saturated moisture conditions and under various surcharge pressures to determine the angle of internal friction of the soils. The results of the direct shear tests performed on the compacted core samples are presented on Plates A-3 and A-4, Compaction Studies.

CONSOLIDATION TESTS:

In order to provide data for the determination of settlement of the Proposed Embankment, consolidation tests were performed on representative undisturbed and compacted core samples. The core samples were compacted to 95 per cent of the maximum density attainable as determined by compaction tests. The tests were performed in accordance with the Method of Performing Consolidation Tests described on Page A-III of this Appendix. The samples were saturated prior to testing. The results of the consolidation tests

performed on compacted core samples are presented on Plates A-3 and A-4. The results of the tests performed on undisturbed soils are presented on Plate A-5, Consolidation Test Data.

COMPACTION TESTS:

In order to study the compaction characteristics of the on-site natural and gypsum soils, compaction tests (Modified A.A.S.H.O.* T 180-57 Method) were performed on selected bulk samples. The tests were performed in the manner described on Page A-IV, Method of Performing Compaction Tests. The results of the compaction tests are presented on Plates A-3 and A-4.

PERCOLATION TESTS:

In order to study the permeability characteristics of the on-site natural and gypsum soils, percolation tests were performed on representative undisturbed and compacted core samples. The core samples were compacted to 95 per cent of the maximum density attainable as determined by compaction tests. The tests were performed in accordance with the Method of Performing Percolation Tests described on Page A-V of this Appendix. The results of the percolation tests are as follows:

| Sample | In-Place Undisturbed or Compacted Core Sample | Scil Type | (Expressed in Feet Fer Year Under a Hydraulic Gradient of One) |
|----------------|--|------------------------|--|
| Boring 3 at 8' | In-Place | Lt. gray silt (gypsum) | 675 |
| Boring 7 at 4' | In-Place | Lt. brown silty loam | 2 |
| Boring D** | Compacted Core | Lt. gray silt (gypsum) | 40 |
| Boring D | Compacted Core | Lt. gray silt (gypsum) | 50 |
| Boring K | Compacted Core | Lt. brown silty loam | . 3 |

^{**}This test was performed utilizing acid water obtained from the gypsum pond.

^{*}American Association of State Highway Officials

PARTICLE-SIZE ANALYSES:

To determine particle-size gradation, sieve and hydrometer tests were performed on the various materials. The tests were performed in accordance with the standards defined by the A.S.T.M. under Designation D 422-54T. The results of the hydrometer tests are presented on Plates A-6A, A-6B, and A-6C, Particle-Size Distribution.

MOISTURE AND DENSITY DETERMINATIONS:

In addition to the moisture and density determinations which were performed in conjunction with the strength and consolidation tests, moisture and density determinations were also performed on additional selected samples. The tests were performed to provide data for correlation between soils at various depths and in different borings. The results of these tests are presented to the left of the Log of Borings.

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The following Plates are attached and complete this Appendix:

Plate A-lA - Log of Borings (Boring 1)

Plate A-1B - Log of Borings (Boring 2)

Plate A-1C - Log of Borings (Boring 3)

Plate A-1D - Log of Borings (Borings 4 and 5)

Plate A-lE - Log of Borings (Boring 6)

Plate A-1F - Log of Borings (Boring 7)

Plate A-1G - Log of Borings (Borings A, B, C, D, E, F, G, H, K, L, and M)

Plate A-2 - Soil Classification Chart and Key to Test Data

Plate A-3 - Compaction Studies, Light Brown Silty Loam
(Natural Soils)

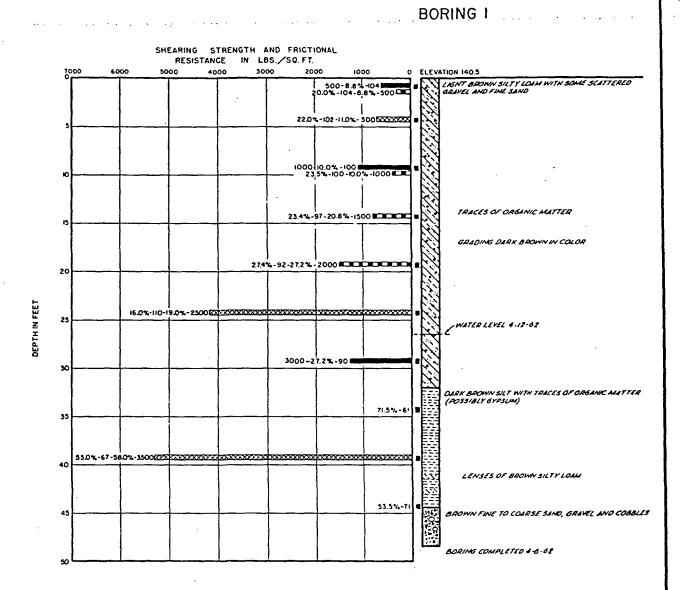
Plate A-4 - Compaction Studies. Light Gray Silt (Gypsum)

Plate A-5 - Consolidation Test Data

Plate A-6A - Particle-Size Distribution

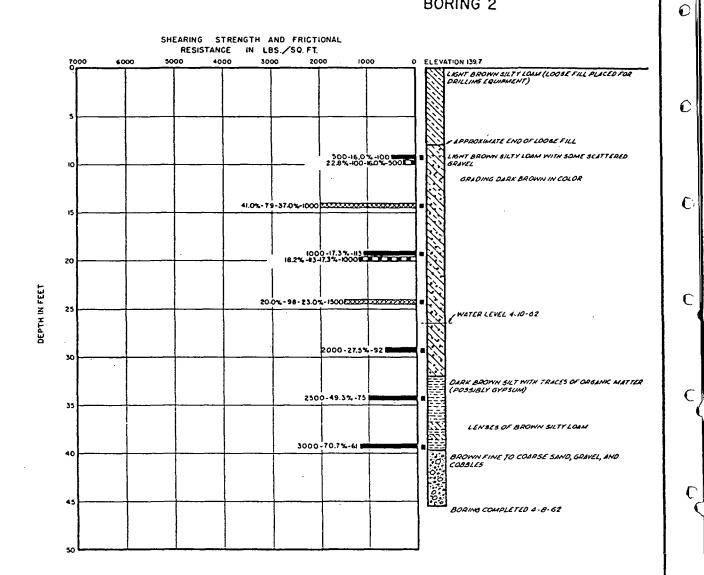
Plate A-6B - Particle-Size Distribution

Plate A-6C - Particle-Size Distribution



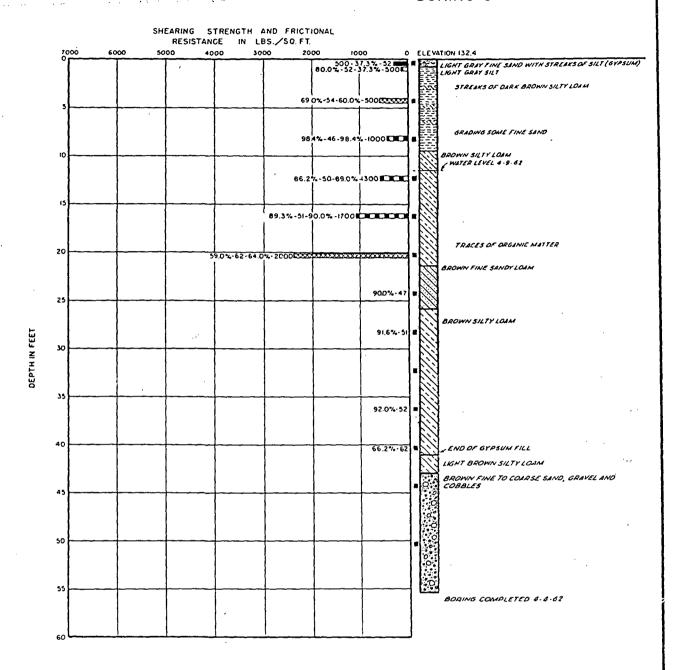
LOG OF BORINGS

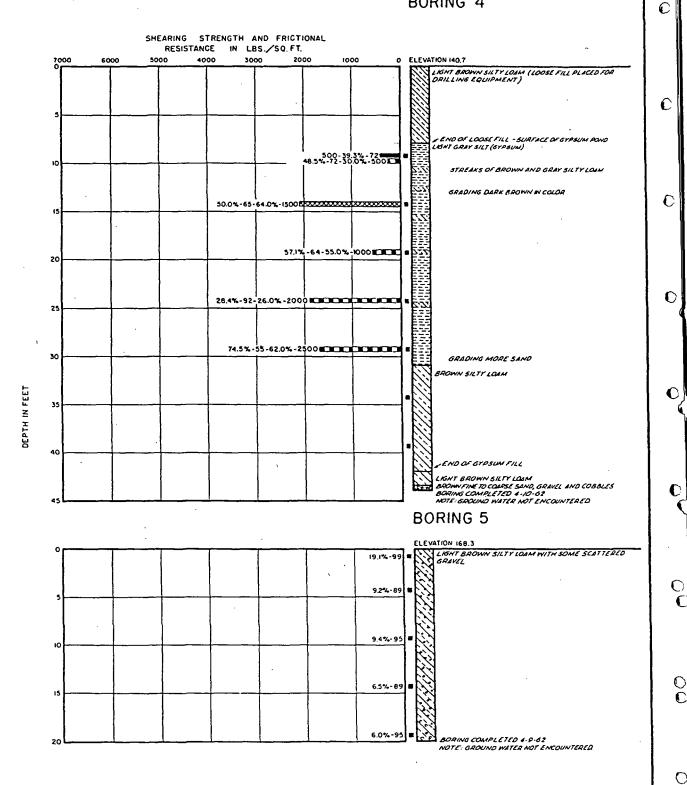
 \mathbf{C}

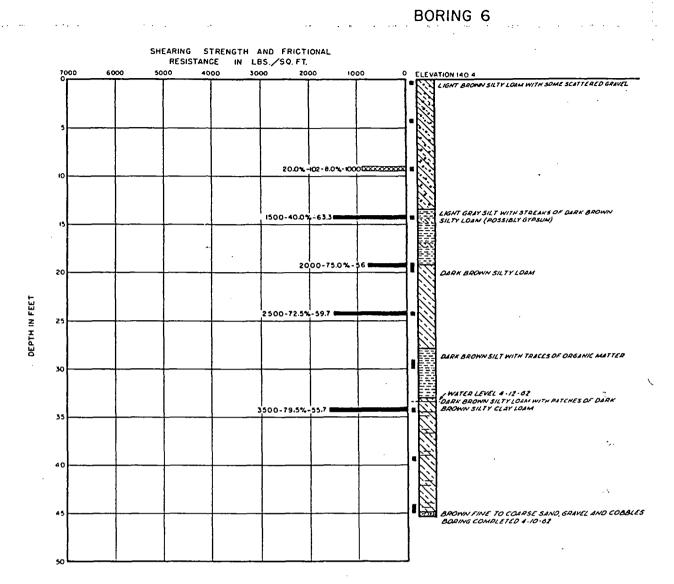


LOG OF BORINGS

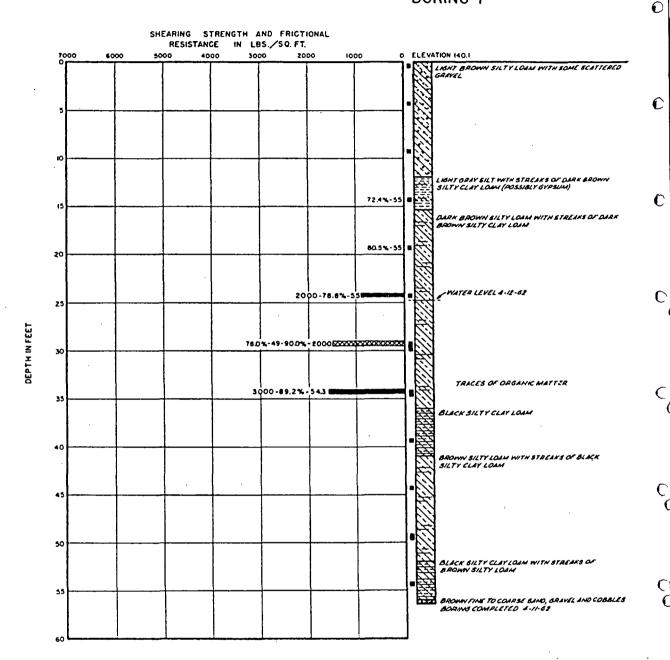
DAMES 8 MOORE

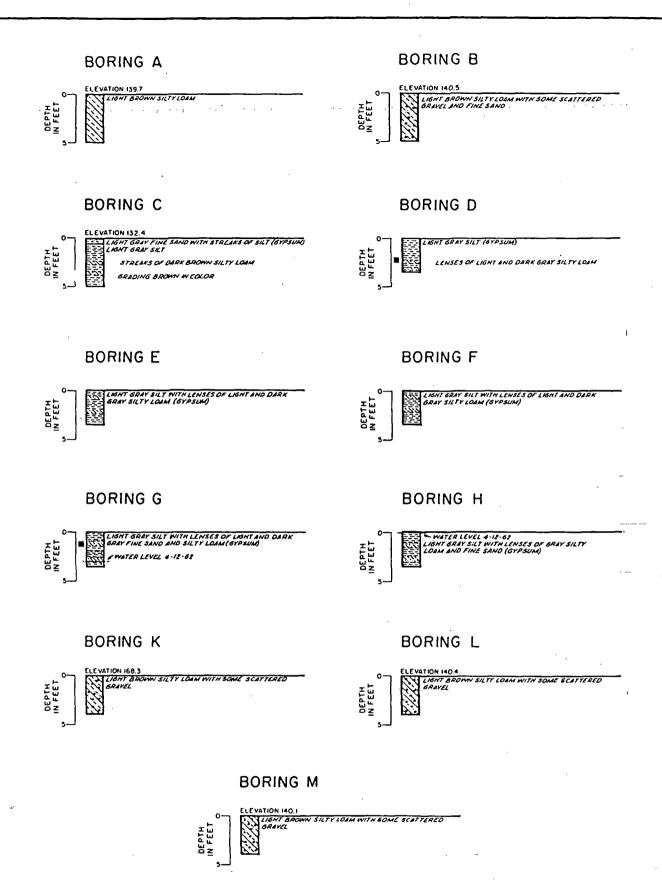


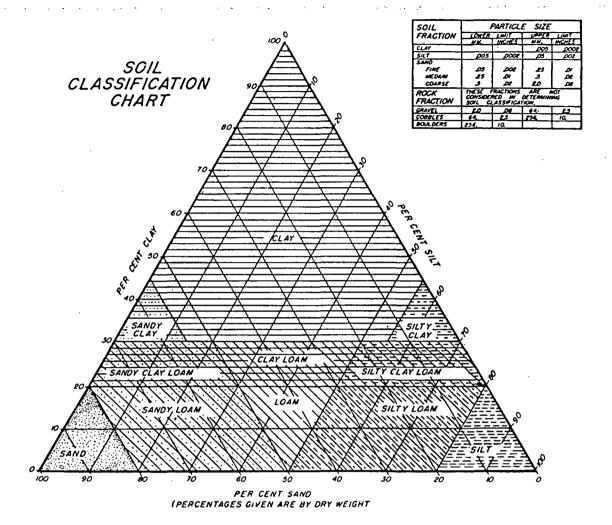




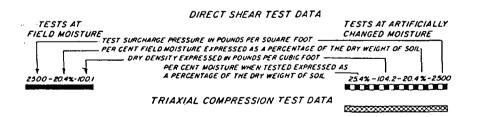
C







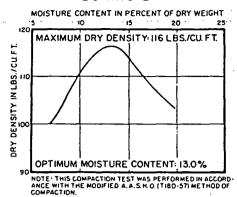
KEY TO TEST DATA



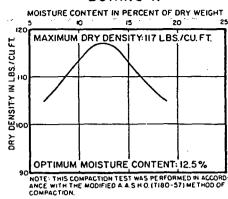
SOIL CLASSIFICATION CHART AND KEY TO TEST DATA

COMPACTION TEST DATA

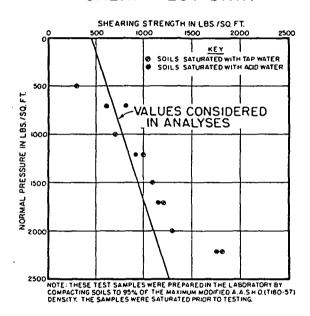
BORING B



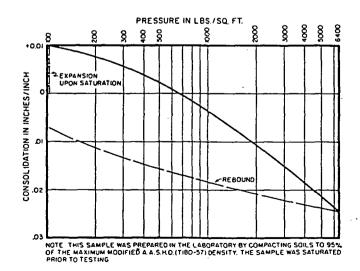
BORING K



SHEAR TEST DATA

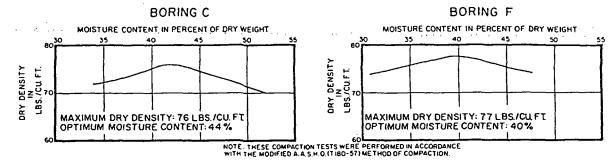


CONSOLIDATION TEST DATA

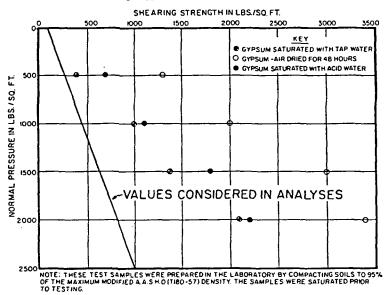


COMPACTION STUDIES LIGHT BROWN SILTY LOAM (NATURAL SOILS)

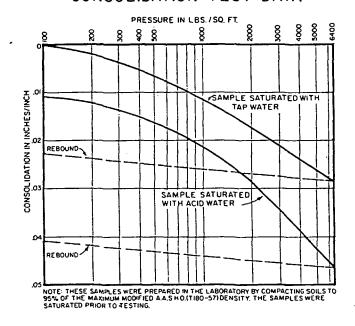
COMPACTION TEST DATA



SHEAR TEST DATA



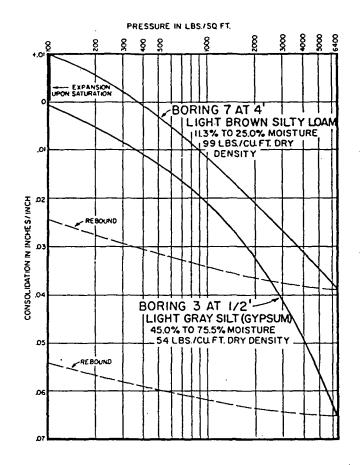
CONSOLIDATION TEST DATA



COMPACTION STUDIES LIGHT GRAY SILT (GYPSUM)

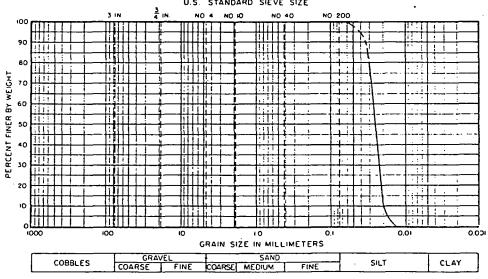
DAMES & MOORI

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CONSOLIDATION TEST DATA

BORING I AT 4' LIGHT BROWN SILTY LOAM U.S. STANDARD SIEVE SIZE NO. 4 NO 10 ili T WEIGHT 70 60 ₽ 50 PERCENT للنيا 30 14:11 ШПП 1111 11111 0.01 10 GRAIN SIZE IN MILLIMETERS CLAY COBBLES FINE COARSE MEDIUM FINE BORING I AT 39' DARK BROWN SILT (GYPSUM) U.S. STANDARD SIEVE SIZE 80 WEIGH 70 60 ₽ Ш. H -----111111 30 20 11111 1.0 GRAIN SIZE IN MILLIMETERS COARSE COBBLES SILT CLAY FINE COARSE MEDIUM BORING 3 AT 4 LIGHT GRAY SILT (GYPSUM) U.S. STANDARD SIEVE SIZE NO 40 3 IN NO 4 NO 10 NO 200 100 1911 161 1 11111 ; [] [] 70 $\Pi \cap \Pi \cap \Pi$.911



NOTE: DASHED PORTION OF CURVE REPRESENTS ESTIMATED VALUE.

PARTICLE - SIZE DISTRIBUTION

BORING 4 AT 14'

LIGHT GRAY SILT (GYPSUM)

C

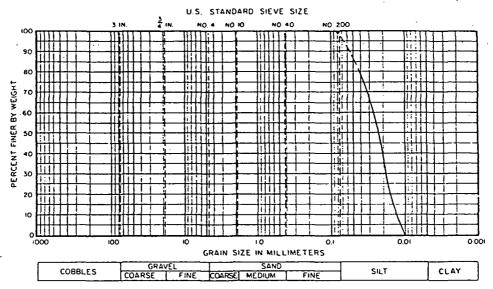
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C

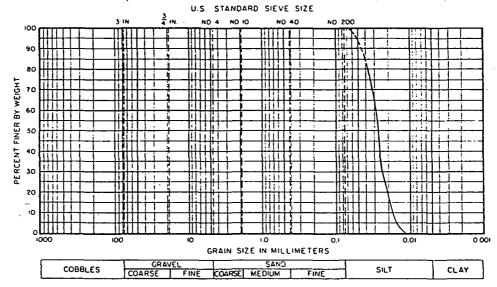
 \boldsymbol{C}

C



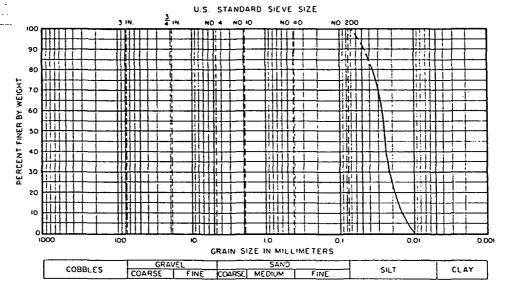
BORING D O-3'

LIGHT GRAY SILT (GYPSUM)



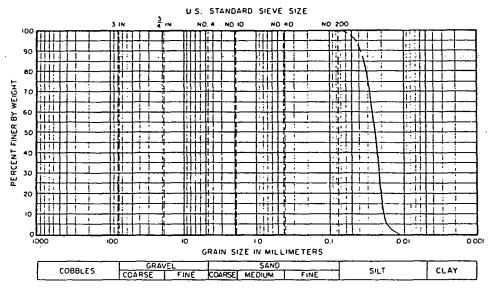
BORING E 0-31/2'

LIGHT GRAY SILT (GYPSUM)



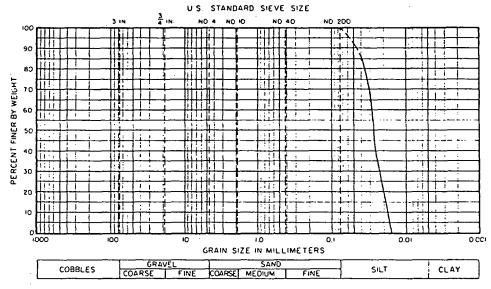


LIGHT GRAY SILT (GYPSUM)



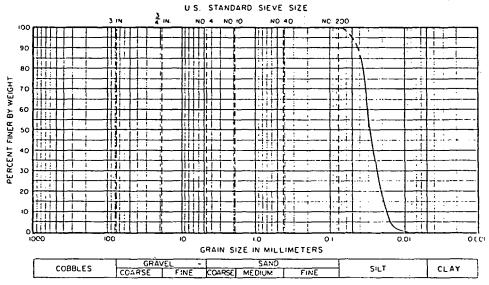
BORING G 0-31/2'

LIGHT GRAY SILT (GYPSUM)

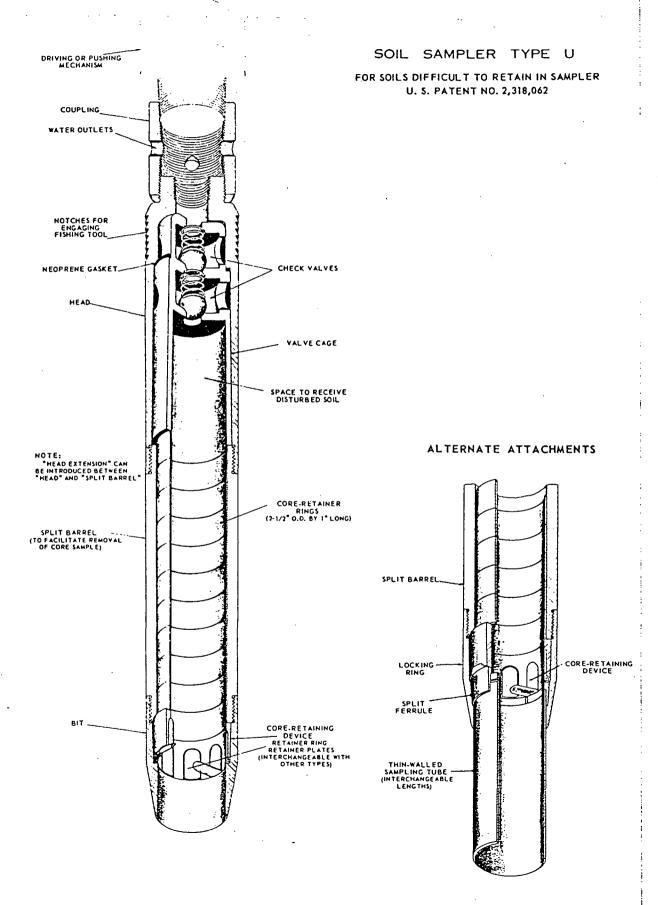


BORING H 0-31/2'

LIGHT GRAY SILT (GYPSUM) --



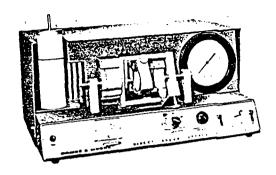
NOTE: DASHED PORTION OF CURVE REPRESENTS ESTIMATED VALUE. PARTICLE - SIZE DISTRIBUTION



METHOD OF PERFORMING DIRECT SHEAR AND FRICTION TESTS

DIRECT SHEAR TESTS ARE PERFORMED TO DETERMINE THE SHEARING STRENGTHS OF SOILS. FRICTION TESTS ARE PERFORMED TO DETERMINE THE FRICTIONAL RESISTANCES BETWEEN SOILS AND VARIOUS OTHER MATERIALS SUCH AS WOOD, STEEL, OR CONCRETE. THE TESTS ARE PERFORMED IN THE LABORATORY TO SIMULATE ANTICIPATED FIELD CONDITIONS.

EACH SAMPLE IS TESTED WITHIN THREE BRASS RINGS,
TWO AND ONE-HALF INCHES IN DIAMETER AND ONE INCH
IN LENGTH, UNDISTURBED SAMPLES OF IN-PLACE SOILS
ARE TESTED IN RINGS TAKEN FROM THE SAMPLING



DIRECT SHEAR TESTING & RECORDING APPARATUS

DEVICE IN WHICH THE SAMPLES WERE OBTAINED. LOOSE SAMPLES OF SOILS TO BE USED IN CONSTRUCTING EARTH FILLS ARE COMPACTED IN RINGS TO PREDETERMINED CONDITIONS AND TESTED.

DIRECT SHEAR TESTS

A THREE-INCH LENGTH OF THE SAMPLE IS TESTED IN DIRECT DOUBLE SHEAR. A CONSTANT PRESSURE, APPROPRIATE TO THE CONDITIONS OF THE PROBLEM FOR WHICH THE TEST IS BEING PERFORMED, IS APPLIED NORMAL TO THE ENDS OF THE SAMPLE THROUGH POROUS STONES. A SHEARING FAILURE OF THE SAMPLE IS CAUSED BY MOVING THE CENTER RING IN A DIRECTION PERPENDICULAR TO THE AXIS OF THE SAMPLE. TRANSVERSE MOVEMENT OF THE OUTER RINGS IS PREVENTED.

THE SHEARING FAILURE MAY BE ACCOMPLISHED BY APPLYING TO THE CENTER RING EITHER A CONSTANT RATE OF LOAD, A CONSTANT RATE OF DEFLECTION, OR INCREMENTS OF LOAD OR DEFLECTION. IN EACH CASE, THE SHEARING LOAD AND THE DEFLECTIONS IN BOTH THE AXIAL AND TRANSVERSE DIRECTIONS ARE RECORDED AND PLOTTED. THE SHEARING STRENGTH OF THE SOIL IS DETERMINED FROM THE RESULTING LOAD-DEFLECTION CURVES.

FRICTION TESTS

IN ORDER TO DETERMINE THE FRICTIONAL RESISTANCE BETWEEN SOIL AND THE SURFACES OF VARIOUS MATERIALS, THE CENTER RING OF SOIL IN THE DIRECT SHEAR TEST IS REPLACED BY A DISK OF THE MATERIAL TO BE TESTED. THE TEST IS THEN PERFORMED IN THE SAME MANNER AS THE DIRECT SHEAR TEST BY FORCING THE DISK OF MATERIAL FROM THE SOIL SURFACES.

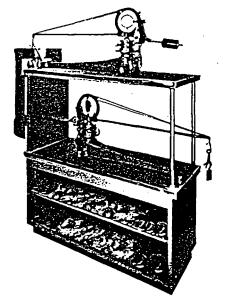
METHOD OF PERFORMING CONSOLIDATION TESTS

Consolidation tests are performed to evaluate the volume changes of soils subjected to increased loads. Time-consolidation and pressure-consolidation curves may be plotted from the data obtained in the tests. Engineering analyses based on these curves permit estimates to be made of the probable magnitude and rate of settlement of the tested soils under applied loads.

Each sample is tested within a brass ring two and one-half inches in

diameter and one inch in length. Undisturbed samples of in-place soils are tested in rings taken from the sampling tool in which the samples were obtained. Loose samples of soils to be used in constructing earth fills are compacted in rings to predetermined conditions and tested.

In testing, the sample is rigidly confined laterally by the brass ring. Axial loads are transmitted to the ends of the sample by porous disks. The disks allow



CONSOLIDATION MACHINES

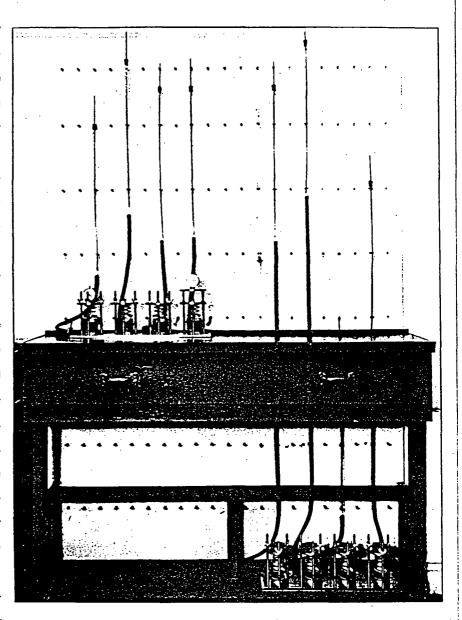
drainage of the loaded sample. The axial compression or expansion of the sample is measured by a micrometer dial indicator at appropriate time intervals after each load increment is applied. Each load is ordinarily twice the preceding load. The increments are selected to obtain consolidation data representing the field loading conditions for which the test is being performed. Each load increment is allowed to act over an interval of time dependent on the type and extent of the soil in the field.

Soils saturated in the field are tested submerged in water. The effect of increased moisture content on partially saturated soils is determined by adding water to the sample during the test.

METHOD OF PERFORMING PERCOLATION TESTS

The quantity and the velocity of flow of water which will escape through an earth structure or percolate through soil are dependent upon the permeability of the earth structure or soil. The permeability of soil has often been calculated by empirical formulas but is best determined by laboratory tests, especially in the case of compacted soils.

A one-inch length of the core sample is sealed in the percolation apparatus, placed under a confining load, or surcharge pressure, and subjected to the pressure of a known head of water. The percolation rate is computed from the measurements of the volume of water which flows through the sample in a series of time intervals. These rates are usually expressed as the velocity of flow in feet per year under a hydraulic gradient of one and at



APPARATUS FOR PERFORMING PERCOLATIONS TESTS

Shows tests in progress on eight samples simultaneously.

a temperature of 20 degrees Centigrade. The rate so expressed may be adjusted for any set of conditions involving the same soil by employing established physical laws. Generally, the percolation rate varies over a wide range at the beginning of the test and gradually approaches equilibrium as the test progresses.

During the performance of the test, continuous readings of the deflection of the sample are taken by means of micrometer dial gauges. The amount of compression or expansion, expressed as a percentage of the original length of the sample, is a valuable indication of the compression of the soil which will occur under the action of load or the expansion of the soil as saturation takes place.

O

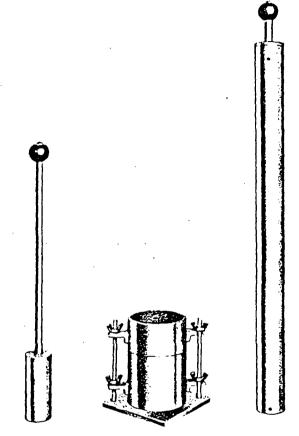
METHOD OF PERFORMING COMPACTION TESTS (STANDARD AND MODIFIED A.A.S.H.O. METHODS)

IT HAS BEEN ESTABLISHED THAT WHEN COMPACTING EFFORT IS HELD CONSTANT, THE DENSITY OF A ROLLED EARTH FILL INCREASES WITH ADDED MOISTURE UNTIL A MAXIMUM DRY DENSITY IS OBTAINED AT A MOISTURE CONTENT TERMED THE "OPTIMUM MOISTURE CON-TENT." AFTER WHICH THE DRY DENSITY DECREASES. THE COM-PACTION CURVE SHOWING THE RE-LATIONSHIP BETWEEN DENSITY AND MOISTURE CONTENT FOR A SPECIFIC COMPACTING EFFORT IS DETER-MINED BY EXPERIMENTAL METHODS. TWO COMMONLY USED METHODS ARE DESCRIBED IN THE FOLLOWING PARAGRAPHS.

FOR THE "STANDARD A.A.S.H.O."

(A.S.T.M. D698-58T & A.A.S.H.O.

T99-57) METHOD OF COMPACTION A
PORTION OF THE SOIL SAMPLE
PASSING THE NO. 4 SIEVE IS COMPACTED AT A SPECIFIC MOISTURE
CONTENT IN THREE EQUAL LAYERS
IN A STANDARD COMPACTION CYLINDER HAVING A VOLUME OF 1/30
CUBIC FOOT, USING TWENTY-FIVE
12-INCH BLOWS OF A STANDARD 5-1/2
POUND RAMMER TO COMPACT EACH
LAYER.



SOME APPARATUS FOR PERFORMING COMPACTION TESTS Shows, from left to right, 5-1/2 pound rammer (sleeve controlling 12" height of drop removed), 1/30 cubic-foot cylinder with removable collar and base plate, and 10 pound rammer within sleeve.

IN THE "MODIFIED A.A.S.H.O." (A.S.T.M. D-1557-58T & A.A.S.H.O. T 180-57) METHOD OF COMPACTION A PORTION OF THE SOIL SAMPLE PASSING THE NO. 4 SIEVE IS COMPACTED AT A SPECIFIC MOISTURE CONTENT IN FIVE EQUAL LAYERS IN A STANDARD COMPACTION CYLINDER HAVING A VOLUME OF 1/30 CUBIC FOOT, USING TWENTY-FIVE 18-INCH BLOWS OF A 10-POUND RAMMER TO COMPACT EACH LAYER. SEVERAL VARIATIONS OF THESE COMPACTION TESTING METHODS ARE OFTEN USED AND THESE ARE DESCRIBED IN A.A.S.H.O. & A.S.T.M. SPECIFICATIONS.

FOR BOTH METHODS, THE WET DENSITY OF THE COMPACTED SAMPLE IS DETERMINED BY WEIGHING THE KNOWN VOLUME OF SOIL; THE MOISTURE CONTENT, BY MEASURING THE LOSS OF WEIGHT OF A PORTION OF THE SAMPLE WHEN OVEN DRIED; AND THE DRY DENSITY, BY COMPUTING IT FROM THE WET DENSITY AND MOISTURE CONTENT. A SERIES OF SUCH COMPACTIONS IS PERFORMED AT INCREASING MOISTURE CONTENTS UNTIL A SUFFICIENT NUMBER OF POINTS DEFINING THE MOISTUREDENSITY RELATIONSHIP HAVE BEEN OBTAINED TO PERMIT THE PLOTTING OF THE COMPACTION CURVE. THE MAXIMUM DRY DENSITY AND OPTIMUM MOISTURE CONTENT FOR THE PARTICULAR COMPACTING EFFORT ARE DETERMINED FROM THE COMPACTION CURVE.

APPENDIX B

HISTORICAL SKETCH OF GYPSUM STORAGE POND

(Submitted by the J. R. Simplot Company)

1953 and 1954

An old gravel pit approximately 30 feet deep was divided into two equal sections. Gypsum was placed first in one section and then the other. In both cases, it entered the ponds at their southwest corners. During these early days, the plant production was such that the two ponds were never completely filled until 1955.

1955

The same two ponds as mentioned in the above paragraph were used alternately. When the ponds were nearly full, one pond was used while the other pond was allowed to set and dry. The dry pond was then excavated to approximately the bottom of the original gravel pit. When the pond was excavated, the gypsum would be diverted into it and the second pond would be allowed to dry and be excavated. The gypsum was allowed to enter both ponds near their southwest corners.

1956

The same procedure was followed as that of 1955.

1957

The same procedure was followed during 1957 as was followed in 1955 with the exception that a more comprehensive method of excavating was used.

1958

Gypsum was deposited into the two ponds again from the southwest corner. A 10-foot dike was constructed on the west, north, and east sides of the gypsum pond from borrowed material. This would make the top of the dike have an elevation of approximately 113 feet.

1959

The gypsum pond was again operated as two ponds except that the dividing dike was opened so that the two ponds behaved as one. The gypsum entered the gypsum pond at the west side. A dike 9 feet high was built from borrowed material. The elevation at the top of the dike was approximately 122 feet.

1960

The gypsum pond was divided into two separate ponds and the gypsum entered these ponds from the west, north, and east perimeter, the object being to keep the water to the south against the foothills and away from the dike. The dike was raised approximately 8 feet with borrowed material. The elevation of the top of the dike was approximately 130 feet. In October of 1960, a failure occurred near the northeast corner of the dike. It was the general opinion that the cause of the failure was water flowing through a seam of gypsum, thus causing erosion of the dike.

1961

February of 1961 the phosphate rock calciner was put into operation. Gypsum entered the two gypsum ponds on the west, north, and east perimeter, again attempting to keep the water to the south against the foothills and away from the dike. The dike on the east end of the pond was raised to an elevation equal to the remainder of the pond and an extension to the pond was constructed on the southwest end of the pond. The main dike elevation remained at approximately 130 feet.

1962

Gypsum was discharged into the two ponds from the west, north, and east perimeter, again attempting to keep the water to the south against the foothills and away from the dike. The dike was raised approximately 10

 \mathbf{C}

feet with borrowed material. The elevation of the top of the dike was approximately 140 feet. In April of 1962, Dames & Moore, Consulting Soils Engineers, started an investigation of the gypsum pond dike.

APPENDIX C

SUGGESTED SPECIFICATIONS FOR PLACING EMBANKMENT FILLS

SCOPE OF WORK

The work under these specifications includes the furnishing of all labor, tools, materials and equipment necessary for the placing of embankment fills in accordance with the applicable plans and specifications.

FILL MATERIALS

Fill materials shall be obtained from sources as directed by the Engineer or Owner. The materials will consist of natural silty materials from adjacent foothills.

COMPACTED FILL REQUIREMENTS AND PLACEMENT OF FILL

All embankment fills should be compacted to a dry density equal to at least 85 per cent of the maximum density determined in accordance with the Modified A.A.S.H.O.* (A.S.T.M. D 1557-57T and A.A.S.H.O. T 180-57) Method of Compaction. This method is described on Page A-IV, Method of Performing Compaction Tests. The maximum density and optimum moisture content should be determined by the engineer on the basis of tests on the material to be used.

Compaction of fill layers in direct contact with soft gypsum will not be possible. To provide a working surface, the gypsum should be covered with approximately 18 inches of fill material before the beginning of compaction operations.

The fill soils should be placed in successive layers of a thickness that will result in a compacted layer approximately six to eight inches in thickness. If the soils are too dry, it will be necessary to add water in a manner that will permit uniform penetration into the soils. Cultivation or other methods may be required during the application of water in order

^{*}American Association of State Highway Officials

to obtain a uniform moisture distribution. If the soils are too wet, a drying period will be necessary. Each layer of soil shall be subjected to sufficient compactive effort to achieve the required density.

Compacting of the fill materials by ponding, flooding, or jetting will not be permitted. Fill material should not be placed in water.

SOILS ENGINEER

The services of an inspecting engineer will be supplied by the Owner. The Engineer will be the respresentative of the Owner and shall have the responsibility to determine whether the filling operations are performed in accordance with the specifications.*

COMPACTION EQUIPMENT

The choice of compaction equipment is left to the discretion of the Contractor; however, the equipment used must be adequate for achieving the specified densities. It is anticipated that the use of smooth-wheeled rubber-tired compaction equipment will work well for the type of soils to be placed.

ACCEPTANCE OF FILL

The Engineer shall be responsible for the acceptance of the fill material used by the Contractor. The Contractor should not proceed with the filling operations until approval has been obtained.

Adequacy of compaction shall be determined by the Engineer on the basis of in-place density determinations that are conducted while the fill is being placed. The results of these tests shall be the basis on which the satisfactory completion of the work is judged.

^{*}If desired, Dames & Moore can instruct a member of the Simplot staff in procedures appropriate to field checking.

RECOMMENDED PRESENT POND CONTROL PROGRAM TAILINGS POND DEVELOPMENT

SIMPLOT PLANT POCATELLO, IDAHO

FOR THE J. R. SIMPLOT COMPANY

PRIOR EMBANKMENT CONTROL

The tailings pond has been developed in an area that at one time served as a gravel pit.

The perimeter embankment is constructed of materials borrowed from the hillside above the pond. A current borrow area is shown on the left of Photo 3 on Plate 4.

A typical cross section showing evolution in embankment development appears on Plate 6, Typical Cross Section. The plate was developed in conjunction with our 1962 studies. Prior to 1962, the embankment had developed to Elevation 140 at the perimeter configuration shown on Plate 6.

On the basis of soil studies by Dames & Moore in 1962, recommendations were advanced to flatten the upper portion of the slope to 3 to 1 and to thereafter continue at that slope. To control the surface of ponded water, the recommendation was made to maintain the edge of water ponds at least 150 feet from the inside edge of the perimeter embankment. Effective control of ponded water by this criterion requires sufficient permeability in the gravel below the gypsum to permit water reaching the gravel through the gypsum deposit to drain from the pond area. Gravel normally provides permeability characteristics that are appreciably in excess of this design requirement.

In the meantime, the embankment has been increased in height. The recommendations have been substantially followed.

CURRENT PROBLEMS

EMBANKMENT FAILURE:

On April 29, 1963, soil displacement at the northwest corner of the pond was noted by plant personnel. Shortly thereafter, the displaced section was examined more fully and causes evaluated by a representative from Dames & Moore.

grades, tailings positions of ponds can be maintained at desired locations.

Objectives of "B" Water Control. If the discharge spigot is maintained at a given location for a sufficient length of time, a ground water mound builds up below the spigot. If the mound is not permitted to dissipate, the mound can be damaging to the embankment. Essentially, our studies indicated the need for control of such mounds.

From evaluation of permeability data developed from previous studies, the ground water pattern below a discharge spigot is expected to advance in the manner shown on Plate 11A, Ground Water Section After One Day of Discharge, and Plate 11B, Ground Water Section After 15 Days of Discharge. In general, rate of the advance of the ground water downward would be on the order of one to two feet per day.* After the level of "A" water is reached, the mound flows into the "A" water system. After the spigot source is cut off, the mound gradually lowers to the level of "A" water. The period of time required for dissipation would be approximately twice the period required for the ground water advance.

To avoid build-up of ground water mound, it is our recommendation that:

- The period of application at any given spigot point be no longer than 15 days in order to prevent excess build-up of the ground water mound.
- The period of absence of discharge from a given location be not less than 30 days in order to permit the ground water mound to dissipate.
- The spacing between points of successive applications of spigots should be sufficient to prevent overlap of mounds.

^{*}This rate reflects variations in measured permeability rates of samples of the gypsum.

If the below-pond gravel in functioning as anticipated, the equilibrium level will be below Elevation 105. If the equilibrium level is above Elevation 105, further methods of ground water control will be required.

As data are developed for the first well, observations should be started on successive wells as soon as they are completed. Outside of the failure zone, the observation should be directed to obtaining data on the rate of rise of ground water at a particular observation location in relation to the position of a spigot in that immediate vicinity. Similarly, the rate of lowering after removal of the spigot should also be observed.

Control heights for ground water at locations other than the present failure zone should correspond with a position not higher than 15 feet above the toe of the slope on the downgrade portion of the embankment, or above an angle of eight degrees with the horizontal, whichever results in the lowest elevation.

DRAINAGE CAPACITY:

As long as the drainage capacity of the gravel below the gypsum deposit remains in excess of the drainage capacity of the gypsum, seepage through the gypsum will be in direct proportion to the pond area covered by water. For the conditions shown on Plate 5, the total water area would be considered as the A' and A'' ponds plus the minor ponds B', B'' and B''', plus the area covered by the streams between the ponds. When the total area thus covered exceeds the shaded area shown in the center of Plate 5, all of the 900 gallons per minute will have been lost through the pond surface. Decanting reduces the size of ponded areas that would otherwise develop. Neglecting rainfall and evaporation, all water entering the pond that is not decanted, drains through the bottom of the pond. Currently, decanted water is drained into the Portneuf River.

at the time need is established.

LONG-RANGE PLANNING

GENERAL:

As the pond increases in height, the "A" water ponds will cover areas that are not underlain by gravel, but which are underlain by silty soils that are less permeable than the gypsum. Accordingly, ground water from the "A" ponds will follow the surface of the silty soils to drain into the present pond area. That condition is now rapidly developing as the A' and A'' ponds are forced upgrade by the deposition process.

These trends in effect place free water ponds against natural gulley embankments that were not initially developed by natural processes to serve as dams to retain water. The effectiveness of such natural embankments in retaining water without failure will be dependent to a large degree by ground configurations and soil profiles at pond locations. Because of these considerations, details of long-range planning will be influenced not only by the current working criteria for pond development, but also by the specific terrain features on and near the area to be covered by tailings in the foreseeable future. In view of these considerations, the five-step program as set forth on Plate 2 has been developed for long-range planning.

Essentially, as soon as control of the present pond has been accomplished, topographic data should be developed for the area to be covered by the pond in the foreseeable future. All drainage channels immediately adjoining the pond area should be mapped. A contour interval not greater than five feet is recommended. After a tentative layout has been made, a review by Dames & Moore is recommended to detect any adjustments appropriate to conditions resulting from specific terrain conditions.

REPORT OF PROJECT PLANNING

PROPOSED TAILINGS POND (TP-K 2.1) POCATELLO, IDAHO

FOR THE J. R. SIMPLOT COMPANY

The samples were tested at a surcharge pressure (pressure applied normal to the ends of the sample) corresponding with the approximate weight of overburden existing at the time of sampling. Selected samples were also tested at an increased surcharge pressure to determine the angle of internal friction of the soils.

The samples were tested at field moisture content. Selected samples were also tested at an increased moisture content corresponding to saturated conditions.

A load-deflection curve was plotted for each test and the shearing strength determined from this curve.

The results of the shear tests, together with the associated moisture and density determinations are presented on the left of the boring logs in a manner described on the Key to Test Data on Plate A-2. The data are summarized on the lower portion of Plate A-3, Summary of Test Data, In-Place Soils.

CONSOLIDATION TESTS:

Consolidation tests were performed on selected samples to provide data for determining the amount and rate of settlement at this site. These tests were conducted in accordance with the Method of Performing Consolidation Tests described on Page A-III. The results obtained are presented on the upper portion of Plate A-3.

PERCOLATION TESTS:

To determine the rate of percolation of water through the in-place soils, percolation tests were performed on selected undisturbed samples of the in-place soils. The tests were performed in accordance with the procedure outlined on Page A-IV, Method of Performing Percolation Tests.

Percolation Tests. To obtain and evaluate data regarding the imperviousness of the fine-grained soils, percolation tests were performed in the laboratory on prepared cores of each type of soil. The cores were prepared by compacting the sample to 85, 90 and 95 percent of the maximum density determined by the compaction method outlined above. Percolation tests were performed in accordance with the procedure outlined on Page A-IV in Appendix A. The results of the tests are tabulated below. The data are expressed in terms of surface drawdown in feet per year under a hydraulic gradient of one for a temperature of 20 degrees centigrade.

| Soil Type | Percent Compaction | Coefficient of Permeability in Feet Per Year (K) |
|------------|-----------------------|--|
| Sandy Loam | 85 | 27.8 |
| Sandy Loam | 90 | 20.3 |
| Sandy Loam | . 95 | 4.3 |
| Silt | 85 | 33.4 |
| Silt | 90 | 28.5 |
| Silt | 95 | 5.4 |

Shear Tests. To provide data to be used in determining the stability of embankments, direct shear tests were performed on compacted cores of each type of soil. The cores were compacted to 90 percent of the maximum density previously described. Samples were tested at both optimum and saturated moisture conditions. To determine the internal angle of friction of the compacted soils, shear tests were performed at varying surcharges. The tests were performed in accordance with the Method of Performing Direct Shear and Friction Tests described on Page A-II of Appendix A.

CONTRACTOR BURNISHED

The results of the percolation tests on the in-place soils are tabulated below:

| Test Pit Number | Depth in Feet | Soil Type | Permeability Rate in Feet Per Year (K) |
|--------------------|------------------|-----------|--|
| 2 | 13½ | Silt | 163 |
| 6 | 2 | Silt | 6 |
| 10 | 2½ | Silt | 87 |
| 11 | 7 | Silt | 218 |
| 12 | 4 | Silt | 158 |
| 17 | 3 | Silt | 191 |
| 18 | 5 | Silt | 123 |
| 19 | 4 | Silt | 208 |

The data are presented in terms of surface drawdown in feet per , year under a hydraulic gradient of one at a temperature of 20 degrees centigrade.

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The following Plates are attached and complete this Appendix:

Plate A-1A - Log of Borings (Boring 1)

Plate A-1B - Log of Borings (Borings 2 and 3)

Plate A-1C - Log of Borings (Borings 4 and 5)

Plate A-1D - Log of Test Pits (Test Pits 1 through 4)

Plate A-1E - Log of Test Pits (Test Pits 5 through 8)

Plate A-1F - Log of Test Pits (Test Pits 9 through 12)

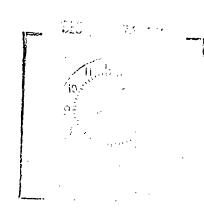
Plate A-1G - Log of Test Pits (Test Pits 13 through 16)

Plate A-lH - Log of Test Pits (Test Pits 17 through 20)

Plate A-2 - Soil Classification Chart and Key to Test Data

Plate A-3 - Summary of Test Data, In-Place Soils

REPORT OF INVESTIGATION AND DESIGN
PROPOSED EARTHFILL DIKES,
TAILINGS POND (TP-K2.1) EXPANSION
NEAR POCATELLO, IDAHO
FOR J. R. SIMPLOT COMPANY



DAMES & MOORE JOB NO. 4048-020-06

AST ABUTMENT CUTOFF - EAST DIKE:

Because of the fractured condition of the volcanic rock at the st abutment of the proposed East Dike, we recommend that a cutoff trench constructed to reduce seepage and to increase stability. The proposed utoff trench is shown in profile on Plate 4, Plan and Profile, East Dike, and is shown in section on Plate 6, Typical Section, Type 2. The maximum lepth of the cutoff trench will depend on observations during construction inspection. During our field investigation, a test pit was excavated in the abutment to a depth of approximately 8 feet, with a tire-mounted backhoe. Required depths for the cutoff trench should be achieved by ripping and dozing without the use of explosives.

MATERIAL TYPES AND BORROW AREAS:

The two dikes, East and West, will be constructed of two on-site borrow materials, Zone 1 and Zone 2 fill, as shown on Plate 6, Typical Sections.

Zone 1 fill will be the main impervious body of the two dikes and will also be compacted into the cutoff excavation of the East Dike.

Zone 1 material is a silt with trace fine sand. Grain size analyses curves of Zone 1 material are presented on Plate A-4A through A-4C. Compaction characteristics of the Zone 1 fill are shown on Plate A-5, Compaction Test Data. Borrow sources for Zone 1 fill are found throughout the site. Proposed Zone 1 borrow areas are shown on Plate 3, Plot Plan.

Zone 2 fill will serve as upstream and downstream slope erosion protection. A minimum of 12 inches of Zone 2 fill will be required for erosion protection. Zone 2 fill is a coarse gravel and cobble mixture of

are shown on Plates A-4A through A-4C, Gradation Curves.

Atterberg Limits. To further aid in classifying the soils and to assist in determining soil characteristics, the liquid limit, plastic limit and plastic indexes of two selected soil samples were measured. The tests were performed according to the ASTM designation: D423-66 and D424-59 methods. Samples from Test Pits 4 and 7 at a depth of 3.0 feet were tested. Both were found to be non-plastic.

Compaction Tests. Compaction tests were performed on representative samples of soils taken from test pits in proposed borrow areas. The purpose of performing the compaction tests were to define the compaction characteristics of these representative soils to be used in the construction of the proposed dikes. After compaction characteristics were determined, recompacted samples of these soils were made in our laboratory to specifications that will be required for the construction of the dikes. These recompacted samples were then subject to several tests as described in the following paragraphs. The procedure used in obtaining the compaction characteristics are described on Plate A-5, Method of Performing Compaction Tests. Results of the compaction tests are presented on Plate A-6,

Percolation Tests. Percolation tests were performed on representative undisturbed samples and on recompacted samples of soil which will be utilized in the construction of the proposed dikes. Tests were performed to provide data which were used in the calculations of surface runoff and the dissipation of surface runoff ponding. Tests were performed in accordance with the method described in Plate A-7, Method of

Performing Percolation Tests.

The degree of permeability is defined as follows: High - greater than 100,000 feet per year; medium - 100,000 to 1,000 feet per year; low - 1,000 to 10 feet per year; very low - 10 to 1 feet per year; and practically impermeable - less than .1 feet per year. Soils of high permeability are rarely encountered, and practically impervious soils, such as clays, are very common.

The results of the percolation tests are presented in tabular form below:

UNDISTURBED SAMPLES

| | | | Permeability | | |
|----------|---------------|-----------|---------------|--------------|--|
| Test Pit | | | Rate (K) in | Degree of | |
| Number | Depth in Feet | Soil Type | Feet Per Year | Permeability | |
| | | | | | |
| 2 | 5.5 | ML | 320 | Low | |
| _ | | | | | |
| 2 | 9.0 | ML | 133 | Low | |
| | | | • - • | _ | |
| 3 | 5.0 | ML | 214 | Low | |

RECOMPACTED SAMPLES

| Test Pit Number | Depth in Feet | Soil Type | Percent Compaction | Permeability Rate (K) in Feet Per Year | Degree of Permeability |
|--------------------|---------------|-----------|-----------------------|--|---------------------------|
| -3 | 3.0 | ML | 90 | 8.5 | Very Low |
| 3 | 3.0 | ML | 89 | 4.7 | Very Low |
| 5 . | 3.0 | ML | 90 | 21.7 | Very Low |
| 5 | 3.0 | ML | 89 | 31.0 | Very Low |

Consolidation Tests. To determine the amount of potential settlement, expansion or classibility of the in situ soils at the site and the soils to be used in the construction of the proposed dikes, consolidation

Dames & Moore Salt Lake City, Utah

April 14, 1987

Job No. 04048-042-18

REPORT

LABORATORY INVESTIGATION
EXISTING GYPSUM TAILINGS IMPOUNDMENT FACILITY
POCATELLO, IDAHO

FOR

THE J. R. SIMPLOT COMPANY

Dames & Moore



Exhibit #8



TABLE A-1

PERMEABILITY TEST RESULTS

| Material | Dry Density (pcf) | Permeability (cm/sec) |
|-------------------------------------|-------------------|--|
| Gypsum Slurry Calciner Clarifier | 56 63 | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ |
| Conda Mud | 89 | 2×10^{-7} |

As shown, the test results indicate a relatively wide range of permeability characteristics with the gypsum tailings being the most free draining.

TRIAXIAL COMPRESSION TESTS

A series of triaxial compression tests were performed on representative samples of the Conda Mud in accordance with the general procedures presented on Plate 3. This material was selected for the testing as a "worst case" condition based upon the results of the index tests. The series entailed testing on three individual samples. Each sample was formed as a slurry and consolidated under a different confining pressure (500, 1,000 and 2,000 pounds per square foot). A summary of the three tests is presented in tabular form on Plates 4A, 4B and 4C. The results of the tests are presented in graphical form on Plate 5. As shown, the test results indicate an "effective stress" and "total stress" angle of internal friction on the order of 36.5° and 22°, respectively.

CONSOLIDATION TESTS

A consolidation test was performed on reconstituted samples of the gypsum tailings and the Conda Mud. The tests were performed in general accordance with the procedures presented on Plate 6. In brief, the purpose of the tests was to evaluate the rate of consolidation for the two materials. This parameter could have a significant impact on the overall strength characteristics of a material particularly within a progressively expanding tailings impoundment. The rate is measured by the coefficient of consolidation, $c_{\rm V}$ which is presented for the two materials in tabular form on the following page.

J. R. Simplot Company April 14, 1987 Page -6-

imes & Moore



feet are projected. In the event that any greater depositional thickness develops, Dames & Moore should be notified so that appropriate recommendations can be provided, if necessary.

An additional concern associated with the gradational variation in the proposed matrials is the effect on the relative permeabilities. The results of our laboratory evaluation indicate that the permeability values vary by an excess of two orders of magnitude. This could significantly retard the vertical drainage characteristics of the impoundment and could cause the development of "perched" water levels within the embankment section. These perched levels could express themselves as seepage areas on the embankment face and could result in localized areas of instability.

In conclusion, the results of our analysis indicate that with the use of proper operational procedures the change of materials should not have a significant impact on the future operation of the facility. However, it is recommended that consideration be given to minimizing the degree of layering within the impoundment area. If possible the impact of the calciner clarifier underflow and the Conda Mud should be reduced by mixing with the gypsum tailings prior to deposition in the impoundment. If, in the future, areas of seepage are noted on the embankment face, Dames & Moore should be notified immediately so that appropriate remedial measures can be implemented.

SEISMIC STABILITY

It should be noted that the stability considerations discussed herein are based only on steady-state loading conditions. To date there has been no evaluation performed on the seismic stability of the impoundment. Recommendations for a proposed study were presented as Phase II in our proposal dated January 2, 1987.

DAMES & MOORE

SALT LAKE CITY, UTAH

JOB NO. 04048-046-31

JANUARY 25, 1988

INVESTIGATION AND STABILITY ANALYSIS
OF TAILINGS POND NO. 2
J. R. SIMPLOT COMPANY'S
POCATELLO, IDAHO OPERATIONS

FOR

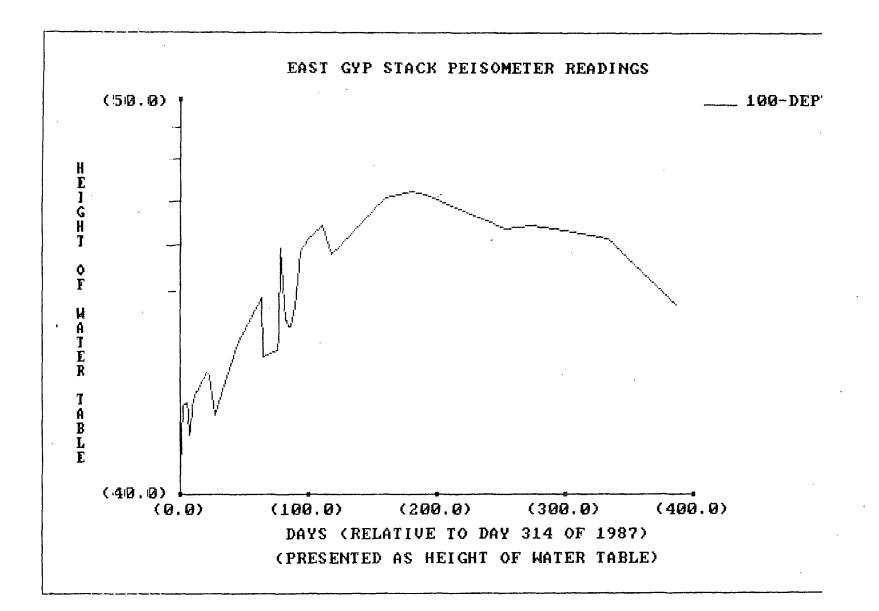
J. R. SIMPLOT COMPANY



Dames & Moore



Exhibit #9



J. R. Simplot Company January 25, 1988 Page -4-

GRAIN-SIZE ANALYSIS

Particle-size characteristics were evaluated through the performance of a hydrometer analysis on a representative sample of the uncalcined gypsum tailings. Analyses were performed in accordance with the procedures set forth under ASTM* D-422-83. A summary of these results are presented on Figure 6.

COMPACTION TEST

Due to the limited size of the sample available for testing a Harvard miniature compaction test was performed using a 40-lb spring and a 1-5/8-inch diameter compaction mold with materials being compacted in three lifts using 25 blows per layer. The results of this test are also presented on Figure 6.

PERMEABILITY TESTS

Coefficient of vertical hydraulic conductivity, i.e., vertical permeability was determined for a laboratory fabricated specimen of gypsum sedimented from a gypsum slurry. Materials were reslurried to a 40 percent density (weight basis) and sedimented in a column with bottom drainage. The specimen prepared for permeability testing had an initial dry unit weight of 52.9 pounds per cubic foot and a moisture content of 91.0 percent. Constant head coefficient of vertical hydraulic conductivity (permeability) determined for this specimen was 3.6×10^{-5} cm/sec.

CONSOLIDATION TEST

A consolidation test was performed on a fabricated laboratory sample sedimented from a 40 percent slurry of uncalcined gypsum tailings. Twenty-four hour values were selected for development of the strain-load relation-ship presented on Figure 7.

^{*}American Society for Testing and Materials

J. R. Simplot Company January 25, 1988 Page -6-

DISCUSSIONS AND CONCLUSIONS

MATERIAL HANDLING CHARACTERISTICS

Laboratory testing was performed to provide a basis to compare material handling characteristics of the uncalcined gypsum as those of gypsum deposited during previous facility operations. Laboratory data was extracted from previous Dames & Moore (references 1, 2 and 3) studies to form a basis for comparison. These data are summarized below in conjunction with data developed for uncalcined gypsum.

Summary of Laboratory Data

| Parameter | Calcined Gypsum* | Uncalcined Gypsum |
|--|---|----------------------------------|
| Specific Gravity - gm/c | 2.36 | 2.38 |
| Atterberg Limits LL - PI - | - non-plastic | - non-plastic |
| Grain Size P ₂₀₀ - % D ₅₀ - mm | 87 - 100 0.01 - 0.04 | 80 0.025 |
| Compaction Max - pcf Wopt - % | 79 - 88 ** 42 - 22 ** | 69 ** * 30 ** * |
| Permeability - cm/sec | $4.8 \times 10^{-4} - 1.9 \times 10^{-5}$ | 3.6×10^{-5} |
| Consolidation C _c - | 0.10 - 0.17 | 0.10 |

^{*} Combined data from 1965 and 1975 Dames & Moore Reports except as indicated otherwise.

^{**} Based on ASTM D-1557 (AASHTO T-180) procedures.

^{***} Based on Harvard Miniature Compaction Test.



J. R. Simplot Company January 25, 1988 Page -7-

The data presented in the previous table suggest little to no significant difference in mechanical behavioral properties between calcined and uncalcined gypsum tailings produced at the Simplot, Pocatello Plant. The compaction, compressibility and permeability data suggest that material handling characteristics of the proposed uncalcined gypsum tailings should be approximately the same as those of the calcined tailings impounded and used in the construction of TP-2 as it stands today.

STRENGTH CHARACTERISTICS

Strength characteristics of the uncalcined gypsum tailings were defined by a series of triaxial compression tests performed on laboratory fabricated test specimens sedimented from a 40 percent solids (weight basis) slurry. Results of these tests when viewed in comparison to those of calcined gypsum indicate strength properties as follows:

| | Uncalcined Gypsum | Calcined Gypsum |
|--|---------------------|---------------------|
| Total Friction Angle | 27 degrees | 20 degrees |
| Total Cohesion | 180 psf | 0 psf |
| Effective Friction Angle Effective Cohesion | 41 degrees O psf | 36 degrees 0 psf |

The strength parameters for calcined gypsum tailings were developed in previous Dames & Moore studies for J. R. Simplot. The values presented represent a conservative estimate based on a review of both triaxial and direct shear data developed for both Ponds 1 and 2.

These data, when compared, indicate that the strength properties of the uncalcined tailings tested exceed those of the calcined tails previously reported.

DAMES & MOORE SALT LAKE CITY, UTAH

JOB NO. 04048-046-31 \

MARCH 16, 1988

SUMMARY REPORT FOLLOW-UP INVESTIGATION AND LABORATORY TESTING GYPSUM TAILINGS POND NO. 2 J. R. SIMPLOT COMPANY'S POCATELLO OPERATIONS FOR J. R. SIMPLOT COMPANY

Dames & Moore



J. R. Simplot Company March 16, 1988 Page -4-

Results of partial grain-size determinations performed on representative samples of both UG and CG obtained from Test Pit 3 indicate 94.2 and 99.4 percent passing the No. 200 sieve, respectively.

Results of compaction tests performed on both UG and CG are presented below and graphically on Plate 1.

| | Maximum | Optimum |
|----------|-------------|----------|
| | Dry Density | Moisture |
| Material | <u>pcf</u> | % |
| · UG | 66.4 | 45.4 |
| CG | 69.6 | 49.5 |

SUMMARY AND CONCLUSIONS

The moisture content data presented above suggest only minor behavioral differences between the calcined and uncalcined gypsum. The data exhibit the minor degree of variation that would be expected in a naturally deposited homogeneous soil. Dry density data show similar variation and suggest only minor behavioral characteristic differences.

Compaction test results suggest only minor behavioral differences between the two types of gypsum tested. These data do indicate, however, that the deeper gypsum strata sampled are presently significantly wet of the optimum moisture for compaction based on the ASTM D698 Standard.

Based on the results of our field observations and subsequent laboratory testing conducted as part of this investigation, no data have been developed to suggest that the material handling properties of the uncalcined gypsum should be significantly different from those of calcined gypsum.



40-WEST LOUISE AVENUE

SALT LAKE CITY, UTAH 84115

PHONE 466-8761

DATE: 05/30/90

CERTIFICATE OF ANALYSIS

J.R. SIMPLOT COMPANY %L.WALKER-TECH SERV F.O. BOX 912 POCATELLO, ID 83201

90-004358

SAMPLE:

PIPELINE SLURRY SAMPLE RECEIVED 5-4-90 FOR E.P. TOXIC ANALYSIS USING PROCEDURE SW846 FOR LEACHABLE METALS STARTING AT 11 A.M. UNDER PO #87200-1040-0.

RESULTS

| 1-Arsenic as As ms/l EPA 7060 | .01 |
|-------------------------------|--------|
| 1-Barium as Ba me/l EFA 6010 | . 1.4 |
| 1-Cadmium as Od ms/l EPA 7130 | . 1. 1 |
| 1-Chromium as Cr mg/l EPA7190 | <.01 |
| 1-Lead as Pb ms/1 EPA 7420 | <.10 |
| 1-Mercury as He me/1 EPA7470 | <.001 |
| 1-Selenium as Se ms/l EPA7740 | <.01 |
| 1-Silver as As ma/l EPA 7760 | <.01 |
| 1-PH Final Units | 4.80 |
| 1-PH Initial Units | 8.00 |
| 3-React.as H28 ms/kgEPA9030 | <30.00 |
| S-React.as HCN ms/ks EPA9010 | <15.00 |
| Currosivity PH EPA 9040 | 7.40 |

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PAGE: 2

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RESULTS

PHONE 466-8761

lenitability EPA 1010

200

Liquid % E.P. Toxic SW 846

32.5

Solids % EP Toxic 8W 846

67.5

FORD CHEMICAL LABORATORY, INC.

FORD ANALYTICAL LABORATORIES

CERTIFICATE OF ANALYSIS

XC: N. 5014 K. Schiess

DATE: 06/12/90

J.R. SIMPLOT COMPANY %L.WALKER-TECH SERV P.O. BOX 912 POCATELLO, ID 83201

90-006376

SAMPLE:

CONDA PIPELINE LIQUOR SAMPLE RECEIVED 5-3-90 FOR ANALYSIS

STARTING AT 3 P.M. UNDER PO #87200-1040-0.

RESULTS

| Alkalinity,CaCO3 me/l SM4O3 | 176 |
|-----------------------------|--------|
| Aluminum as Al m9/1 SM 303C | .15 |
| Ammonia, NH3-N mg/l SM417G | 1.89 |
| Arsenic, As mg/l SM304 | .007 |
| Barium, Ba me/1 SM3O3C | .01 |
| Beryllium as Be ms/ISM303A | .002 |
| Bicarbonate,HCO3 mg/l SM4O3 | 215 |
| Boron as B ma/1 SM 404A | .29 |
| Cadmium, Cd mg/1 SM304 | .007 |
| Calcium, Ca mg/l SM303A | 101.02 |
| Carbonate as CO3 ms/1 SM4O3 | <.10 |
| Chloride, Cl mg/l SM407A | 24.0 |
| Chromium, Or me/l EPA218.1 | <.010 |

CHORDERESSEE CONTRACTOR CONTRACTO

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PAGE: 2

190-006376

RESULTS

| | ====== |
|-------------------------------|--------|
| Cobalt as Co mg/1 SM 303A | <.03 |
| Cond. umhos/cm EPA 120.1 | 842 |
| Copper, Cu ma/1 SM303A | <.01 |
| Cyanide Cn tot.mg/1 EPA 335.2 | <.010 |
| Fluoride, F me/1 EPA 340.2 | 6.30 |
| Hydroxide as OH ma/1 SM 403 | <.10 |
| Iron, Fe mg/l SM303A | .22 |
| Lead, Pb ms/l SM304 | <.002 |
| Lithium as Li ms/l | .02 |
| Magnesium, Mg mg/l SM303A | 16.52 |
| Manganese, Mn mg/1 SM303A | .18 |
| Mencuny, Halma/1 SM320A | .0002 |
| Molybdenum as Mo mg/1 SM303C | 1.59 |
| Nickel, Ni mg/l SM303A | <.03 |
| Nitrate, NO3-N mg/l SM418C | . 17 |
| Phosphorus Tot P mg/1 EPA 365 | 3.20 |
| Potassium, K me/l SM303A | 8.14 |

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CERTIFICATE OF ANALYSIS

PAGE:

90-006376

RESULTS

| Residual Sodium Carbonate | -2.874 |
|-------------------------------|--------|
| Selenium, Se me/l SM304 | .004 |
| Silica SIO2 (DIS) mg/l SM425A | 33.28 |
| Silver, As ms/l SM304 | <.010 |
| Sodium Absorption Ratio | 1.511 |
| Sodium, Na me/i SM303A | 62.13 |
| Sulfate, SO4 mg/1 EPA 375.2 | 253 |
| Surfactants PPm SM512B | <.10 |
| Tot.Dis.Solids mg/l EPA 160.1 | 804 |
| Vanadium as V mg/1 SM 3030 | . 29 |
| Zinc. Zn mg/l SM303A | .08 |
| PH Units EPA 150.1 | 7.30 |

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CERTIFICATE OF ANALYSIS

DATE: 06/12/90

90-006376-01

FORD CHEMICAL LABORATORIES

BALANCE SHEET FOR SAMPLE: (1) RESULTS

| CATIONS | l\em | mea/1 |
|-----------------------------------|---------------|-------|
| Calcium, Ca me/l SM303A | 101.020 | 5,041 |
| Maanesium, Ma ma/1 SM303A | 16.520 | 1.359 |
| Sodium, Na mg/l SM303A | 62.130 | 2.703 |
| Potassium, K m9/1 SM303A | 8.140 | .208 |
| Ammonia, NH3-N mg/l SM417G | 1.890 | .135 |
| ANIONS | m 9/ l | me4/l |
| Carbonate as CO3 mg/1 SM403 | .000 | .000 |
| Bicarbonate, HCO3 mg/1 SM4O3 | 215.000 | 3.526 |
| Sulfate, S04 mg/1 EPA 375.2 | 253.000 | 5.267 |
| Chloride, Cl mg/l SM407A | 24.000 | .677 |
| Nitrate, NOS-N mg/l SM418C | .170 | .003 |
| Hydroxide as OH mg/1 SM 403 | .000 | .000 |

BALANCE INFORMATION

CATIONS: 9.446 9.473 ANIONS: TOTAL: 18.919 DIFFERENCE: .027 •SIGMA: .001

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xc: File \$180,2.2



Ford Chemical LABORATORY, INC.

Bacteriological and Chemical Analysis

40 WEST LOUISE AVENUE SALT LAKE CITY, UTAH 84115

PHONE 466-8761

X1 X4 Norm JPC Orig to Kay Busen GTE.

DATE: 01/25/90

CERTIFICATE OF ANALYSIS

J.K. SIMPLOT COMPANY % NORM SELF P.O. BOX 910 POCATELLO, ID 83204

90-000757

SAMPLEX

COMPOSITE WATER SAMPLE FROM SEPT. - NOV. 1989 FROM SMOKY CONDA SLURRY FIRELINE RECEIVED 12-20-89 FOR ANALYSIS STARTING AT 11:30 A.M.

REBULTS

| en e | |
|--|------------|
| Alkalinit/stat00 mm/1 8M403 | 176 |
| Atominum as Al me/1 CM 1903C | . <u> </u> |
| Ammonias NHS-W mp/1 SP417G | . Ob |
| Arsenic, As ma/1 8M304 | <.002 |
| Barium, Ba ms// 1868080 | , OD |
| Berrllium as Be ma/15M303A | .040 |
| Bicarbonate, HCOS me/1 55405 | 239 |
| Buron as 5 mg/l 37 4044 | . 15 |
| Cadmium, Cd ms/) SM304 | <.001 |
| Calcium, Ca me/: SM303A | 100.00 |
| Carbonate as CUS me/1 8M403 | <.10 |
| Chloride, Cl me/l SM407A | 20.8 |
| Chromium, Cr me/l EPA218.1 | <.001 |

All reports are submitted as the confidental property of clients. Authorization for publication of our reports, conclusions, or, extracts from or regarding them, is reserved pending our written approval as a mutual protection to clients, the public and ourselves.



40 WEST LOUISE AVENUE
SALT LAKE CITY, UTAH 84115
PHONE 466-8761

PAGES

CERTIFICATE OF ANALYSIS

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RESUL 15

| | de producto es es tes solos se |
|-------------------------------|--|
| Cobatt as Co me/1 SM 303A | 0.03 |
| Cond. Umhos/cm EPA 120.1 | 1,050 |
| Copeer, Cu ma/1 SM303A | <.01 |
| Cranide On tot.me/1 EPA 335.2 | 4.00% |
| Fluoride, F mp// SM413B | 6.23 |
| Hydroxide as OH me/1 SM 403 | <.10 |
| Iron, Fe mg/t SM303A | the second of th |
| Lead, Fb me/1 8M304 | <.002 |
| Lithium as Li ms/1 | .03 |
| Maenesium, Me ms/l SM303A | 18.26 |
| Menseness, Mu ms/1 SM303A | .19 |
| Mercury, Ha ma/l SM320A | <.0002 |
| Molybdenum as Mo_me/1 SM303C | 1.80 |
| Nickel, Ni ms/l SM303A | .09 |
| Nitrate, NOS-N ms/1 SM4180 | . 20 |
| Phos. Total P04-P ms/1 SH4240 | W. 10 |
| Polassium, K m9/1 SM303A | 6.76 |

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PAGE: 3

CERTIFICATE OF ANALYSIS

90-003757

REBULTS

PHONE 466-8761

| The state of the s | |
|--|-----------|
| Residual Sodium Carbonate | -5,108 |
| Selenium, Se ma/l SM304 | .010 |
| Silica 5102 (DIS) ma// SM425A | 28.10 |
| Silver, As mg/l SM304 | <.005 |
| Sudium Absorption Natio | 1,207 |
| Sodiem, Ne mezl SMSOSA | 08.78 |
| Sulfate, SOA me/f EPA 375.2 |](.de.)_j |
| Surfactants prm SM5128 | 0.03 |
| Tot.Dis.Colids me// EPA 160.1 | 712 |
| Total-KJeldahl Nit.eem EPA 35 | .10 |
| Vanadium as V me/T SM 3030 | .36 |
| Zinc. Zn me/1 SMSOSA | .36 |
| PH Units ESA 420.1 | 7.50 |

FURD CHEMICAL LABORATORY, INC.



40 WEST LOUISE AVENUE SALT LAKE CITY, UTAH 84115 PHONE 466-8761

DATE: 01/25/90

CERTIFICATE OF ANALYSIS

90-003757-01

FURD CHEMICAL LABORATURIES

BALANCE SHEET FOR SAMPLE: (1) RESULTS

| ©CATIONS | :me/) | me≒71 |
|------------------------------|------------------|-------|
| Ualcioms Da me/1 SMSOCA | 196,000 | 7,485 |
| Maenesium, Me me/l 5M303A | 18.740 | 1.543 |
| Sodium, Na ms/1 SMSOSA | 35.900 | 2.566 |
| Polassium, K ms/l SM303A | 6.730 | .172 |
| ●Ammonia: RHS-N me/) SH4176 | .000 | .004 |
| ANIONS | s merzi | mes/1 |
| Carbonate as CCC ms/1 3M4CC | , (H) (J | ,000 |
| BicarbonatesHCOS ms/1 CM4CO | 209. 0 00 | 3.920 |
| ▲301fate: 504 me/1 EPA 375.2 | 540,000 | 7.079 |
| Chloride, Cl mez: SMADZA | 20.900 | .590 |
| Nitrate: NOS-W me/1 SM4180 | .200 | .003 |
| Hydroxide as OH me/1 SM 403 | ,000 | .000 |

PALANCE INFORMATION

CATIONS: 11.770
ANIONS: 11.092
TOTAL: 23.542
DIFFERENCE: 1.178
SIGMA: .007

FORD ANALYTICAL LABORATORIES

CERTIFICATE OF ANALYSIS

DATE: 01/18/91

J.R. SIMPLOT COMPANY % NORM SELF P.O. BOX 912 POCATELLO, ID 83204

91-003656

SAMPLE:

DRIER DISCHARGE COMPOSITE SAMPLE FROM SMOKEY CANYON RECEIVED 1-14-91 FOR LEACHABLE METALS USING TCLP PROCEDURE ON RUSH BASIS UNDER PO #10572-M.

RESULTS

- TCLP METALS

| Þ | 1-Arsenic as As mg/1 EPA 7060 | | OK 5.0 |
|---|-------------------------------|---------------|----------|
| | 1-Barium as Ba ms/1 EPA 6010 | .266 | OK 100.0 |
| | 1-Cadmium as Cd mg/l EPA 7130 | .506 | OK 1.0 |
|) | 1-Chromium as Cr ma/l EPA7190 | c. 010 | ok 5.0 |
| | 1-Lead as Pb ms/1 EPA 7420 | <.050 | OK 5.0 |
| | 1-Mercury as Hs ms/1 EPA7470 | <.001 | ox 0.2 |
| | 1-Selenium as Se ms/l EPA7740 | <.080 | |
| | 1-Silver as As mg/l EPA 7760 | C.007 | OK 5.0 |
| | i | • | |

FORD ANALYTICAL LABORATORIES

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MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. BIMPLET COMPANY

ADDRESS:

P. 0. BOX 712

POCATELLO, IDAHO 83264

COUNTY

FEMER.

RELEASE LOCATION:

DEM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/30/67

MATERIAL RELEASED:

93% H2904

QUANTITY RELEASED:

30 GALS (500 LES)

DID MATERIAL ENTER A WATERWAY:

N5

SOURCE OF RELEASE

400 SULFURIO ACID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/02/87

MATERIAL RELEASED:

BULFUR DIOXIDE

GUANTITY SELEASED:

UNKNOWN. >1 L3

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

SULFUR STOCKPILE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

400RE53:

P. 0. 30% 712

POCATELLO, IDAMO 53204

COUNTY

POWEE

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30 W

RELEASE DATE:

19/17/87

MATERIAL RELEASED:

SULFUR DIOXIDE

QUANTITY RELEASED:

200-300 POUNDS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

BOURCE OF RELEASE

SULFUR FIRE AT AR TRACKS NEAR SULFUR UNLOADING AREA BY \$4 H2504

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. A. SIMPLOT COMPANY

ADDRESS:

P. S. BOX 912

POCATELLO, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

XXM. IDA∺Ū

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/24/87

MATERIAL RELEASED:

93% SULFURIO

SUANTITY RELEASED:

200 GALLONS

DID MATERIAL ENTER A WATERWAY:

NG ·

SOURCE OF RELEASE

93% ACID TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/23/87

MATERIAL RELEASED:

73% H2804

QUANTITY RELEASED:

AFPROX 200 GALLONS

DID MATERIAL ENTER A WATERWAY:

NC

SOURCE OF RELEASE

PRODUCT TANK OVERFLOW AT #3 HZSD4

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY.

ADDRESE:

P. O. EOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

CON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/24/87

MATERIAL RELEASED:

93% H28804

QUANTITY RELEASED:

APPROX 55 BALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

BOURCE OF RELEASE

499 H2504

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

9. 8. BEX 912

POCATELLO. IDAMO 33204

COUNTY

FCMER

RELEASE LOCATION:

00%, 19AHS

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/04/67

MATERIAL RELEASED:

NIT DICKIDE & MIT OX

QUANTITY RELEASED:

20MUCR 91%

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

AMMO I SORAGE TANK (FEED TANK)

MINERALE & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 6. 80% 912

POCATELLO, IDAHO 83204

COUNTY

P(WEE

RELEASE LOCATION:

DON. IDA#O

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/22/87

MATERIAL RELEASED:

93% 82564

QUANTITY RELEASED:

120 5AL (1700 LBS)

DID MATERIAL ENTER A WATERWAY:

ŅŪ

SOURCE OF RELEASE

HE HESSE FRODUCT LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/31/67

MATERIAL RELEASED:

H2804 (38.41%)

QUANTITY RELEASED:

150 GALLONS

DID MATERIAL ENTER A WATERWAY:

Ni)

SOURCE OF RELEASE

73% DILUTION TANK @ #300 H2504

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/20/38

MATERIAL RELEASED:

SULFURIO ACID

QUANTITY RELEASED:

40 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

75% TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 712

FOCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

₹3/21/**39**

MATERIAL RELEASED:

NITEIC AGID

CHANTITY RELEASED:

150 GALLENS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

BOURCE OF RELEASE

STORAGE TANK NO. 2

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO. IDAHO 83204

COUNTY

POMER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/24/88

MATERIAL RELEASED:

H2504 .

GUANTITY RELEASED:

35 GALLONS

DID MATERIAL ENTER A WATERWAY:

M)

SOURCE OF RELEASE

HOLE WORM IN SIDE OF DUCT PIFFING; 98% DILUTION GOOT LEAKED AT FLANSED GUTLET PIPING ON

. MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

9. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM. IDAHO

RELEASE ADDRESS:

1:50 WEST HIGHWAY 30

RELEASE DATE:

03/29/98

MATERIAL RELEASED:

H2304

BUANTITY RELEASED:

50 SALLOMS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

MAIN ACTE COOLER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/13/88

MATERIAL RELEASED:

H2304

@DANTITY RELEASED:

50 SALLOWS

DID MATERIAL ENTER A WATERWAY:

MŪ.

SOURCE OF RELEASE

LEAK AT FLANGE ON PUMP DISCHARGE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SCUPCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. 20% 91Z

POCATELLO. IDAHO E3204

POWER

DON, IDAHO

1150 WEST HIGHWAY 30

04/19/88

0-52-0

40-50 EALLONS

ΝŪ

OVERFLOW RAILCAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

20N. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/19/98

MATERIAL RELEASED:

H2904

QUANTITY RELEASED:

ED EALLONE

DID MATERIAL ENTER A WATERWAY:

NJ.

FOURCE OF RELEASE

REMOVING GLD COILS 200 HZSS4

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/13/38

MATERIAL RELEASED:

SULFUR

QUANTITY RELEASED:

300 BALLONS

DID MATERIAL ENTER A WATERWAY: -

ΝŪ

SOURCE OF RELEASE

BULFUR TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83264

COUNTY

FLWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/13/66

MATERIAL RELEASED:

52% PHOS ACID

QUANTITY RELEASED:

500 GALLONS

DID MATERIAL ENTER A WATERWAY:

WD

SOURCE OF RELEASE

4" LIGUID FEED LINE

SPILL/RELEASE REPORT FORM

J R SIMPLOT - POCATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

9. 0. BOX 912

POCATELLO, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

94/20/88

MATERIAL RELEASED:

98% H2504

QUANTITY RELEASED:

270 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

EGURCE OF RELEASE

LEAK ON 98% TANK GUTLET FIFINE ON BOTTOM SIDE OF TANK.

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

CON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

94/20/88

MATERIAL RELEASED:

10-34-0

QUANTITY RELEASED:

50 + GALLONS

DID MATERIAL ENTER A MATERWAY:

Νū

SDURCE OF RELEASE

10-34-0 TRUCK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

64/27/88

MATERIAL RELEASED:

93% H2S04

GUANTITY RELEASED:

3 TO 4 BALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

SOURCE OF RELEASE

H2S04 PUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/27/38

MATERIAL RELEASED:

52% PHOSPHORIC ACID

QUANTITY RELEASED:

450 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

TRANFER LINE PHOS ACID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

PEWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/95/88

MATERIAL RELEASED:

9-52-0

QUANTITY RELEASED:

800 GALLONS

DID MATERIAL ENTER A WATERWAY:

N.5

BOURCE OF RELEASE

METER DID NOT CLOSE VALVE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83264

COUNTY

PEWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/12/88

MATERIAL RELEASED:

0-52-0 FEED

GUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

MO

SDURCE OF RELEASE

BROKEN FEED LINE 0-52-0 FEED TO LIQUID PLANT

SPILL/RELEASE REPORT FORM

J R SIMPLOT - POCATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 63204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/12/98

MATERIAL RELEASED:

93% 42904

PLANTITY RELEASED:

120 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

BROKEN LINE #3 #2384

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

YTAUCO

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/12/98

MATERIAL RELEASED:

ACID WASH WATER

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

Νū

SOURCE OF RELEASE

EAST FEED ACID LINE SPLIT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/13/98

MATERIAL RELEASED:

98% H2S64

QUANTITY RELEASED:

20 TO 30 SALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

SQUACE OF RELEASE

98% TANK DOWN LEG

SPILL/RELEASE REPORT FORM

J R SIMPLOT - POCATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. G. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

CON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/13/88

MATERIAL RELEASED:

52% P205

QUANTITY RELEASED:

60-80 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

SOURCE OF RELEASE

52% F205 LEAKING LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

FOCATELLO, IDAKO 83204

COUNTY

POWER

RELEASE LOCATION:

DOW, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE PATE:

05/16/86

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

20 GALLONS

DID MATERIAL ENTER A WATERNAY:

NO

SOURCE OF RELEASE

ACID PIPING LEAK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DUN, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/17/88

MATERIAL RELEASED:

93%.ACID

SUANTITY RELEASED:

35 CALLONS

DID MATERIAL ENTER A WATERWAY:

NO

EDURCE OF RELEASE

ACID PIPING LEAK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COLENTY

POWER

RELEASE LOCATION:

004, 10480

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/15/28

MATERIAL RELEASED:

42% F205

SUANTITY RELEASED:

IÐ GALLENS

DID MATERIAL ENTER A MATERWAY:

NO

SOURCE OF RELEASE

FLANGE IN LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. 0. 86% 912

FOCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

CON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/19/88

MATERIAL RELEASED:

NETRIC ACID

GEANTITY RELEASED:

2-3 GALLONE

DID MATERIAL ENTER A WATERWAY:

N

BOURCE OF RELEASE

ACTO LINE LEAK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

2. **0.** BOX 712

POCATELLO, IDAHO 83204

COUNTY

FOMER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/20/88

MATERIAL RELEASED:

0-52-0

SUANTITY RELEASED:

30 TO 50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

VALVE LEAKING

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

95/27/89

MATERIAL RELEASED:

73% H2S04

QUANTITY PELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NG

SOLACE OF RELEASE

93% TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 50% 912

POCATELLO, IDAHO 83204

COUNTY '

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 36

RELEASE DATE:

05/27/68

MATERIAL RELEASED:

52% ACID MUD

QUANTITY RELEASED:

75-100 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

BOURCE OF RELEASE

BOTTOM VALVE RAIL CAR AT CAR WASH

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/29/68

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

100 GAL (1506 LBS)

DID MATERIAL ENTER A WATERWAY:

NÜ

BOURCE OF RELEASE

93% H2SO4 DILUTION TANK AT 300 H2SO4

SPILL/RELEASE REPORT FORM

J R SIMPLOT - POCATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. F. SIMPLOT COMPANY

ADDREES:

P. 8. 80% 912

POCATELLO, IDAMO 83204

COUNTY

FORER

RELEASE LOCATION:

DON. EDAHO

RELEASE ADDRESS:

1156 WEST HIGHWAY 30

RELEASE DATE:

05/31/88

MATERIAL RELEASED:

93% H2S54

QUANTITY RELEASED:

SP 6AF1948

DID MATERIAL ENTER A WATERWAY:

NO

SOLACE OF RELEASE

SOULING TOWER OF DAY TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/31/88

MATERIAL RELEASED:

HFA

QUANTITY RELEASED:

1580 EALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

HEA TANK RAN OVER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

AGORESE:

9. 0. BOX 912

POCATELLO, IDAHO 83204

DOUNTY .

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 36

RELEASE DATE:

95/92/58

MATERIAL RELEASED:

52% P205

CUANTITY BELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

SOURCE OF RELEASE

LIGUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

400RESS:

COUNTY

ASLEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

GUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

F. O. BOX 912

POCATELLO, IDAHO 83204

POHER

DOM, IDAHO

1150 WEST HIGHWAY 30

 $\hat{v}_0/\hat{\phi}^4/2\hat{s}$

DIESEL FUEL

SA GALLONS

111

#33 SWITCH ENGINE FUEL TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO. IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

06/08/38

MATERIAL RELEASED:

98% HZS04

APANTITY RELEASED:

10 BALLONE

DID MATERIAL ENTER A WATERWAY:

A...

SOURCE OF RELEASE

FS% PEPING TO DRYING TOWER

MIMERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

P. J. 80% FIE

POCATELLO. IDAHO 30204

COLATY

POKER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1156 WEST HIGHWAY 36

RELEASE DATE:

96/11/88

MATERIAL RELEASED:

#3H28G4

QUANTITY RELEASED:

LESS THAN 10 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝO

SOURCE OF RELEASE

ECONOMIZER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAMO 83294

COUNTY

FOXER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

∂£/22/E8

MATERIAL RELEASED:

98% H2S04

GLAGGITY RELEASED:

4 CALLDNS

DID MATERIAL ENTER A WATERWAY:

ın

SOURCE OF RELEASE

DRYING TOWER OUTLET LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREBS:

P. O. BOX 713

POCATELLO. IDAMO 83204

COUNTY

POMER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

06/24/88

MATERIAL RELEASED:

98% HZS04

GUANTITY RELEASED:

65 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

GOURCE OF RELEASE

#4 H2SD4 78 TANK DRAIN LINE

MINERALS & CHEMICAL DIVISION

DOMPANY NAME:

J. R. SIMPLOT COMPANY

490AE58:

2. 0. 30% 912

FOCATELLO. IDAMO 83204

DUNTY

POWER

FELEASE LOCATION:

00%, 10AHJ

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

FELEASE DATE:

96724735

"ATERIAL ASLEASED:

98% H2804

LANTITY RELEASED:

5 6ALLONS

THE MATERIAL ENTER A WATERWAY:

Nū

BOURGE OF RELEASE

#4 H2504 H20 DILUTION LINE ON SIDE OF 95% TANK

MINEFALS & CHEMICAL DIVISION

COMPANY WAME:

J. P. SIMPLOT COMPANY

ADDRESS:

P. C. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOW, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

*06/26/8*8

MATERIAL RELEASED:

98% 42804

BUANTITY RELEASED:

150 6AL (2000 LBS)

DID MATERIAL ENTER A WATERWAY:

ΝŪ

BOURCE OF RELEASE

#4 40804

SPILL/RELEASE REPORT FORM

J R SIMPLOT - POCATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. G. 80% PIZ

PODATELLO, IDAFO 33204

COUNTY

FOWER 1

RELEASE LOCATION:

004. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

98736783

MATERIAL RELEASED:

0-70-0 DEFL0

GUANTITY RELEASED:

150 SALLENS

DID MATERIAL ENTER A WATERWAY:

NG

SOURCE OF RELEASE

HOLE IN CAR SATX 52157

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

PIPUER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

97/98/98[°]

MATERIAL RELEASED:

502

QUANTITY RELEASED:

100 TO 500 POUNDS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

FIRE AT A SULFUR FILE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

BELEAGE DATE:

MATERIAL RELEASED:

GUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SLURCE OF RELEASE

3. R. SIMPLOT COMPANY

P. J. BOX 912

POCATELLO, IDAMO 83204

FOWER

DOM. IDAHO

1150 WEST HIGHWAY 30

97/15/88

6-52-6

2 TO 5 GALLONS

ΝŪ

BROKEN LINE FROM 53 TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 20% 912

POCHTELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

904. EDAHO

RELEASE ADDRESE:

1150 WEST HIGHWAY 30

RELEABE DATE:

95/97/88

MATERIAL RELEASED:

0-50-0

SUARTITY RELEASED:

BO BACLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

BROKEN LIME

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. BIMPLOT COMPANY

ADDRESS:

P. 8. BOX 912

POCATELLO, IDAHO 83204.

COUNTY

FOWER

RELEASE LOCATION:

DEN, IDAHO

RELEASE ADDRESS:

1156 WEST HIGHWAY 30

RĘLEASE DATE:

03/04/88

MATERIAL RELEASED:

93% H2804

QUANTITY RELEASED:

40 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĢ

SQUACE OF RELEASE

DRAINING ACID TRUCK LOADING LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. E. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DEN, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

v8/15/98

MATERIAL RELEAGED:

98% H2S04 /

GUANTET/ RELEASED:

100 GALLONS

DID MATERIAL ENTER A WATERWAY:

Nū

SCURCE OF RELEASE

FIRING FROM ACID TOWERS TO PUMP TANK -

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADJAESS:

F. 8. 88% 912

POCATELLO, 104HO 832W4

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/18/**98**

MATERIAL RELEASED:

53% H2904

QUANTITY RELEASED:

15 SALLONS

DID MATERIAL ENTER A WATERWAY:

NŌ

SOURCE OF RELEASE

ACID RAILCAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 90/ 712

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 MEST HIGHWAY 30

RELEASE DATE:

98/19/38

MATERIAL RELEASED:

DE-FL0 0-70-0

QUANTITY SELEASED:

50 TO 60 GALLOXS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

9-70-0 TRANSFER LINE TO DILUTION TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 712

POCATELLO. IDAHO 83204

COUNTY

P3655

RELEASE LOCATION:

10A. 15AHS

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

08/15/EB

MATERIAL RELEASED:

93% 82**9**04

QUANTITY RELEASED:

100 SAL (1500 LSS)

DID MATERIAL ENTER A WATERWAY:

NO.

SCURCE OF RELEASE

93% TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/06/38

MATERIAL RELEASED:

0-70-0

ZLANTITY RELEASED:

10 SALLONS

DID MATERIAL ENTER A WATERWAY:

Nō

SOURCE OF RELEASE

BATX 17225 ACID CAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

P. 8. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FORES

RELEASE LOCATION:

DOM, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/07/88

MATERIAL RELEASED:

CHROMATE

QUANTITY RELEASED:

J SALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

CHROMATE STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

FUWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 HIGHWAY 30 W

RELEASE DATE:

09/13/88

MATERIAL RELEASED:

98% H2SG4

GUANTITY RELEASED:

2 EALLONS

DID MATERIAL ENTER A WATERWAY:

Νū

SOURCE OF RELEASE

THERMOCOUPLE LEAKED

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

- DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/15/88

MATERIAL RELEASED:

P205

QUANTITY RELEASED:

30 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

OLD UNUSED FIBERCAST LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 30% 712

POCATELLO, IDAMO B3204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

89/28/38

MATERIAL RELEASED:

HPA

JUANTITY RELEASED:

300 GALLONE

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

TANK RAM OVER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. EOX 912

POCATELLO. IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 36

RELEASE DATE:

10/06/89

MATERIAL RELEASED:

H2504

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

HZ504 FUMP SEAL

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 8. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

19/95/89

MATERIAL RELEASED:

98% HZS04

QUANTITY RELEASED:

10 BALLONS

DID MATERIAL ENTER A WATERWAY:

Nõ

SOURCE OF RELEASE

ABBURBING TOWER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 913

POCATELLO, IDAHO 83204

COUNTY

POMER

RELEASE LOCATION:

DON, IDAFO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/20/36

MATERIAL RELEASED:

NITRIC ALID

SUANTITY RELEASED:

5 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

#2 TANK OVERFLOW

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAMO 83204

PTMUGG

POWER

RELEASE LOCATION:

DCN, IDAHO

RELEASE ADDRESE:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/22/88

MATERIAL RELEASED:

93% 92804

SCANTITY RELEASED:

5.5 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

#3 H2304 PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 80% 912

POCATELLO, IDAHO 63204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/25/88

MATERIAL RELEASED:

93% H2304

QUANTITY RELEASED:

40 SALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

93% TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESE:

P. D. 30X 912

FOCATELLO, IDAHO 63204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/28/88

MATERIAL RELEASED:

SULFURIC ACID

QUANTITY RELEASED:

150 SALLONS AFPROX

DID MATERIAL ENTER A WATERWAY:

...

SOURCE OF RELEASE

TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

.P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/31/38

MATERIAL RELEASED:

98% H2**904**

QUANTITY RELEASED:

755 BALLONS

DID MATERIAL ENTER A WATERWAY:

邶

SOURCE OF RELEASE

OLD 100 H2804 SULFURIC FEED LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. 20% 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAMO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/05/85

MATERIAL RELEASED:

NITRIC ACID

QUANTITY RELEASED:

<50 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SCURCE OF RELEASE

NEWEST NITRIC ACID STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

COUNTY

ADDRESS:

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED: .

DID MATERIAL ENTER A WATERWAY:

BOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

POWER

DON, IDAHO

1150 WEST HIGHWAY 30

11/15/88

93% H2904

3 GALLONS

No.)

OH CONTROL TANK AT 200 C.T. NH3

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

POCATELLO, ICAHO

RELEASE ADDRESS:

UNION PACIFIC RAILYARD, BOWL #7, POCATELLO, IDAHO

RELEASE DATE:

11/21/85

MATERIAL RELEASED:

PHOSPHORIC ACID

GUANTITY RELEASED:

3000-4000 POUNDS

DID MATERIAL ENTER A WATERWAY:

ΝŌ

BOURCE OF RELEASE

LEAKING RAILCAR UTLX 13785

MINERALS & CHEMICAL DIVISION

COMPANY NAME: .

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

00N, 10AH0

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/28/38

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

150 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŌ

BOURCE OF RELEASE

#200 NH3 COOLING TOWER OH TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

POKER

RELEASE LOCATION:

DON, IDAHO

RÉLEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/29/88

MATERIAL RELEASED:

H2S04

QUANTITY RELEASED:

75 GALLONS

DID MATERIAL ENTER A WATERWAY:

Nű

SOURCE OF RELEASE

98% ACID COOLER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COÚNTY

POWER

RELEASE LOCATION:

DOM. IDAHE

RELEASE ADDRESS:

nami Inpe

1150 WEST HIGHWAY 30

RELEASE DATE:

12/01/88

MATERIAL RELEASED:

H2S04

QUANTITY RELEASED:

LESS THAM A QUART

DID MATERIAL ENTER A WATERWAY:

ΔÜ

BOURCE OF RELEASE .

NES PLANT H2504 LINE

MINERALS & CHEMICAL DIVISION

CONFANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

12/01/58

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

10 BALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

93% H2804 LINE TO MH3 PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY.

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/03/88

MATERIAL RELEASED:

93%

"@UANTITY RELEASED:

1 PINT

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

FILL LINE TO 200 NH3 C.T. pH TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 712

POCATELLO, IDAHO 83204

CGUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/12/58

MATERIAL RELEASED:

93% H2904

GLANTITY RELEASED:

20 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

EDURGE OF RELEASE

200 NH3 200 C.T. OH CONTROL ACID TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. 30% 912

POCATELLO, IDAHO 83204

COUNTY

POHER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/20/85

MATERIAL RELEASED:

NITRIC ACID 52%

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO -

BOURCE OF RELEASE

#2 NITRIC ACID STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FORER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/29/88

MATERIAL RELEASED:

SUPERPHOSPHORIC ACID

QUANTITY RELEASED:

15 SALLONS (245 LB)

DID MATERIAL ENTER A WATERWAY:

NO

SCURCE OF RELEASE

#3 LOADING STATION

MINERALS & CHEMICAL DIVISION .

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAMO 33204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

01/04/39

MATERIAL RELEASED:

H2364

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

VALVE OPEN ON TRUCK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

01/07/99

MATERIAL RELEASED:

93% H2604

GUANTITY RELEASED:

33 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

200 NH3 COOLING TOWER OH TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. 20% 912

POCATELLO, IDAHO 63204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

91/11/89

MATERIAL RELEASED:

WATER & P205

QUANTITY RELEASED:

400-800 POUNDS

DID MATERIAL ENTER A WATERWAY:

úΩ

SOUNCE OF RELEASE

#53 TANK PAD

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDAESS:

P. 0. BGX 712

POCATELLO, IDAHO 83204

COUNTY

POMER

RELEAGE LOCATION:

CON, IDAHO

RELEASE ADDRESS:

1150 MEST HIGHWAY 30

RELEASE DATE:

01/12/69

MATERIAL RELEASED:

H2504

QUARTETY RELEASED:

475 GALLONS

DID MATERIAL ENTER A WATERWAY:

NÜ

SOUPCE OF RELEASE

STORAGE TANK NO. 4

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. A. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 712

POCATELLO, IDAHO 83304

COUNTY

POWER

RELEASE LOCATION:

DON. IDAFO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

01/17/89

MATERIAL RELEASED:

93% H2S04

DUANTITY RELEASED:

20 BALLONS

DID MATERIAL ENTER A WATERWAY:

ΝO

EQUACE OF RELEASE

93% ACID FEED LINE TO BULFATE UNIT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

BELEASE DATE:

01/18/89

MATERIAL RELEASED:

PHOS ACID SPS, 1.342

GUANTITY RELEASED:

200 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

TRANFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. D. BOX 912 FOCATELLO. IDAHO 83204

COUNTY '

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

01/18/89

MATERIAL RELEASED:

H2SO4 AND WATER

QUANTITY RELEASED:

1180 POUNDS .

DID MATERIAL ENTER A WATERWAY:

NO

SCURCE OF RELEASE

H2904 FEED STATION

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREES:

P. 5. BOX 712

POCATELLO. IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

02/03/69

MATERIAL RELEASED:

H2504 93%

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

BOURCE OF RELEASE

73% SAMPLE LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. 200 912

POCATELLO, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

02/07/89

MATERIAL RELEASED:

52% 8205

QUANTITY RELEASED:

500 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

52% TO LIQUID PLANT FEED LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADERESS:

F. O. BOX 912

PCCATELLO. IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

BON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

02/10/29

MATERIAL RELEASED:

9-52-9

QUANTITY RELEASED:

25 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

DILUTION TANK AT LIQUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 63204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

02/10/39

MATERIAL RELEASED:

0-68-0

QUANTITY SELEAGED:

30 SALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

TRUCK LOADING LINE AT LIQUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

a. 6. BOX 912

POCATELLO, IDANO E3204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1156 WEST HIGHWAY 36

RELEASE DATE:

02/18/89

MATERIAL RELEASED:

52% P205

QUANTITY RELEASED:

500 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

DILUTION TANK OVERFLOWED

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

. P. O. BOX 712

POCATELLO, IDAHO 63204

COUNTY

POWER

RELEASE LOCATION:

DCM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/03/89

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

JO GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SCURCE OF RELEASE

COOLING TOWER OH CONTROL TANK FILL LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO B3204

POWER

DON. IDAHO

1150 WEST HIGHWAY 30

05/14/89

52% PHOS ACID /

150 GALLONS

NŪ

LIGUID FEED LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 63204

COUNTY

POHER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/15/99

MATERIAL RELEASED:

SULFURIC ACID

CUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

Nijī i

SOURCE OF RELEASE

3" SULFURIC TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

93/18/89

MATERIAL RELEASED:

98% H2804

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

SOURCE OF RELEASE

FINAL PUMP DISCHARGE LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. C. BOX 712

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/19/87

MATERIAL RELEASED:

93% H2SO4

QUANTITY RELEASED:

30 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

93% PUMP TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. U. 80X 912

1150 WEST HIGHWAY 30

POCATELLO, IDAHO 83264

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

RELEASE DATE:

03/17/89

MATERIAL RELEASED:

QUANTITY RELEASED:

93% H2604

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

MO

BOURCE OF RELEASE

93 PLANT PRODUCT LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESE:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/19/89

MATERIAL RELEASED:

93% H2904

QUANTITY RELEASED:

200 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

93 PUMP TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/20/89

MATERIAL RELEASED:

98% H2SO4

BUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

FINAL PUMP DISCHARGE LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

FOCATELLO, IDAHO 83204

COLINTY

FOWER

RELEASE LOCATION:

00N, 10AH0

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/20/99

MATERIAL RELEASED:

SULFURIC ACID

QUANTITY RELEASED:

40 GALLONS

DID MATERIAL ENTER A WATERWAY:

No.

SOURCE OF RELEASE

LEAK ON 3" L INE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

PUNER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/29/89

MATERIAL RELEASED:

HPA

QUANTITY RELEASED:

100 CALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

PAIL CAR FAN OVER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

r (NES

RELEASE LOCATION:

DON, IDAHE

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/03/69

MATERIAL RELEASED:

6-68-6

QUANTITY RELEASED:

4 CALLONS

DID MATERIAL ENTER A WATERWAY:

Ю.

SOURCE OF RELEASE

TRANSFER LINE AT LIQUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOHER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/21/89

MATERIAL RELEASED:

93% H2S04

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

7ANK

MINERALS & CHEMICAL DIVISION

COMPANY MAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/24/89

MATERIAL RELEASED:

37% H2S04

QUANTITY RELEASED:

40 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

OLD PIPING

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

POWER

DON, IDAHO

1150 WEST HISHWAY 30

04/24/89

6-52-0 PHGS ACID

75 SALLONS

NO

LOADING RAIL JAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SEMPLOT COMPANY

ADDRESS:

P. C. BEX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

PELEASE LOCATION:

DOM, IDAhO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

96/16/89

MATERIAL RELEASED:

H2504

QUANTITY RELEASED:

AFFROX 5 SALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

HZSG4 4 FIPINS

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

ABLEAGE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HISHWAY 30

RELEASE DATE:

96/27/99

MATERIAL RELEASED:

96% H2904

QUANTITY RELEASED:

20 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO .

SOURCE OF RELEASE

LINE BROKE APART (INACTIVE LINE)

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

FOCATELLO, IDAHO 63294

POWER

DON, IDAHO

1150 WEST HIGHWAY 30

05/25/59

AMMEGX

100 SALLONS

NO

OVERFLOWED THE PAD

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

8. 0. **30%** 712

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/28/**89**

MATERIAL RELEASED:

₽205

QUANTITY RELEASED:

50 SALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

SOURCE OF RELEASE

PRODUCT 4" LINE TO AP I FLANT TANKS

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

. J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 93204

COUNTY

FORER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

07/01/59

MATERIAL RELEASED:

98% H2S04 #300 H2S04

QUANTITY RELEASED:

100 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

SOURCE OF RELEASE

95% PUMP TANK (CONTAINED 98% H2504)

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

07/04/89

MATERIAL RELEASED:

98% H2S04

BLANTITY RELEASED:

3-5 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

EDURCE OF RELEASE

H2904 LINE TO NH3 COOLING TOWER OH TANK AND DEMINERALIZER SYSTEM

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. S. BOX 912

POCATELLS, IDAMO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

97/19/39

MATERIAL RELEASED:

P205 - 63%

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SCURCE OF RELEASE

0-70-0 TRANSFER LINE

MINERALS & CHEMICAL DIVISION

CONFANY NAME:

J. R. SIMPLOT COMPANY

ADERESE:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FORER

RELEASE LOCATION:

00M, 10AHC

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

07/31/69

MATERIAL RELEASED:

68% P205

QUANTITY RELEASED:

25 GALLONE

DID MATERIAL ENTER A WATERWAY:

157

SOURCE OF RELEASE

FILTER COOLER FUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. A. SIMPLOT COMPANY

ADGREES:

F. G. EGX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

98/95/39

MATERIAL RELEASED:

54% F205

QUANTITY RELEASED:

10 TG 25 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

DILUTION COOLER AT LIGUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

PCCATELLO, IDAHO 83204

COLINTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

0S/09/97

MATERIAL RELEASED:

SULFURIC ACID

GLANTITY RELEASED:

5 CALLONS

DID MATERIAL ENTER A WATERWAY:

Nō

SOURCE OF RELEASE

3" TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

SOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

98/12/89

MATERIAL RELEASED:

PHOS ACID

QUANTITY RELEASED:

APPROX 50 SALLONS

DID MATERIAL ENTER A WATERWAY:

Nū

SOURCE OF RELEASE

CAR WASH

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 KEST HIGHWAY 30

RELEASE DATE:

08/29/89

MATERIAL RELEASED:

68% P205

QUANTITY RELEASED:

10 + SALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

LIGUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 33264

COUNTY

FOMER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

07/01/97

MATERIAL RELEASED:

78% H2504

QUANTITY RELEASED:

: PINT

DID MATERIAL ENTER A WATERWAY:

NO

BOUAGE OF RELEASE

HOLE IN LINE

MINERALS & CHEMICAL DIVISION

JOMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. 0. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

PEMER

RELEASE LOCATION:

DOW, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

09/06/29

MATERIAL RELEASED:

PHOS ACID - 0-52-0

QUANTITY RELEASED:

APPROX 60 SALLONS

DID MATERIAL ENTER A WATERWAY:

NG

SOURCE OF RELEASE

9-52-0 LOADING LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POMER

RELEASE LOCATION:

DEM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/08/39

MATERIAL RELEASED:

BETZ 7114 POLYMER

QUANTITY RELEASED:

15 GALLONS

DID MATERIAL ENTER A WATERWAY:

MO

SOURCE OF RELEASE

TOTE TANK OVERFILLED

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 30% 912

FOCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/21/89

MATERIAL RELEASED:

16.4% P285

QUANTITY RELEASED:

2000-3000 BALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SCURCE OF RELEASE

#4 LSL STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. Q. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWES

RELEASE LOCATION:

00M, 18HAG

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/22/69

MATERIAL RELEASED:

H2S84 F3%

QUANTITY RELEASED:

LESS THAN 10 SALLOWS

DID MATERIAL ENTER A WATERWAY:

kO

SOURCE OF RELEASE

PIPING

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

J. R. SIMPLOT COMPANY

POCATELLO, IDAHO 83204

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

P. O. BOX 912

FOWER

DON, IDAHO

1150 WEST HIGHWAY 30

10/05/89

ML FROM CRYSTALLIZER

5000 GALLONS

MD

10" DRAIN LINE AT SULFATE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 30% 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

19/11/89

MATERIAL RELEAGED:

52% P205

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

...

SOURCE OF RELEASE

52 CAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

PESER

RELEASE LOCATION:

DON, IÓAHG

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

10/27/87

MATERIAL RELEASED:

NITRIC ACID - 55%

QUANTITY RELEASED:

20 GALLONS

DID MATERIAL ENTER A WATERWAY:

¥0

SOURCE OF RELEASE

#2 STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY WAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FLWEE

RELEASE LOCATION:

DON. IDAHE

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/11/89

MATERIAL RELEASED:

CHROMATE

SUGNITITY RELEASED:

AFFROX 3 GALLONE

DID MATERIAL ENTER A WATERWAY:

MΩ

BOURCE OF RELEASE

SUCTION LINE TO PUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 712

POCATELLO, IDAMO 83204

COUNTY

POWER

ABLEASE LOCATION:

00M, 194HO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/06/89

MATERIAL RELEASED:

. -0-70-0 PKOS

QUANTITY RELEASED:

Z5 SALLOAS

DID MATERIAL ENTER A WATERWAY:

NĒ

SCURCE OF RELEASE

BROKEN VALVE ON #5

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 85% 712

POSATELLO. 104HO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHÓ

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

12/11/69

MATERIAL RELEASED:

93% HZSG4

GUANTITY RELEASED:

LESS THAN 10 SALLONS

DID MATERIAL ENTER A WATERWAY:

NC

SOURCE OF RELEASE

ACID SUFFLY LINE TO MHS FLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

9. 0. 20% 912

POCATELLO, IDAHO 83264

COUNTY

FOWER

RELEASE LOCATION:

DOM, IDAHS

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/11/89

MATERIAL RELEASED:

54% NITRIC ACID

RLANTITY RELEASED:

2 BALLONS

DID MATERIAL ENTER A WATERWAY:

柳

SCURCE OF RELEASE

#2 ACTO STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMEANY

ADDRESS:

P. C. EOX 912

POCATELLO, IDAMG 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, SDAMO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/12/89

MATERIAL RELEASED:

0-70-0

QUANTITY RELEASED:

75-100 GALLONS -

DID MATERIAL ENTER A WATERWAY:

Kijī)

SOURCE OF RELEASE

#5 ¢-70-0 TA/#

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

⊃ÜMEK

RELEASE LOCATION:

DOM, ICAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/20/89

MATERIAL RELEASED:

SCRUBBER LIQUOR (73%

GCANTITY RELEASED:

20 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

1/2" SAMPLE LINE TO SH METER

MINERALS & CHEMICAL DIVISION

CONPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESE:

P. D. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1156 WEST HIGHWAY 30

RELEAGE DATE:

12/24/89

MATERIAL RELEASED:

98% H2S94

QUANTITY RELEASED:

1-2 GALLONS

DID MATERIAL ENTER A WATERWAY:

NĐ

SOURCE OF RELEASE

LEAK IN DRYING TOWER TEMPERATURE CONTROL AUTO VALVE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

POCATELLO, IDAMO 83204

COUNTY

FOWER

SELEASE LOCATION:

COM, EDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/25/99

MATERIAL RELEASED:

54% NITRIC ACID

QUANTITY RELEASED:

5-5 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

MATLACK TRUCK #39. TRAILER 3081, BILL OF LADING 6537

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAMO 83204

COUNTY

FOWER

RELEASE LOCATION:

OCN, IDHAD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

12/29/99

MATERIAL RELEASED:

524 MH63

QUANTITY RELEASED:

20 CALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

#2 ACID STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912

POCATELLO. IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

12/29/89

MATERIAL RELEASED:

78% H2904

ODANTITY RELEASED:

5 GALLONS

DID MATERIAL ENTER A MATERWAY:

NO

BOURCE OF RELEASE

OVERFLOW FUMFOUT TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREES:

P. J. BOX 912 POCATELLO, IDAHO 33204

COUNTY

FOMER

RELEASE LOCATION:

BON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/29/89

MATERIAL RELEASED:

H2S04

GUANTITY RELEASED:

ZA GALLONS

DID MATERIAL ENTER A WATERWAY:

ŅŪ

SOURCE OF RELEASE

93% TANK RAN OVER AT #4 H2804

SPILL/RELEASE REPORT FORM

J R BIMPLOT - PODATELLO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDAESS:

P. G. 56% 912

POCATELLO, IDAHO 85204

COUNTY

FOWER

RELEASE LOCATION:

DON, 10AH9

RELEASE ADDRESS:

1150 WEET HIGHWAY 30

RELEGEE DATE:

91/∂6/₹9

MATERIAL RELEASED:

₩:-32

QUANTITY RELEASED:

28,000-30.000 GALS

DID MATERIAL ENTER A WATERWAY:

MC.

SOUACE OF RELEASE

#1 UN-STORAGE TANK; ALL SPILL REGLAIMED

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 30% 912

POCATELLS, IDAHO 53264

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

:156 WEST HIGHWAY 30

RELEASE DATE:

01/09/50

MATERIAL RELEASED:

AMMEDI SCRUBBER LID

QUANTITY RELEASED:

APPROX 190 GALLONS

DID MATERIAL ENTER A WATERWAY:

19.

SOURCE OF RELEASE

PAD OVERFLOWED

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 20% 912

POCATELLO, IDAHO 83204

COUNTY

- WER

RELEASE LOCATION:

DOW, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

₩1/27/**9**₩

MATERIAL RELEASED:

78% H2SO4

QUANTITY RELEASED:

20 GALLONE

DID MATERIAL ENTER A WATERWAY:

ΝŌ

SOURCE OF RELEASE

PIPING SPOOL PIECE FAILED

MINERALS & CHEMICAL DIVISION

COMPANY MAKE:

J. R. SIMPLOT COMPANY

ADBRESS:

P. D. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAMO

RELEAGE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

02/08/90

MATERIAL RELEASED:

52% PHOSPHORIC ACID

QUANTITY RELEASED:

129 POUNDS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

TANK 53

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDESES:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

CUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. J. 30% 912

POJATELLO, IDAHO 83204

FUMER

DON. IDAHD

1150 WEST HIGHWAY 30

92/98/99

LSL

500 SALLONE

桕

LIQUID, FLANT #4 DOCK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

P. C. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FUMER

RELEASE LOCATION:

30M. 1**0**AHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

82/29/90

MATERIAL RELEASED:

52% PHOS ACID

QUANTITY RELEASED:

39 TO 100 GALLONS

DID MATERIAL ENTER A MATERWAY:

NE ·

SOURCE OF RELEASE

LEAKING PACKING ON #53 TRANSFER PUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POMER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/02/90

MATERIAL RELEASED:

2.5% P205

GUANTITY RELEASED:

150 6ALLOWS .

DID MATERIAL ENTER A WATERWAY:

MO '

SOURCE OF RELEASE

EVAPS

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

2. 0. 20% 91Z

POCATELLO, IDAHO 83204

COUNTY

FONER

RELEASE LOCATION:

004. IDAFO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

03/07/90

MATERIAL RELEASED:

78% H2904

QUANTITY RELEASED:

30-50 GALLONS

DID MATERIAL ENTER A WATERWAY:

NŪ

SOURCE OF RELEASE

ACID LINE TO B.F.W. FREHEATER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY SELEAGED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

f. 0. 20X 912

POCATELLO, IDAHO 83204

FOMER

DOA, IDAHG

1150 WEST HIGHWAY 30

93/29/90

54% NITRIC ACID

70 GALLONS

NO

#2 NITRIC ACID STORAGE TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912 POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/03/50

MATERIAL RELEASED:

NITRIC ACID

SUANTITY RELEASED:

APPROX 100 GALLONS

DID MATERIAL ENTER A WATERWAY:

NÜ

EQUACE OF RELEASE

ACID BUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

AŭŪRESS:

P. O. EOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

94/18/99

MATERIAL RELEASED:

6-52-0

QUANTITY RELEASED:

30 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

53 TRANSFER LINE

MINERALS & CHEMICAL DIVISION

CONFANY NAME:

J. E. SIMPLOT COMPANY

ADDRESS:

2. 6. BOX 712

FOCATELLO, EDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

00A, 10AHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

04/19/90

MATERIAL RELEASED:

52% PHOS ACID

QUANTITY RELEASED:

JV 6ALLONS

DID MATERIAL ENTER A WATERWAY:

MO

SOURCE OF RELEASE

53 TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

7. 0. 80% 712 POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

❖

MATERIAL RELEASED:

94/29/99

52% P205

GUANTITY RELEASED:

15 GALLŪNS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

53 TANK TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 912

POCATELLO. IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/06/90

MATERIAL RELEASED:

0-52-0 ACID

QUANTITY RELEASED:

APPROX 20 GALLONS

DID MATERIAL ENTER A WATERWAY:

Sil

SOURCE OF RELEASE

BROKEN LIQUID PLANT FEED LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 712

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/98/90

MATERIAL RELEASED:

0-52-0 ASID

QUANTITY RELEASED:

APPROX 10 GALLONS

DID MATERIAL ENTER A WATERWAY:

MiT.

STATELE OF RELEASE

BROKEN LIQUID PLANT FEED LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLUT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 33204

1150 WEST HIGHWAY 30

COUNTY

PEWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

RELEASE DATE:

04/27/89

MATERIAL RELEASED:

0-68-0 DEFLO

QUANTITY RELEASED:

150-200 GALLONS

DID MATERIAL ENTER A WATERWAY:

MΩ

SOURCE OF RELEASE

LOADING LINE TO RAIL CAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

GUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

BOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

POWER

DON, IDAHO

1150 WEST HIGHWAY 30

05/07/89

WEAK H2504 30%

15 GALLONS

NO

STACK DRAIN - 400 FLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

- POCATELLO, IDAHO 83204

COUNTY

FOMER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

*0*5/15/89

MATERIAL RELEASED:

H2S04

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

MO

SOURCE OF RELEASE

#4 H2504

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LUCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/16/89

MATERIAL RELEASED:

H2S04

QUANTITY RELEASED:

440 POUNDS

DID MATERIAL ENTER A WATERWAY:

Νū

SOURCE OF RELEASE

ABS TOWER SEAL LEG DRAIN LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

9. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/22/89

MATERIAL RELEASED:

H2804

QUANTITY RELEASED:

AFPROX 5 SALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

MAG METER ON PROD LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. EIMPLOT COMPANY

ADDRESS:

P. 3. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

a5/23/89

MATERIAL RELEASED:

98% ACID

QUANTITY RELEASED:

17 GALLONG

DID MATERIAL ENTER A WATERWAY:

Νΰ

SOURCE OF RELEASE

FLANGE LEAK ON FINAL TOWER RETURN LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FORER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

05/24/99

MATERIAL RELEASED:

30% H2304

QUANTITY RELEASED:

10 GALLENS

DID MATERIAL ENTER A WATERWAY:

MO

SOURCE OF RELEASE

#2 H2S34 DAYING TOWER DOWN LEG

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDAE55:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

GUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

FONER

DON, IDAHO

1150 WEST HIGHWAY 30

∂5/25/8**9**

0-68-0

1200-2000 GALLSMS

M

LOADING LINE TO MAIL CAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREE5:

P. D. BOX 912 POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LUCATION:

Düt. 19AHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

95/95/39

MATERIAL RELEASED:

75% H2SQ4

PLANTITY RELEASED:

2-3 SALLONS

DID MATERIAL ENTER A WATERWAY:

λij.

SOURCE OF RELEASE

5" HZ504 TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREES:

P. O. 50% 912

POCATELLO, IDAHO 83204

COUNTY

07,50

RELEASE LOCATION:

DCM, 15AHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

06/96/89

MATERIAL RELEASED:

98% H2804

CLANTITY RELEASED:

: GALLON

DID MATERIAL ENTER A WATERWAY:

Νū

BOURCE OF RELEASE

100 COOLING TOWER PH CONTROL TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. BOX 912

POCATELLO, IDAMO 83204

COLINTY

FOWER

RELEASE LOCATION:

00M, 104H0

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

96/11/8**9**

MATERIAL RELEASED:

H2504

QUANTITY RELEASED:

7-10 GALLONS

DID MATERIAL ENTER A WATERWAY:

約

BOURCE OF RELEASE

#1 HZBO4 TANK AND PUMP AREA SUMP PUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 712

POCATELLO, IDAHO 63204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

06/13/39

MATERIAL RELEASED:

SULFURIO ACID - 98%

CUANTITY RELEASED:

150 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

ERGKEN ACTO LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. EINPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

NAN. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

96/15/39

MATERIAL RELEASED:

93% H2804

QUANTITY RELEASED:

5 GALLONE .

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

BUMP BASIN AT PUMPS

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL/RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A MATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

BANNSOK

DON, IDAHO

1150 WEST HIGHWAY 30

05/07/90

SUPES ACID DEFLO

AFPROX 250 64LLONS

NO

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 6. BOX 912

PCCATELLO, IDAHO 83204

COUNTY

POWER

SELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 36

PELEASE DATE:

95/14/90

MATERIAL RELEASED:

93% H2SO4

QUANTITY RELEASED:

10 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

SOURCE OF RELEASE

RAILCAR LOADING LINE FILTER

MINERALS & CHEMICAL DIVISION

COMFANY NAME:

J. R. SIMPLOT COMPANY

ADDREES:

P. J. 30% 713

PODATELLO, IDAHO 83204

COUNTY

FOMES

RELEASE LOCATION:

DON, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

*0*5/16/90

MATERIAL RELEASED:

UX32

QUANTITY RELEASED:

400 TO 500 GALLONS

DID MATERIAL ENTER A WATERWAY:

Νĵ

BOURCE OF RELEASE.

KENTCO TRUCK #1146, LEAKING VALVE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

GEANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

SOURCE OF RELEASE

J. R. SIMPLOT COMPANY

F. D. BOX 712

FOCATELLO, IDAHO 63204

FUWER

DOM. IDAHO

1150 WEST HIGHWAY 30

95/23/70

2-44 8205

200 GALLONE

MT.

LIGUID PLANT

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

QUANTITY RELEASED:

DID MATERIAL ENTER A WATERWAY:

BOURCE OF RELEASE

J. R. SIMPLOT COMPANY

P. C. BOX 912

FOCATELLO, IDAHO 83204

POHER

DOM, IDAKO

1150 WEST HIGHWAY 30

95/39/90

NITRIC ACID

APPROX 20-25 64LLONS

NŪ .

#2 MITRIC ACID TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BO% 912

POCATELLO, IDAMO 83204

1150 WEST HIGHWAY 30

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHO

RELEASE ADDRESS:

•

RELEASE DATE:

MATERIAL RELEASED:

06/09/90 H2S04

OLANTITY RELEASED:

ZOO BALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

PRODUCT TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

50M. 104H0

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

06/11/90

MATERIAL RELEASED:

H2504

QUANTITY RELEASED:

100 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

SOURCE OF RELEASE

#3 H2SO4, ACID FIRING

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 50% 712

POCATELLO, IDAMO 83204

COUNTY

FOWER .

RELEASE LOCATION:

DOM, HEARD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

96/15/90 ·

MATERIAL RELEASED:

98% H2904

QUANTITY RELEASED:

150 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

HZSO4 TRANSFER PIPING

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

FONER

RELEASE LOCATION:

DON, IDAHD

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

95/29/70

MATERIAL RELEASED:

QUANTITY RELEASED:

76% K2904

•

SW SALLONS

DID MATERIAL ENTER A WATERWAY:

N5

SOURCE OF RELEASE

DRAIN LINE @ #3 H2SD4

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. 0. 80% 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON. IDAHC

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

85/20/96

MATERIAL RELEASED:

98% H2804

QUANTITY RELEASED:

35 JALLONS

DID MATERIAL ENTER A WATERWAY:

NO.

ECURCE OF RELEASE

73 ACID COOLER

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDREES:

P. 0. 86% 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DON, IDAHO

RELEAGE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

86/22/98

MATERIAL RELEASED:

SULFURRIC ACID

GUANTITY BELEASED:

30 GALLONS

DID MATERIAL ENTER A WATERWAY:

Νū

SOURCE OF RELEASE

98% FUMP TANK

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

9. 6. BOX 912

POCATELLO, IDAMO 83204.

COURTY

POWER

RELEASE LOCATION:

CON, COARO

RELEASE ADDRESS:

1150 WEST HISHWAY 30

RELEASE DATE:

MATERIAL RELEASED:

97/15/**9**0

98% #2504

QUANTITY RELEASED:

JØ SALLDAS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

SOUTH 98 I.A.T. FUMP #4 H2EO4

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMFANY

ADDRESE:

8. **3. BOX 912**

POCATELLO, IDAHO 53204

COUNTY

STATE

RELEASE LOCATION:

DEN, TEAHD

RELEASE ADDRESS:

1156 WEST HIGHWAY 30

RELEAGE DATE:

07/19/90

MATERIAL RELEASED:

78% H**29**04

QUANTITY RELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝO

SOURCE OF RELEASE

ACTO TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 0. 30% 912

POCATELLO, IDAHG 83204

1150 WEST HIGHWAY 30

COUNTY

FOWER

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

RELEASE DATE:

07/24/90

MATERIAL RELEASED:

93% H2804

QUANTITY RELEASED:

. 20-25 GALLONS

DID MATERIAL ENTER A WATERWAY:

NΩ

SOURCE OF RELEASE

LOADING RAILCAR

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. 3. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

BOA. IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

09/17/90

MATERIAL RELEASED:

0-70-0

QUANTITY RELEASED:

25+ GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

MIRIC REACTOR

· MINERALE & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. 0. 30/ 912

FOCATELLO, IDAFO 83204

COUNTY

구민무구의

RELEASE LOCATION:

564, 10ARC

RELEASE ADDRESS:

1156 WEST HIGHWAY 30

RELEASE DATE:

99/29/99

MATERIAL RELEASED:

42% P235

QUANTITY RELEASED:

1000 6AL (7300 LBS)

DID MATERIAL ENTER A WATERWAY:

N/D

BOURCE OF RELEASE

MORTH OF #22 TANK PAD

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. J. BOX 912

POCATELLO, IDAHO 83204

COUNTY

FOWER

RELEASE LOCATION:

906, 19A69

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

97/19/96

MATERIAL RELEASED:

<u>∟S__0-76</u>--6

QUANTITY RELEASED:

20 TO 30 GALLONS

DID MATERIAL ENTER A WATERWAY:

M.

EGURCE OF RELEASE

#4 STOPAGE TANK TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY MAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

POCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

DOM, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

PELEASE DATE:

99/26/99

MATERIAL RELEASED:

P205, 0-70-0

QUANTITY SELEASED:

50 GALLONS

DID MATERIAL ENTER A WATERWAY:

ΝĐ

SOURCE OF RELEASE

LIGUID

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

F. O. BOX 912 FOCATELLO, IDAHO 83204

COUNTY

POWER

RELEASE LOCATION:

SON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEAGE DATE:

11/03/90

MATERIAL RELEASED:

NITRIC ACID, 52%

GLANTITY RELEASED:

30 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

SOURCE OF RELEASE

NITRIC ACID STORAGE TANK #1

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. 8. BOX 912

FOCATELLO, IDAHO 83204

COUNTY

FENER

RELEASE LOCATION:

DOM, IDHAG

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/85/90

MATERIAL RELEASED:

93% H2904

QUANTITY RELEASED:

5 TO 10 BALLONE

DID MATERIAL ENTER A WATERWAY:

NO ·

EDURCE OF RELEASE

3" H2SO4 TRANSFER LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. S. BOX 912

POCATELLO, 10AHO 63204

COUNTY

POAER

RELEASE LOCATION:

DOM. IBAhO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/66/76

MATERIAL RELEASED:

42% F265

QUANTITY RELEASED:

3,834 LBS (H3FC4)

DID MATERIAL ENTER A WATERWAY:

Nū

GCURCE OF RELEASE

PHOS ACID - #22 TANK TRANSFER SYSTEM

MINERALS & CHÉMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. D. BEX 712

POCATELLO, IDAHO 53204

COUNTY

POWER

RELEASE LOCATION:

CON. ICAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/13/99

MATERIAL RELEASED:

93% H2804

SUAWTITY RELEASED:

56 GALLONS

DID MATERIAL ENTER A WATERWAY:

NO

BOURCE OF RELEASE

AMMSOX ACID SUPPLY LINE

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. O. BOX 912

FOCATELLO, IDAHO E3204

1150 WEST HIGHWAY 30

COUNTY

o jack

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

RELEASE DATE:

11/17/90

MATERIAL RELEASED:

QUANTITY RELEASED: .

93% H2804

80 GALLONE

DID MATERIAL ENTER A WATERWAY:

Ni)

SOURCE OF RELEASE

EAST AMMO PHOS FEED PUMP

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

ADDRESS:

COUNTY

RELEASE LOCATION:

RELEASE ADDRESS:

RELEASE DATE:

MATERIAL RELEASED:

GUANTITY RELEASED:

DID MATERIAL ENTER A MATERWAY:

SCURCE OF ASLEAGE

J. R. SIMPLOT COMPANY

P. O. BOX 912

POCATELLO, IDAHO 83204

POKER

DON, IDAHO

1150 WEST HIGHWAY 30

11/21/70

SULFURIC ACID H2804

AFFROX 50 GALLONS

Vi.

H2304 LINE

MINERALS, & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. G. 80% 712

POCATELLO, IDAHO 83204

COUNTY

POWER .

RELEASE LOCATION:

DON, IDAHO

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

11/30/90

MATERIAL RELEASED:

78% H2804

BUANTITY RELEASED:

15 GALLENS

DID MATERIAL ENTER A WATERWAY:

ΝŪ

SOURCE OF RELEASE

RE DILUTION FOOT INLET ELBOW

MINERALS & CHEMICAL DIVISION

COMPANY NAME:

J. R. SIMPLOT COMPANY

ADDRESS:

P. D. BCX 912

POCATELLO. 19AHO 83204

COUNTY

DOMER!

RELEASE LOCATION:

354, 1544C

RELEASE ADDRESS:

1150 WEST HIGHWAY 30

RELEASE DATE:

12/61/90

MATERIAL RELEASED:

93% H2964

QUANTITY RELEASED:

15 GALLONS

DID MATERIAL ENTER A WATERWAY:

NC.

SOURCE OF RELEASE

PRODUCT ACID TRANSFER LINE

J. R. SIMPLOT COMPANY

MINERALS & CHEMICAL GROUP DON, IDAHO

PRODUCT FLOW CHARTS

&

INFORMATION SHEETS

November 7, 1989

DON PLANT

Phosphate ore is shipped in by rail from the Smoky Canyon Mine year round, and from the Gay Mine during the summer months. The ore is stockpiled during the heavy shipping months and used during the winter or light shipping months.

The ore is conveyed from the stockpile to the calciner where it is heated to about 1,500°F., burning out the organic material contained in the ore, thus upgrading the phosphate content by 2-3%. The rock exits the calciner analyzing approximately 32-34% P₂O₅ (Phosphorous Pentoxide).

The calcined ore is then ground in Raymond Roller Mills to a fine powder. The ground ore is reacted with sulfuric acid in the phosphoric acid plant to produce phosphoric acid and gypsum, the gypsum being a byproduct. This reaction is approximated by the equation:

$$2H_2O + Ca_3 (PO_4)_2 + 3H_2SO_4 ----> 2H_3PO_4 + 3CaSO_4 \cdot 2H_2O$$

Water + Phosphate Ore + Sulfuric Acid = Phosphoric Acid + Gypsum

The phosphoric acid produced in the phosphoric acid plant is 28-30% P_2O_5 . This acid is then used to make various grades of fertilizers, either as is or, in most applications, concentrated up to 44-52% P_2O_5 .

The sulfuric acid used to make phosphoric acid is produced in two separate plants capable of making 3,200 tons per day of sulfuric acid. The acid is produced by burning liquid sulfur with air to form SO_2 . The SO_2 is then reacted with oxygen over a catalyst to form SO_3 . The SO_3 is then absorbed in water, in the presence of 98% sulfuric, to form sulfuric acid. The reactions are as follows:

$$S + O_2 - SO_2$$

 $2SO_2 + O_2 - SO_3$
 $SO_3 + H_2O - H_2SO_4$

The Don Plant makes and ships five grades of solid fertilizers and four grades of liquid fertilizers. Three of the solids are designated as 'Ammo-Phos' (ammonium phosphate). They are 16-20-0 (ammonium phosphate-sulfate), 18-46-0 (di-ammonium phosphate), and 11-52-0 (mono-ammonium phosphate). Ammonium Sulfate (21-0-0) is another solid fertilizer. The fifth is Triple Superphosphate (0-45-0). The numbers, in order, represent the percent of nitrogen, phosphate, and potash - the basic plant foods - in the product.

In the manufacture of solid ammo-phos the ammonia, phosphoric acid, and sulfuric acid are mixed in a reactor, forming a slurry. This slurry is then mixed with recycle fine product in a granulator. The slurry coats the outside of the recycle particle to form a layer of fresh ammo-phos. The granulated material is then dried and screened. The oversized material is crushed and is recycled with the fines. The intermediate fraction, the product, is cooled and conveyed to storage.

Ammonium sulfate is produced by reacting ammonia and sulfuric acid in a crystallizer under a vacuum, which forms a crystalline product. The crystals are separated from the liquid phase by centrifuging, the crystals being dried and conveyed to storage, and the liquid phase returned to the crystallizer as a "seed" solution.

Triple superphosphate (0-45-0) is produced by reacting ground limestone with phosphoric acid, using a patented Simplot process. This acidulated material is granulated, dried, and screened.

The four grades of liquid fertilizer are 0-52-0 (normal shipping acid), 0-68-0 (super acid), 10-34-0 (liquid ammo phos), and 32-0-0 (UN-32, a solution of ammonium nitrate and urea). The first two are produced by concentration, by evaporation under vacuum, the 28-30% P_2O_5 acid produced in the process first described.

The 10-34-0 is made by reacting ammonia, water, and super acid.

The 32-0-0 (UN-32) is made in a plant that is really three plants in one. Urea is produced by the reaction between carbon dioxide and ammonia in an autoclave. Nitric acid is produced by the conversion of ammonia into nitric oxides with subsequent solution in water. The nitric acid is reacted with

ammonia to produce ammonium nitrate. The urea and ammonium nitrate are then dissolved in water in the proper ratio to produce a solution containing 32% nitrogen (32-0-0).

The ammonia used in the manufacture of the previously mentioned fertilizers is also produced at the Don Plant. It is produced by mixing steam and natural gas together, passing it over a catalyst at high temperature and relatively high pressure to form hydrogen (H₂) and carbon monoxide (CO). Air is mixed in with this stream following the first stage to furnish the nitrogen requirements. The CO is then converted to carbon dioxide (CO₂) and absorbed in monoethanolamine. The unabsorbed CO₂ is then reacted with hydrogen to form methane and water. The water is removed, and the gaseous stream is then compressed to a high pressure (4,200 psig) and passed over a catalyst to form ammonia from the nitrogen and hydrogen. The basic reactions occurring in the plant are:

REFORMING:
$$CH_4 + H_2O \longrightarrow CO + 3H_2$$

METHANATOR:
$$CO_2 + 4H_2 - CH_4 + 2H_2O$$

SYNTHESIS:
$$N_2 + 3H_2 \longrightarrow 2NH_3$$

Simplot schematic flow sheets of most of the described processes are attached.

GAY MINE

The phosphate rock and shales in Southeastern Idaho, Western Wyoming, Northern Utah, and part of Southwestern Montana were deposited during the Permian geological period some two hundred million years ago. The entire area was covered by a sea in which the conditions were exactly right for its deposition from sea water. There is considerable conjecture

about the method of deposition, but it is thought the climate was cool and the atmosphere high in carbon dioxide which could give the right conditions for the formation of phosphate deposits. The deposits were deeply covered by later marine sediments with the area being subsequently uplifted and cut by erosion to expose the ore.

The Gay Mine is located 30 miles northeast of Pocatello on the Fort Hall Indian Reservation, where the J. R. Simplot Company has industrial and mineral leases from the Shoshone-Bannock Indian Tribes.

In 1945 the J. R. Simplot Company became actively engaged in exploration for a source of phosphate rock for their fertilizer plant located at Don, Idaho (near Pocatello). At that time, phosphate rock was being purchased and shipped to the plant from the Montpelier area to the east.

The Fort Hall deposits were examined and found to be satisfactory. Production started in 1947. At that time it was recognized that in order to utilize the maximum tonnage or high grade ores ($+31\% \, P_2 O_5$) from relatively cheap open pit operations, it would be necessary to find a market for the phosphatic shales moved before the high grade ores could be mined, and unless they could be sold the open pit tonnage was limited.

The Westvaco Chemical Division of Food and Machinery Corporation (FMC) was contacted, and the result is the large electric furnace installation for the production of elemental phosphorous now located just west of the Simplot fertilizer plant.

In 1949 a railroad was completed to the mine and loading installations were constructed. A short time later an automatic sampler was built in order to get a continuous sample of the material being shipped and to facilitate blending to maintain grade. Our practice is to mine from two or more pits in one year and to have several faces in any one pit ready for mining. We are thus able to blend and maintain quite uniform grade by short moves of the mining equipment.

The high grade ores are now used for the production of Simplot Triple Superphosphate fertilizers and the manufacture of phosphoric acid. The grade of the phosphate shales is maintained as close to 24% P_2O_5 as possible for the production of elemental phosphorous. The high grade ores

are from three feet to six feet thick and are separated from the furnace shales above by a three foot bed of limestone. The furnace shales vary in thickness from fifteen feet to sometimes as much as forty feet.

The first year's operation was accomplished with small 3/4 yard shovels, tractors, and contract truckers. The ore was transported to Fort Hall, 18 miles west of the mine, and loaded on the railroad at this point. There were 58,000 tons produced that first year.

The mine now operates two shifts per day; 8-hour shifts in winter, and 9-hour shifts in summer. In order to maintain a uniform grade of ore, continuous sampling and assaying is necessary on ore being mined and on ore found in drill holes. This continues the entire year. During summer, when the ore is being shipped, additional sampling and assaying is done to record and control all shipments.

The mining areas are selected for grade and location. The selection for grade is made from drill hole results, and the selection of location is based on averaging the length of ore haul to the railroad loading point. The operation consists of two phases: stripping, which is the removal of waste material to uncover the ore, and mining, which is the taking of the ore. Because of the large workload, these operations are continuous during the entire year. They are usually done simultaneously within a given mining area but can be done alternately, depending upon the conditions. As the mining in an area nears completion, it is necessary to prepare another.

During the year, the total production is over 2,000,000 tons, which requires 24,000 to 25,000 railroad cars. In order to keep the ore moving, the Union Pacific Railroad supplies between 400-450 cars in the circuit. They run two trains of 100 to 110 cars a day, five days a week, and one train on Saturday.

Because of the moisture content in the ore, it is necessary that the total ore production is shipped to Pocatello in the summer to avoid its freezing in the railroad cars. This operations usually starts in April and continues to October.

We are continually adding larger equipment to move the tonnage required. As the near surface ores are depleted, it is necessary to strip a greater yardage to uncover the ores. Presently we are mining to the depth of 300 feet and are removing approximately six tons of waste to recover one ton of ore. Power shovels are used in the mining and in the stripping operations. However, most of the waste is removed by 24 cubic yard self-powered scrapers. These are aided by crawler tractors in loading. The waste is discarded and substantial tonnage of low grade phosphate shales are stockpiled for future beneficiation.

The ore reserves in the western phosphate field are tremendous, but only a small part are suited for open pit mining. As the open pit ores are exhausted and the economics become favorable, underground mining may become more important.

CONDA OPERATIONS

The Conda phosphate operation of the J. R. Simplot Company is located in Caribou County in Southeastern Idaho, seven miles north of Soda Springs and seventy miles east of Pocatello.

This property was formerly owned by the Anaconda Company and operated by them since 1920. In April of 1959 the J. R. Simplot Company entered into a joint operating agreement with A.C.M. where we would operate their Triple and Acid plants at Anaconda. We would also supply our Don Plant with phosphate rock needed over and above the Gay Mine production. In July of 1960, the J. R. Simplot Company purchased the entire Conda facilities and acquired a long term lease of the mining claims and government leases. We also purchased the fertilizer production facilities of A.C.M. at Anaconda, Montana.

Conda has an interesting history. It was developed because A.C.M. needed an outlet for their sulfuric acid, which was a by-product from the copper smelter at Anaconda. Smelting of the sulfide ores produced fumes which were harmful to the surrounding area. This condition was eliminated by conversion to sulfuric acid.

A.C.M. acquired a number of phosphate claims by location and had them patented. Later they acquired additional government leases. They built a camp consisting of about seventy homes, a company store, church, school, railroad, and all other facilities to make Conda relatively self-sufficient. In 1920 Conda was isolated, especially in the winter with the railroad being their only link with Soda Springs.

Open pit equipment was unknown in those days, so all production was from underground. Only the high grade ore was mined. This was crushed and dried and put in very large wooden bins for shipment by rail to Anaconda. This method of operation was continued for thirty-five years, to 1956, at which time some open pit work was started under contract to the Morrison Knudson Company.

In 1952 or 1953 it was found that the upper high grade ore member, which they started to recover from underground, could not be used for fertilizer production without prior washing and discarding some of the impurities. This resulted in construction of an addition to the crushing and drying plant. The desired ores were crushed to a minus one-half inch, and scrubbed in a hardinge mill. The undesirable slimes produced were eliminated by separation in hydroclones.

This method of beneficiation or upgrading of the high grade hanging wall ore could be used on the phosphate shales to produce an acid grade product. However, the economics of mining shales from underground precluded their use. Only when open pit mining was started were the shales used for beneficiation.

The J. R. SImplot Company acquired the A.C.M. phosphate mining and fertilizer interests in 1959. The J. R. Simplot Company uses a mill process essentially the same as that developed by A.C.M. The ore fed to the mill averages about 24.5% P_2O_5 . The final product has an analysis of 31.5% to 32% P_2O_5 .

The Conda mining operation ceased functioning in May 1984 because a new operation, known as the Smoky Canyon Mine, had been developed.

The Conda facility continues to process phosphate ore. The incoming phosphate ore from the Smoky Canyon Mine is transported to Conda by a

25-mile long slurry pipeline. At Conda the phosphate ore is separated from the water by vacuum filters. The moist filter cake is dried and loaded in rail cars for shipment to the Don Plant where it is calcined. A calciner at Conda, which is currently shut down, is available if the phosphate ore needs to be calcined prior to shipment.

SMOKY CANYON MINE

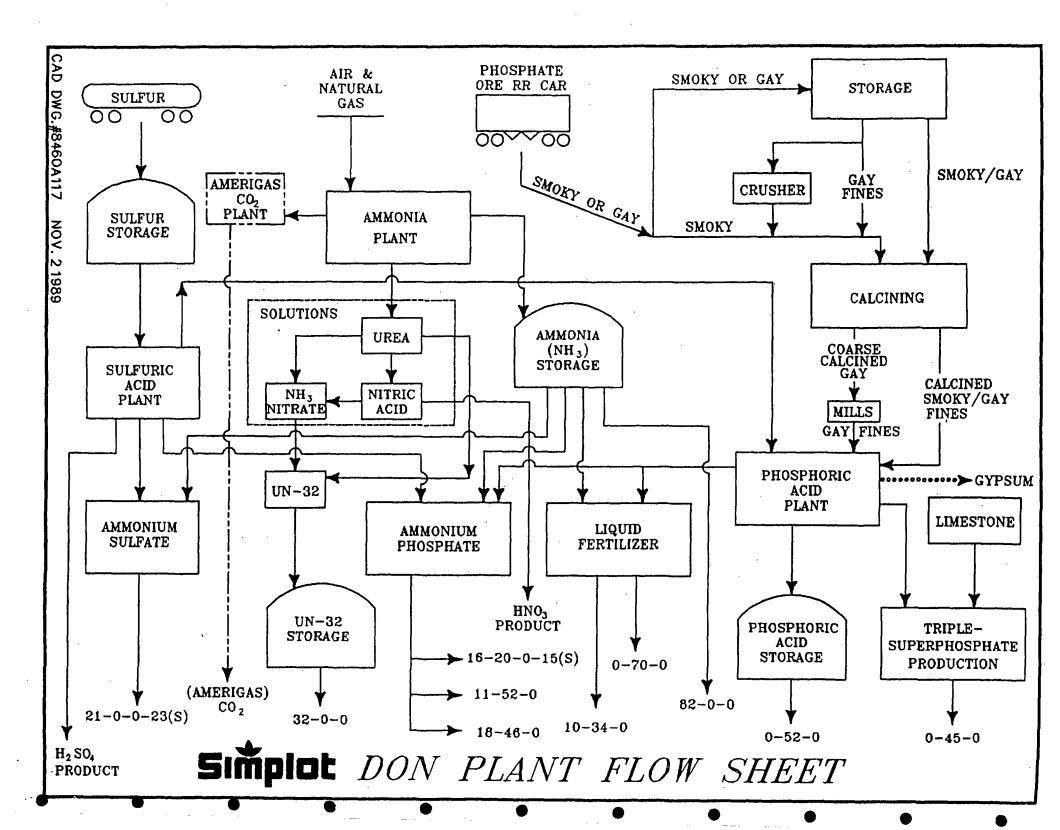
The Smoky Canyon phosphate mining/processing plant is located 25 miles east of Soda Springs, Idaho and 10 miles west of Afton, Wyoming. The mine produces about one million tons of phosphate rock per year. Overburden from the mine is initially placed in surface dumps. As areas are mined to completion, overburden from subsequent mining areas back fill the mined-out pits. The ore is beneficiated (physically washed) on site with tailings disposed of on private land about one mile east of the mine. The beneficiated ore is transported about 25 miles in a buried slurry pipeline to the existing J. R. Simplot Company plant in Conda, Idaho.

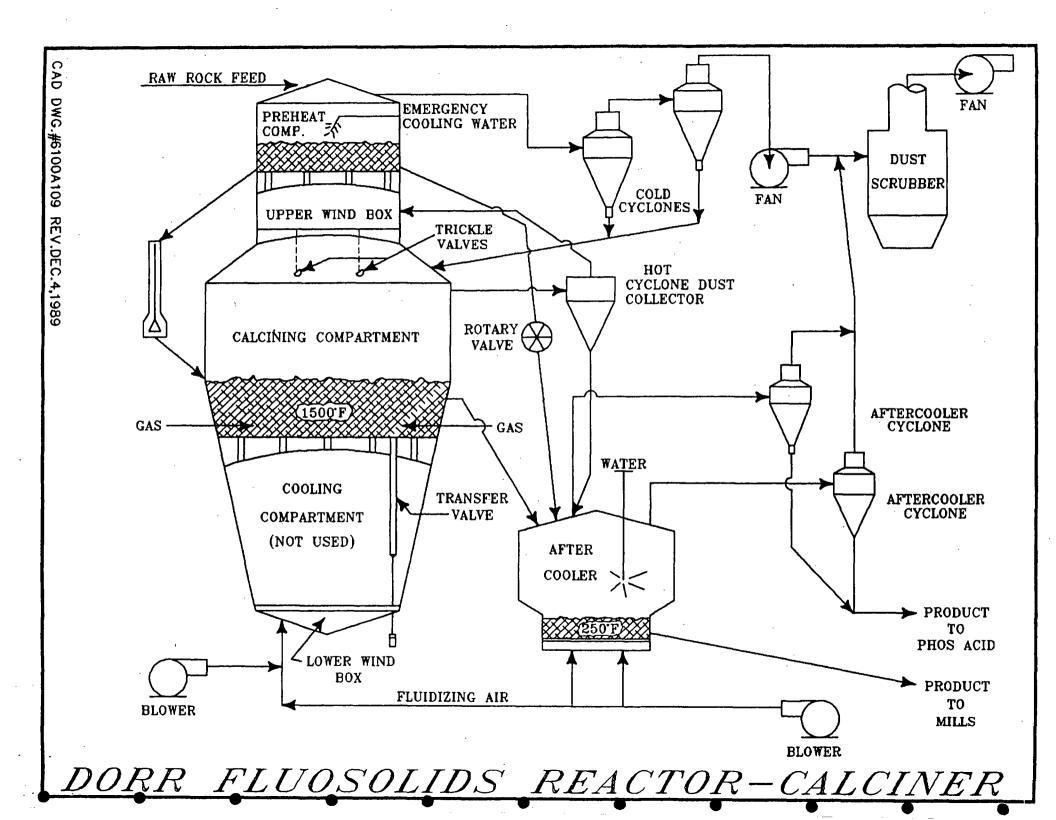
The Smoky Canyon Mine is an open pit operation using a P&H 2300 electric shovel matched with 170-ton Lectra Haul trucks. The mining and stripping operations use the same equipment. In most places the overburden must be drilled and blasted prior to stripping. The overburden and Meade Peak waste material is loaded in the 170-ton trucks and hauled to the overburden disposal area or back filled into the pits. The exposed ore in benches is mined and transported to the mill stockpile for processing and beneficiation.

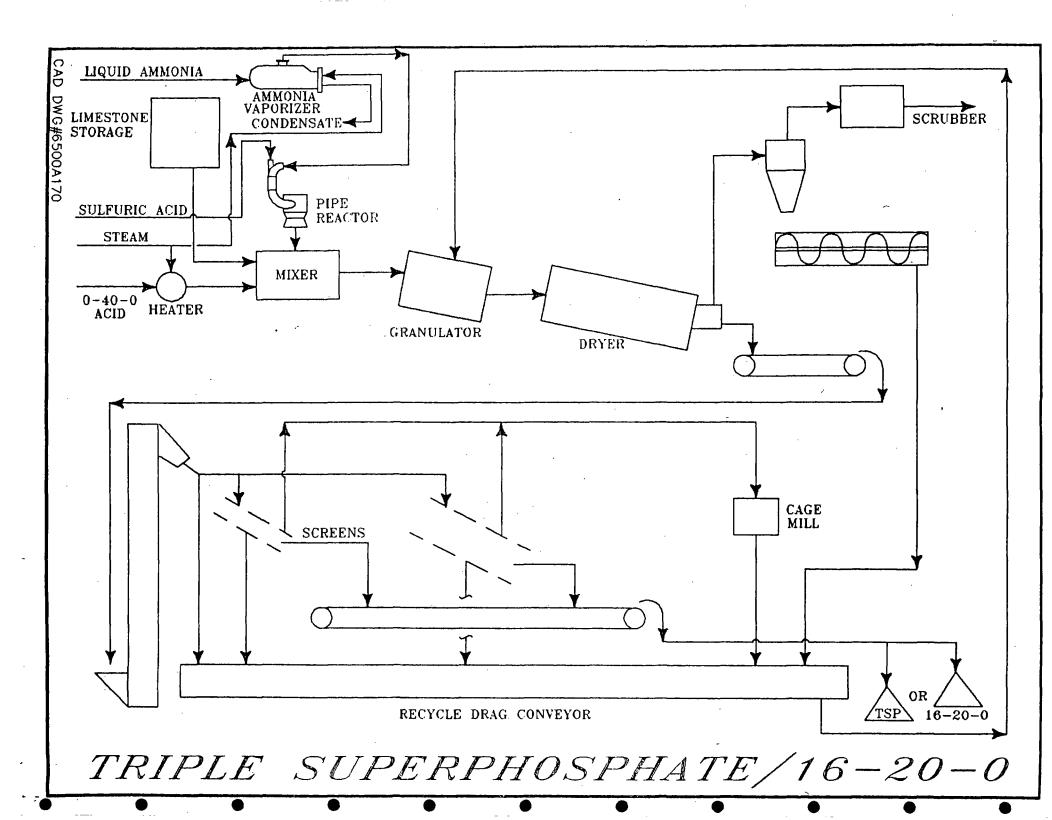
The Simplot lease is on the nose of the north-plunging Boulder Creek Anticline, covering five and one-half miles of the west limb and two miles of the east limb phosphoria outcrop. Dips range from five to forty-five degrees except for the east limb, which becomes vertical to overturned near the valley floor. The phosphoria outcrop appears to be relatively free of faulting. Most of the mapped faults strike northwest and tent to repeat the section in a fashion favorable to open pit mining. Sections measured by Simplot indicate a Meade Peak member thickness of 150 feet, and a Rex Chert member

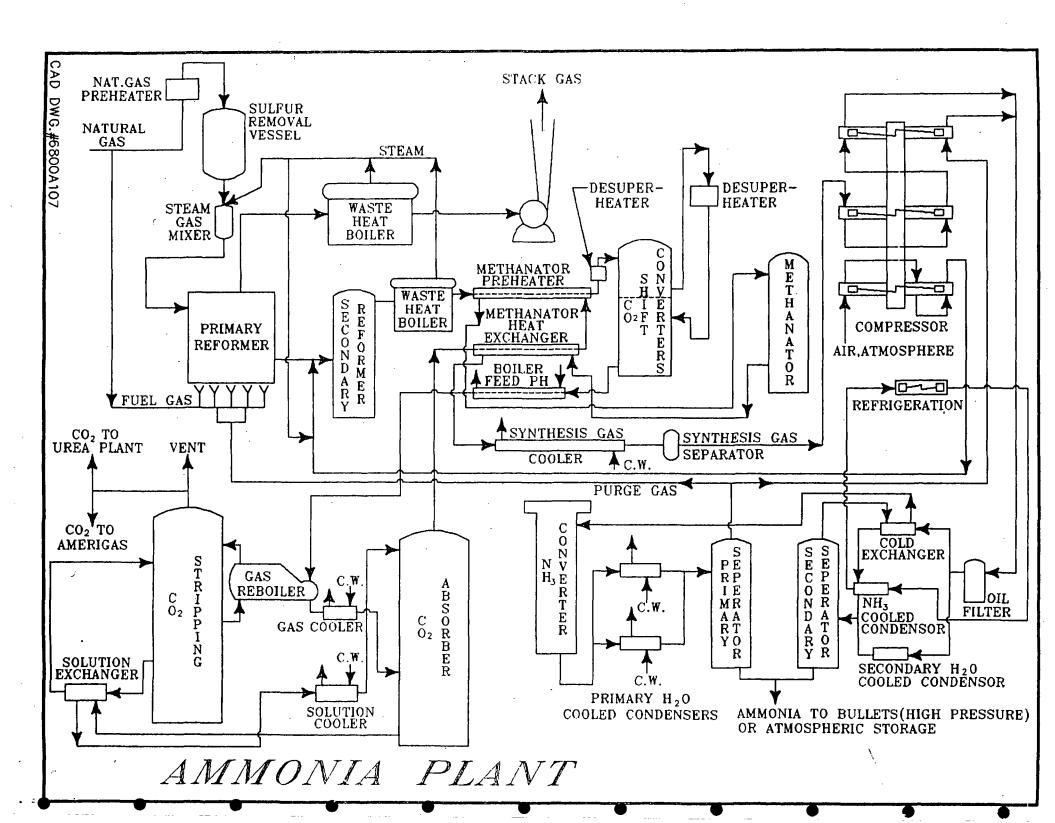
thickness of 100 to 150 feet. The ore section is one of the thickest in the Western Phosphate Field. The hanging wall or upper ore section is 23 feet thick and the foot wall or lower ore section measures about 20 feet thick.

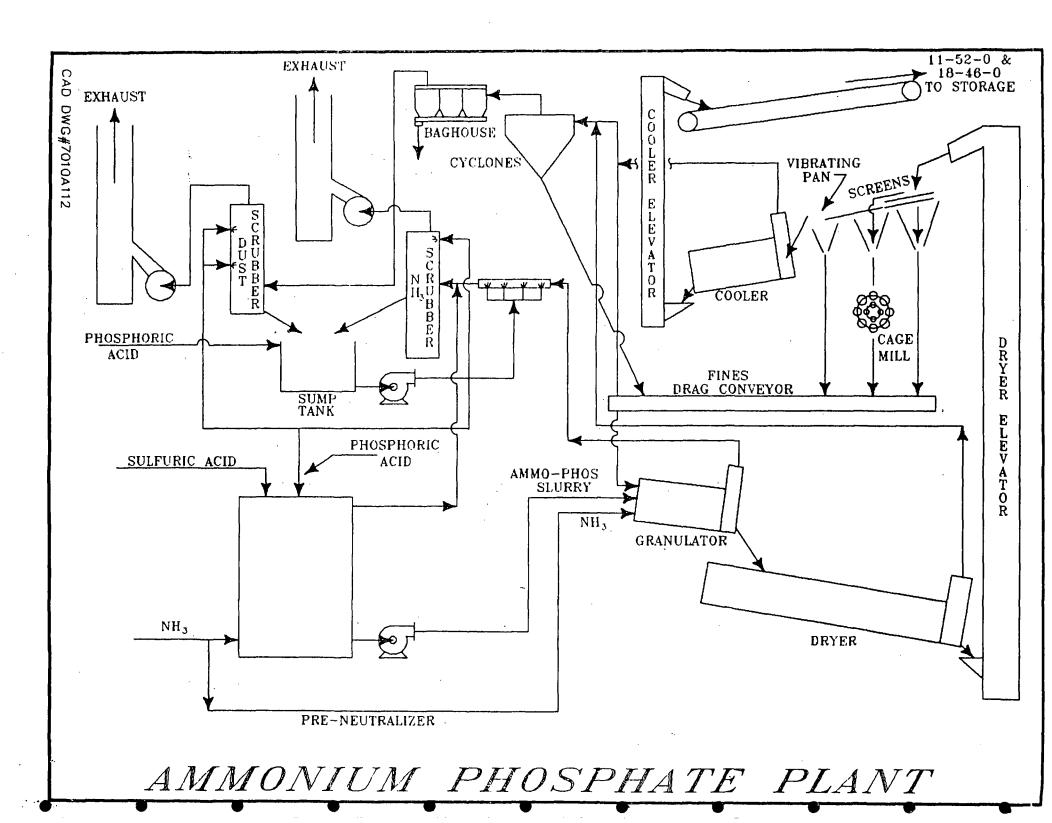
The various grades of ore are stockpiled at the Conda plant and are blended to provide a mill feed of 26% to 27% P_2O_5 . Beneficiation consists of crushing and washing, which yields a 72% BPL (33% P_2O_5) concentrate suitable for production of phosphoric acid. The ore is first screened into three size ranges: minus 6mm (-1/4"), minus 16mm to plus 6mm (-5/8" to +1/4"), and minus 22mm (-7/8"). The plus 22mm fraction is discarded. In the following stages the fine fraction reports to classifiers and hydroclones while the coarser material is reduced in a Marcy rod mill prior to entering the hydroclone system. Beneficiated product grades at +324 mesh, dewatered in Eimco vacuum filters and dried to 3% moisture. Tailings contain 10-12% P_2O_5 and 7-8% moisture, and are disposed of in an 80-acre pond. Approximately one-third of process water is recovered.

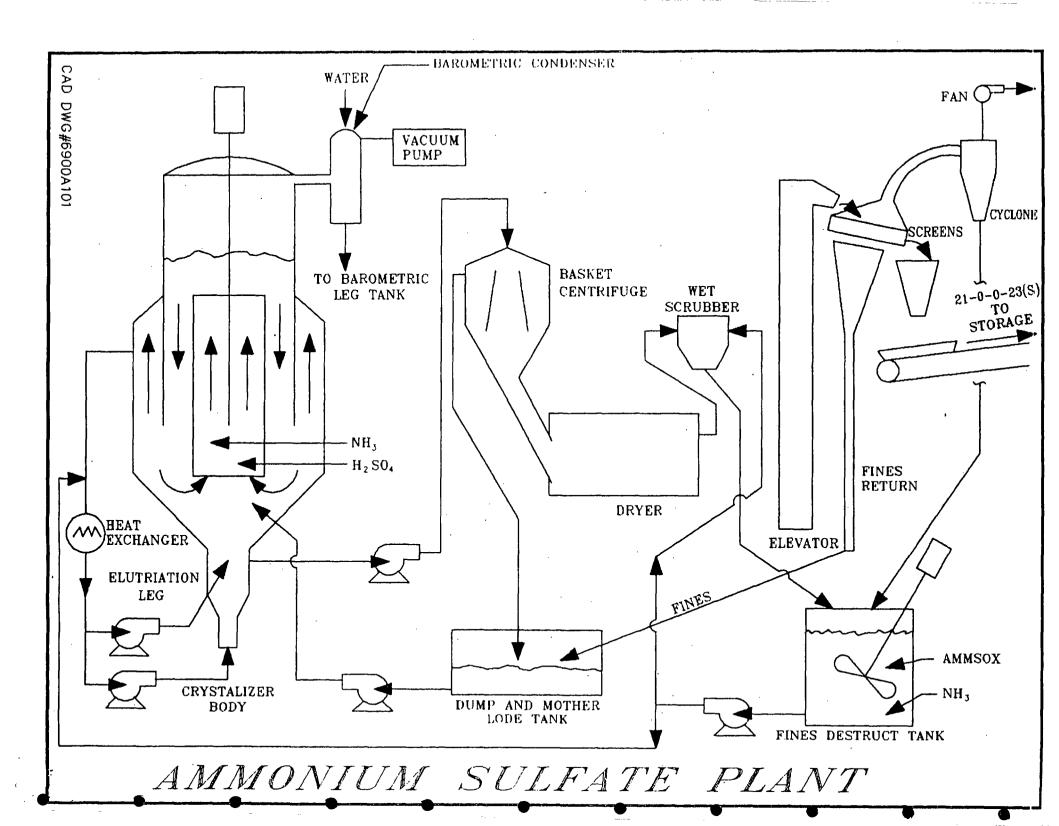


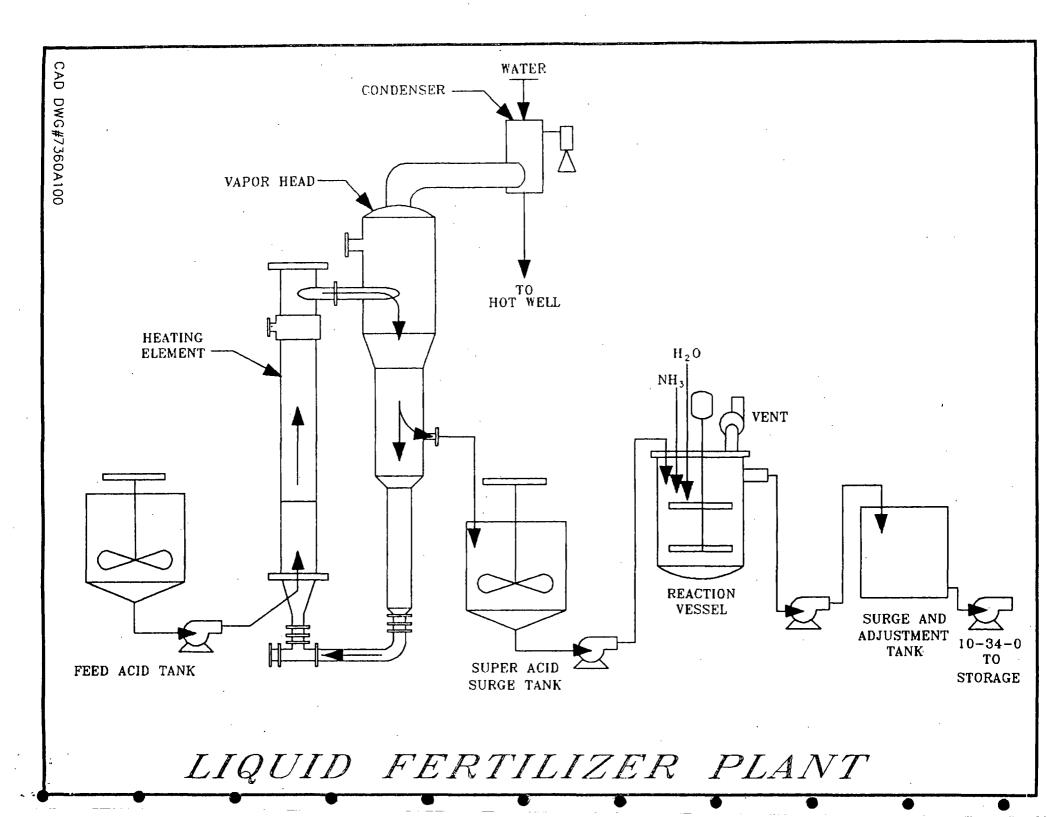


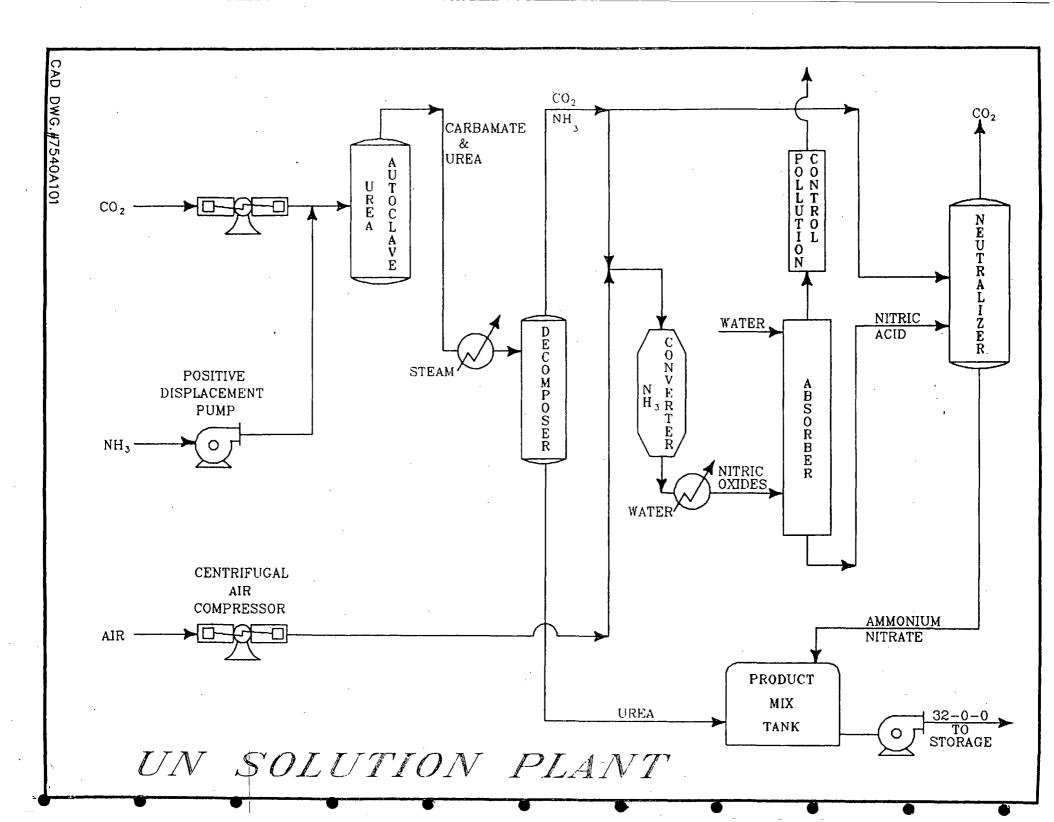


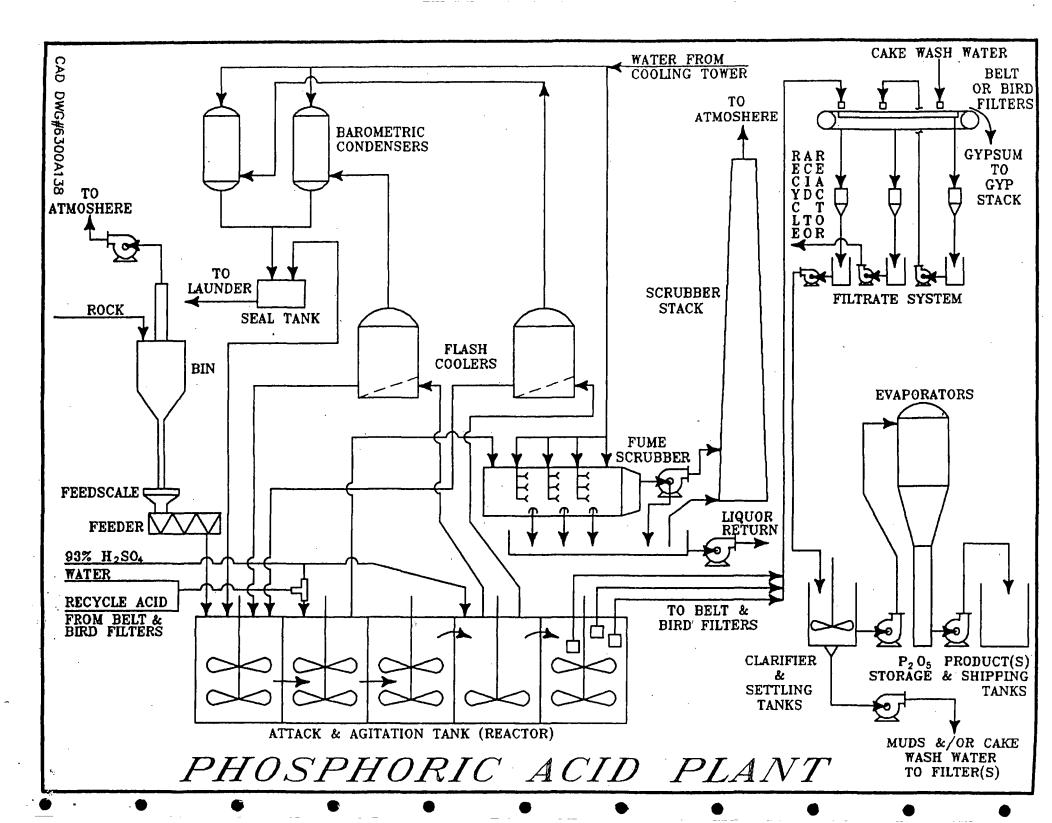


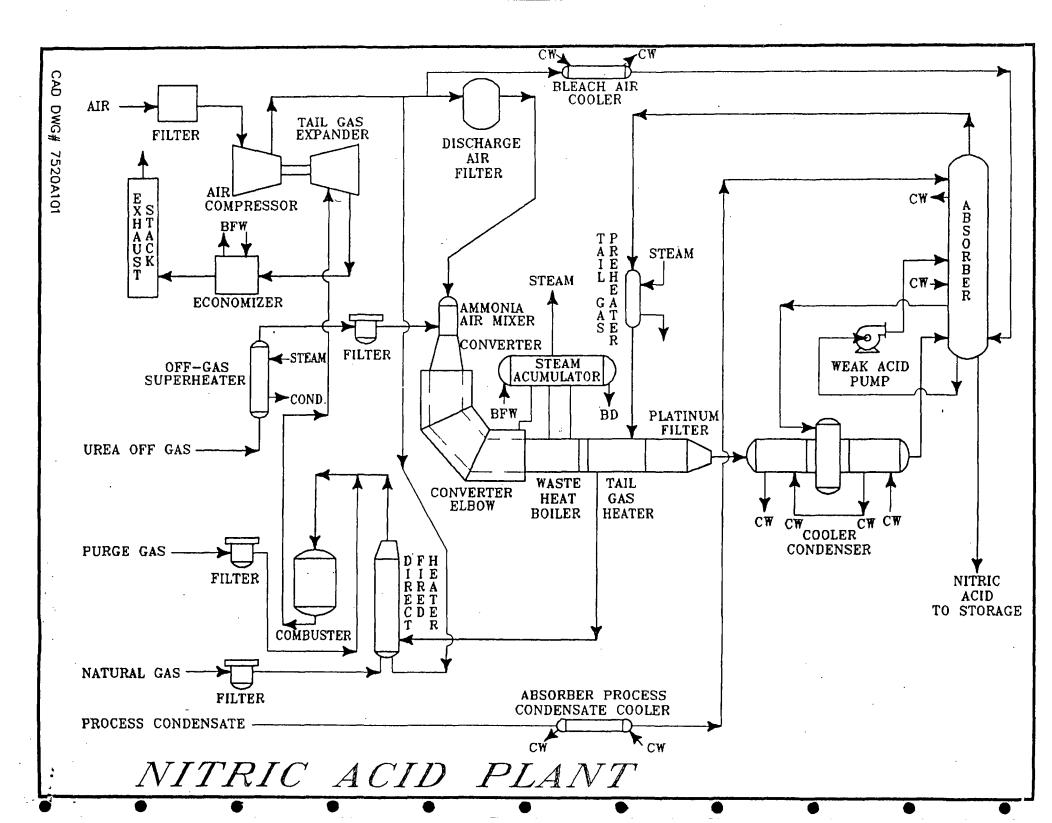


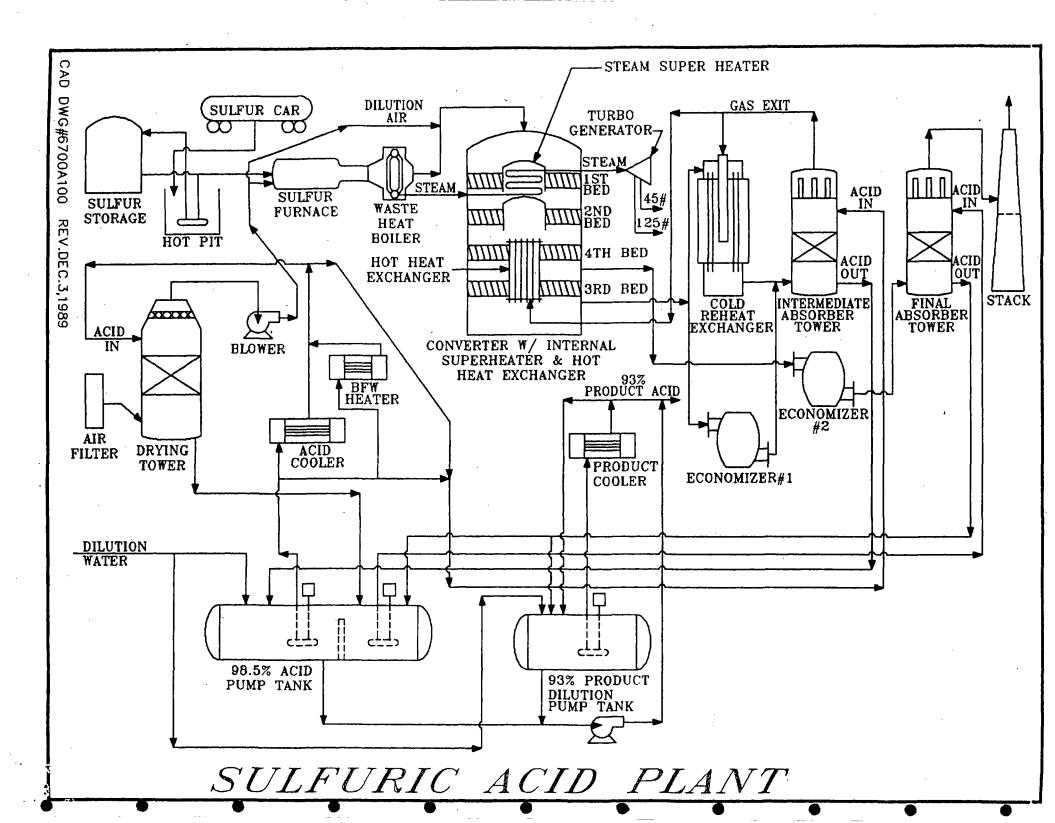


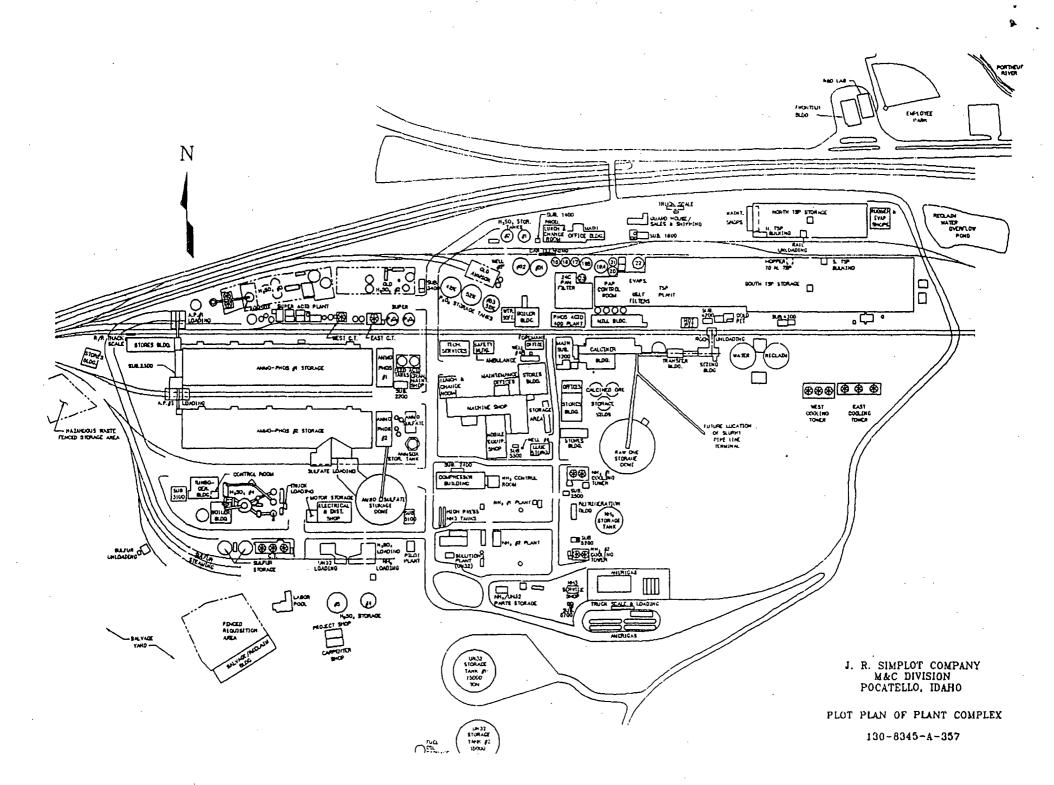












EASEMENT

THIS AGREEMENT Made and entered into this ______ day of April, 1949, by and between J. R. SIMPLOT and RUBY A. SIMPLOT, his wife, and J. R. SIMPLOT COMPANY, a corporation, hereinafter known and designated as parties of the first part, and FOOD MACHINERY AND CHEMICAL CORPORATION, a foreign corporation of the State of Delaware, hereinafter known and designated as party of the second part, WITNESSETH:

That said first parties for and in consideration of the sum of One Dollar (\$1.00), to them in hand paid by said second party, the receipt of which is hereby acknowledged, and for other and valuable considerations, and in consideration of the mutual covenants on behalf of said parties, all as hereinafter contained, said first parties do sell and convey unto said second party, its successors and assigns, a strip or parcel of land of sufficient width for the construction, operation and maintenance of a waste water disposal ditch that as and when constructed and maintained will be two feet wide at the bottom and be so constructed as to adequately carry the waste water for the purposes for which it is constructed, the same to be located all as is shown by Simplot Drawing No. M - 3 - 128, dated 4/4/49, a copy of such map being hereto attached and made a part hereof; the course and direction of such ditch to be as follows, to-vit:

Beginning at the SW corner of the SW-SW-, Sec. 7, T. 6 S., R. 34 E.B.M. and proceeding due north on the range line separating Section 7, T. 6 S., R. 34 E.B.M. from Sec. 12, T. 6 S., R. 33 E.B.M. a distance of 632.80 feet to a point (A). Point MAM is the point of intersection of the center line of the proposed waste unter disposel ditch and the above described range line. Proceeding from point MAM on a bearing of M 72° 23' E for a distance of 324.7 ft. to station 0,00; thence S 56°58' E for a distance of 200.0 ft. to station 2,00; thence S 36°42' E for a distance of 100.0 ft. to station 3,00; thence on a bearing of S 45° 34' E for a distance of 300.0 ft to station 6,00; thence on a bearing of S 31° 32' E for a distance of 200.0 ft. to station 8,00; thence on a bearing of N 76° 10' E for a distance of 400.0 ft. to station 12,00; thence on a bearing of N 75° 04' E for a distance of 200.0 ft to station 14,00; thence on a bearing of N 75° 04' E for a distance of 200.0 ft to station 14,00; thence on a bearing of N 75° 04' E for a distance of 200.0 ft to station 14,00; thence on a bearing of N 75° 04' E for a distance of 200.0 ft to station 14,00; thence on a bearing of N 75° 04' E for a distance of 200.0 ft to station 14,00; thence on a bearing of N 629 15' E for a distance

5.2.1 0001

of 200.0 ft. to station 16400; thence on a bearing of N 78° 43' E for a distance of 200.0 ft. to station 18400; thence on a bearing of S 84° 25' E for a distance of 200.0 ft. to station 20+00; thence on a bearing of S 66° 46' E for a distance of 200.0 ft. to station 22+00; thence on a bearing of 79° 12' E for a distance of 100.0 ft. to station 23+00; thence on a bearing of N 830 261 E for a distance of 100.0 ft. to station 24+00; thence on a bearing of N 65° 42' E for a distance of 200.0 ft. to station 26-00; thence on a bearing of S 87° 26' E for. a distance of 200.0 ft. to station 28-00; thence on a bearing of S 75° 56' E for a distance of 200.0 ft to station 30-00; thence on a bearing of N 65° 52' E for a distance of 200.0 ft. to station 32-00; thence on a bearing of N 70° 59' E for a distance of 200.0 ft. to station 34400; thence on a bearing of N 74° 22'E for a distance of 20:.00 ft. to station 36:00; thence on a bearing of 8 86° 30' E for a distance of 163.9 ft. to station 37-63.9 (point of intersection of existing Simplot drainage ditch); thence on a bearing of N 780 18' E for a distance of 46.6 ft. to station 38-10.5; thence on a bearing of N 69° 20' E for a distance of 25.5 ft. to station 38-46; thence on a bearing of S 78° 00' E for a distance of 103.0 ft. to station 39-49; thence on a bearing of N 85° 42' E to point "B", the point of intersection of the center line of the proposed waste water disposal ditch and the east Simplot property line. Point "B" is situated on a bearing of NOO 09'W of the SE corner (found) of the SUESE, Sec. 7, T. 6 S., R. 34 E.B.M., a distance of 606.71 ft.

The center line of the proposed Westvaco Waste water disposal ditch passes through the SW2SW2, SE2SW2, SW2SE2, Sec. 7, T. 6 S., R. 34 E.B.M.

for the purpose of building, constructing and maintaining a drain ditch to carry waste water from second party's operations, subject to the rights of said first parties, or either of them, their heirs, assigns or successors to change or alter said course of such ditch, and likewise the right to use therefrom all m any portion of the said water draining through such ditch.

IT IS FURTHER UNDERSTOOD AND AGREED By and between the parties hereto that in the event said first parties, or either of them, their heirs, successors or assigns, desire to build an extension on the said present buildings, or any extensions in the future on their said buildings, that such extension, or extensions, would be of sufficient size or so located as to interfere with the operation of such ditch, that said second party will, upon written request, mave such ditch, to the end that the construction, operation and maintenance thereof will not interfere with the building of such new buildings, extension, or extensions,

of the present or future constructed buildings, or said second party will tile such ditch, such tiling to be so performed as to serve said first parties' purpose, and said first parties herein are hereby granted the privilege to request either removal of such ditch to another location on its, or their, said premises, or that the ditch be tiled, the cost thereof to be born by said second party.

IT IS FURTHER UNDERSTOOD AND AGREED By and between the parties hereto that the right herein granted is one for the transportation of water through the lands of said first parties, and that said second party shall at all times furnish a sufficient and adequate waste-way, or drain-way, or easement of right of way for the transportation of such water from first parties premises to a point where the same enters the Portneuf River, and that as soon as said water is placed in the said ditch, as herein described, the same shall be deemed to be the property of said first parties merely for the right to the use thereof, and not otherwise,

IT IS FURTHER UNDERSTOOD AND ACREED By and between the parties hereto that in the event said first parties desire to cross over said ditch that they shall construct adequate and proper crossings.

IT IS FURTHER UNDERSTOOD AND AGREED By and between the parties hereto that first parties shall have the privilege to construct the said ditch, the cost, however, of such construction work to be storevailing prices and to be born by said second party.

IT IS FURTHER UNDERSTOOD AND AGREED By and between the partles hereto that the first parties reserve the right to change the course of such ditch at such time, or times, as is deemed advisable by them, or either of them, provided, however, the change shall in no wise destroy the right to have a ditch and the maintenance of a ditch sufficient in all respects to carry said waste water, and this right and privilege is in addition to the right of change heretofore mentioned.

IT IS FURTHER UNDERSTOOD AND AGREED By and between the parties hereto that when the said first parties are referred to the same shall

include all or either one of said first parties.

IN WITHESS WHEREOF The parties hereto have hereunto set their hands the day and year first above written.

J. R. SIMPLOT

RUBY A. SIMPLOT

J. R. SIMPLOT COMPANY, a corporation,

By

President

Parties of the First Part.

ATTEST:

Secretary

FOOD MACHINFRY AND CHEMICAL COFPORATION,

A Corporation,

Βv

Recorded May 11,1949 Inst. No. 67527

Rescinded in 1973 by a new easement EXDOC MÉC # 28 File also vortains various [
Doeds De 52, Don Block Joseph

EASEMENT

THIS AGREEMENT, made and entered into as of the first day of July, 1973 between J. R. SIMPLOT COMPANY, a corporation (hereinafter called "Simplot") and FMC CORPORATION, a corporation, (hereinafter called "FMC")

WITNESSETH:

That Simplot, for and in consideration of the sum of One Dollar (\$1.00) to it in hand paid by FMC, the receipt of which is hereby acknowledged and for other good and valuable considerations, does hereby grant and convey to FMC, its successors and assigns, an easement and right-of-way over, across and under a strip of land as hereinafter described for the construction, operation, maintenance and repair of a 36" concrete pipeline for disposal of waste water. The course and distances of such pipeline are as outlined on attached map made a part hereof, all as more particularly described as follows:

A strip of land 20.00 feet in width in Section 7, T.6S., R 34E, Boise Meridian lying 10.00 feet on each side of the following described center line:

Commencing at the center of Section 7, T.6S., R. 34E., Boise Meridian;

Thence S29°29'38"W, a distance of 952.79 feet, to a Point on the Southerly Right of Way of U. S. Highway 30, said Point being shown on State of Idaho Highway Department drawing T-15W-4(10) 73, Sheet 11 of 45, being 75.00 feet right of the Centerline Station 29+00;

Thence Sll°10'43"W, a distance of 163.65 feet, along the Westerly property line of the J. R. Simplot Company, to the True Point of Beginning;

Thence S83°46'37"E., a distance of 5.73 feet;

Thence S89°24'37"E., a distance of 381.57 feet;

Thence N15°38'23"E., a distance of 78.31 feet more or less, to a Point of Ending on the Southerly Right of Way of U. S. Highway 30.

ALSO:

A strip of land 20.00 feet in width in Section 7, T6S., R.34 E., Boise Meridian, lying 10.00 feet on each side of the following described Centerline.

Commencing at the Center of Section 7, T6S., R.34 E., Boise Heridian;

Thence S26°56'40"E., a distance of 1029.53 feet to a Point on the Northerly Right of Way of U. S. Highway 30, said Point being shown on State of Idaho, Highway Department drawing T-15W-4(10) 73, Sheet 11 of 45, being 103.22 feet left of Centerline Station 38+28.26;

Thence N74°29'47" W., 444.23 feet;

Thence N47°29'43" E., 86.18 feet;

Thence N64°57'43"E., 13.43 feet to the True Point of Beginning same being on the North Line of the State of Idaho Property;

Thence N64°57'43"E., 707.71 feet;

Thence N69°26'13"E., 425.00 feet, more or less, to a Point of Ending, said Point being located on the Southwesterly Bank of the Portneuf River.

FMC is hereby granted the right of ingress to and egress from the above described premises for the purpose of laying, relaying, repairing and maintaining said pipeline.

Upon the completion of said pipeline and the commencement of delivery of waste water therein by FMC, the parties hereto, as one of the considerations of this agreement, each release and relieve the other from all of the terms and conditions of a certain easement granted by J. R. Simplot Company, J. R. Simplot and Ruby Simplot, his wife, to Food Machinery and Chemical Corporation dated May 11, 1949 and bearing Instrument No. 67527.

At any time subsequent to Twenty years (20) from the date hereof that Simplot shall determine it has a requirement for the use of the property on which said pipeline is located, Simplot may request FMC to change its location, without cost to Simplot, such relocation to be over and across other

available portions of the subject Simplot premises wherein the pipeline is located as may be feasible and convenient for the relocation of said pipeline.

Simplot recognizes that the subject pipeline is to be installed at Simplot's request pursuant to the right of Simplot to request a relocation of a drainage ditch installed by FMC under the terms of the easement of May 11, 1949 hereinabove referred to; that such relocation has been a technical and costly procedure for FMC in procuring permits and easements from third parties and performing engineering work in connection with the construction and installation of such pipeline. If, subsequent to 20 years from the date hereof Simplot requests a further change in the location of the subject pipeline Simplot recognizes it may be necessary for FMC to secure other essements and permits from third parties and from governmental authorities for the further relocation of such pipeline and that FMC's ability to comply with Simplot's request for further relocation of the pipeline will be dependent upon the procurement of such other rights of way and permits as may be required; that FMC will not be required to release the subject easement until it shall have been able to procure adequate and complete permits and rights of way for the further relocation, completion and commencement of operation of said relocated pipeline.

In the event Simplot desires to install a crossing over such pipeline it agrees to take adequate precautions to so construct such crossing in such manner as not to damage said pipeline.

FMC recognizes that Simplot shall in no way be responsible for the negligence of FMC or its employees in installing and maintaining said pipeline.

FMC may abandon the subject pipeline at any time it so

desires and upon such abandonment Simplot shall be completely released of its obligations hereunder. If FMC should permanently shut down its plant thereby terminating the use of said pipeline then this easement shall be deemed abandoned and shall lapse.

IN WITNESS WHEREOF, the parties have hereunto set their hands and seals the day and year first above written.

J. R. SIMPLOT COMPANY

By Vice President

ARTEST Classon Applicant Secretary

FMC CORPORATION

By Vice President

Assistant Secretary

STATE OF NEW YORK
COUNTY OF NEW YORK

On this grad day of July 1973, before me, the undersigned, a Notary Public in and for said County and State, personally appeared John S. DEWICK and HAROLD VOGEL of FMC Corporation, a corporation, the corporation that executed the foregoing instrument, and acknowledged to me that such corporation executed the same.

IN WITNESS WHEREOF, I have hereunto set my hand and affixed my official seal, the day and year in this certificate first above written.

Motary Public Residing at: NE

ELIZADETH A. NYERS

Wetery Public Clate of New York
Hs. 81-200770

Qualificate Hiery York County
Commission Empires March 30, 1075

(SEAL)

100

STATE OF Iclouho SES:

On this 30 th day of file 1973, before me, the undersigned, a Notary Public in and for said County and State, personally appeared for the file and for said County and State, known to me to be the foregoing and for said County and State, and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and for said County and State, personally appeared for any formation and said County any for any for

IN WITNESS WHEREOF, I have hereunto set my hand and affixed my official seal, the day and year in this certificate first above written.

(SEAL)

Notary Public Residing at: Exercic

Stand (1.1.1.)
Loud - Power -

Glorida M. this /devoi Court A. Architecture 17 Land

N 101967 in Drawer.

Margane Glescool

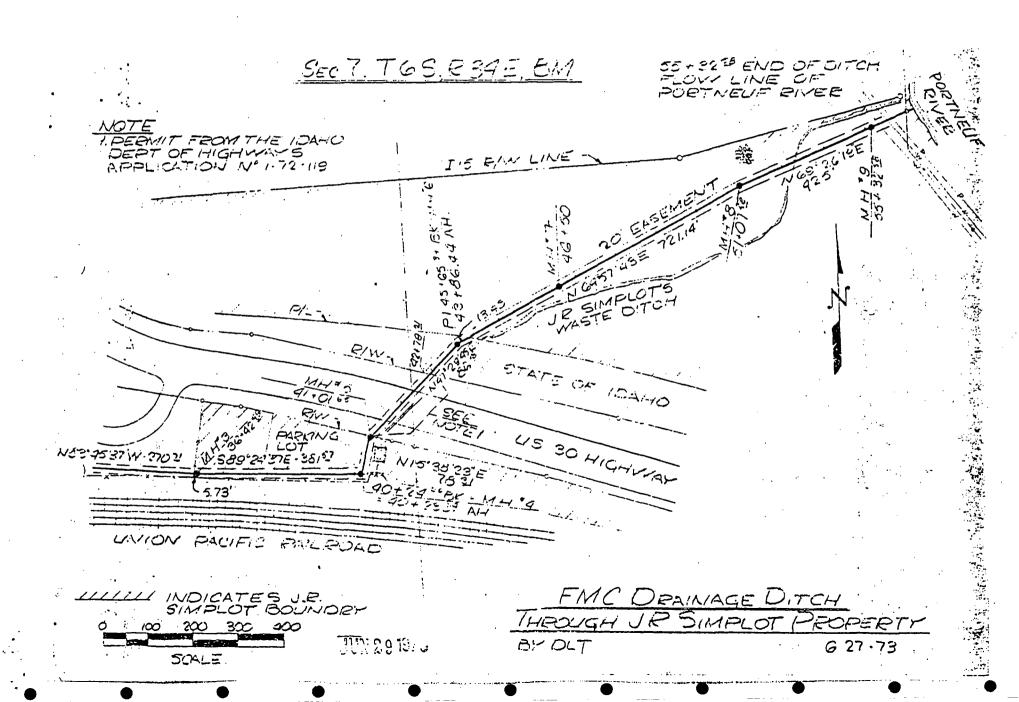


Exhibit #20

.:-

MINERALB AND CHEMICAL DIVIBION
P. O. BOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: November YEAR 1971

| | WEST | PLANT OUTFAI | L | EAST | PLANT OUTF | | 10" DRAIN |
|------|---|--------------|-----------------|--|------------|-----------------|--|
| DAY | ppm (P ₂ 0 ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | 33 | 980 | 388 | 8 | 2550 | 245 | * 17 |
| 5 | 23 | 760 | 210 | 11 | 2700 | 178 | 15 |
| 3 | 11 | . 1050 | 139 | 11 | 2950 | | 18 |
| 4 | 15 | 980 | 176 | 11 | 2700 | 178 | 30 |
| 5 | 13 | 920 | 144 | 15 | 2550 | 459 | 27 |
| . 6 | * 10 | 1250 | 150 | 13 | 3150 | 491 | |
| 7 | 88 | 1170 | 112 | 8 | 2950 | 283 | |
| 8 | * 13 | 1170 | 183 | 8 | 2700 | 259 | 17 |
| 9 | 15 | 1170 | 211 | 8 | 2700 | 259 | 20 |
| 10 | 13 | 1100 | 172 | 15 | 2750 | 495 | 70 |
| 11 | 18 | 1050 | 227 | 23 | 3000 | 828 | 102 |
| 12 | 178 | 200 | 427 | 44 | 2950 | 1558 | 143 |
| 13 | 100 | 920 | 1104 | 20 | 3300 | 792 | |
| 14 | 139 | 1170 | 1952 | 28 % | 3300 | 1109 | |
| 15 | 151 | 270 | 489 | 23 | 3000 | 828 | 147 |
| 16 | 25 | 920 | 386 | 18 | 2950 | 687 | 92 |
| 17 | 30 | 920 | 331 | 25 | 2950 | 885 | 105 |
| 18 | 23 | 840 | 232 | 17 | 2950 | . 602 | 57 |
| 19 | 94 | 920 | 1038 | 28 | 2750 | 924 | 46 |
| 20 | 57 | 760 | 520 | 17 | | . 612 | |
| 21. | 33 | 920 | 364 | 11 | 3300 | 218 | |
| 22 | 72 | 800 | 691 | 20 | 2950 | 708 | 123 |
| 23 | 18 | 800 | 173 | 8 | 3100 | 298 | 28 |
| 24 | | 1050 | , | 10 | 2950 | 354 | |
| 25 | 17 | 760 | 155 | 11 | 3000 | 198 | |
| 26 | 255 | 800 | 2448 | 13 | 2700 | 421 | 105 |
| 27 | 23 | 840 | 232 | 20 | 3000 | 720 | |
| 28 | 57 | 840 | 575 | 50 | 2950 | 1770 | |
| 29 | 46 | 700 | 386 | 48 | 2700 | 1555 | 72 |
| 30 | 165 | 270 | 535 | 46 | 2500 | 1380 | 362 |
| 31 | | | | | | | |
| AVE. | 58 | 877 | 489 | 20 | 2900 | 664 | 80 |

^{*}Grab Samples

MINERALS AND CHEMICAL DIVISION

P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH April YEAR 1974

| · | WEST | | |
|-------------|--------------------|---------|----------|
| Day | Gal/Min | ppm P | lbs/day |
| <u></u> | <u> </u> | (total) | <u> </u> |
| <u>l</u> _ | 446 | 47 | 250 |
| 2 | | 1 | ! |
| 3 | 534 | 44 | 281 |
| 4 | 544 | 55 | 358 |
| 5 | 1 549 | 20 | 134 |
| 5 6 7 | l 680 ⁵ | 65 | 530 |
| | 680 | 70 | 572 |
| 8 | 618 | 10 | 74 |
| 9 | 632 | 7 | ! 56 |
| 10 | 1 759 | 73 | 666 |
|]] | ı 680 | 331 | 2701 |
| 12 | 708 | 114 | 969 |
| 1.3 | ! 680 | 38 | 312 |
|] / | i 680 | 9 | 73 |
| 15 | 628 | 1 6 | 48 |
| 16 | 680 | 24 | 196 |
| 17 | i 679 | 112. | 1 90 |
| 18 | i 592 | 7 | . 48 |
| 19 | 821 | 7 | 73 |
| 20 | 850 | 41 | 414 |
| 2] | 850 | 51 | 523 |
| 2.2 | 758 | 11 | 1 96 |
| 23 | 771 | 1 4 | 1 38 |
| 24 | 771 | i 5 | 1 50 |
| 25 | 588 | 7 | 51 |
| 26 | 748 | 93 | 836 |
| 2.7 | 680 | 103 | 840 |
| 2.8 | 720 | 6 | 50 |
| 29 | 1 679 | ! 8 | 1 64 |
| 30 | 748 | 1 4 | 34 |
| 31 | | | |
| Avg. | 680 | 44 | 360 |

10 drain diverted to west on thell 4/1/74 Off. lechan

MINERALS AND CHEMICAL DIVISION
P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH March YEAR 1974

| | WEST PLANT OUTFALL | | | I | EAST PLANT OUTFALL | | | |
|------|--------------------|---------|---------|---------|--------------------|---------|--|--|
| Day | Gal/Min | ppm P | lbs/day | Gal/Min | ppm P | lbs/day | | |
| _ | | (total) | P | | (total) | P | | |
| 1 | 650 | 192 | 1498 | 70 | 100 | 84 | | |
| 2 | 575 | 154 | 1063 | 70 | 50 | 42 | | |
| 3 | 600 | 237 | 1706 | 70 | 46 | 39 | | |
| 4 | 500 | 71 | 428 | 70 | 39 | 33 | | |
| 5 | 600 | 280 | 2016 | 70 | 14 | 12 | | |
| 6 | 600 | 146 | 1051 | 70 | 105 | 88 | | |
| 7 | 600 | 213 | 1533 | 297 | 49 | 174 | | |
| 8 | 500 | 250 | 1. 1500 | 261 | 1. 11 | 35 | | |
| 9 | 550 | 128 | 845 | 247 | 8 | 25 | | |
| 10 | 550 | 53 | 350 | 247 | 6 | 19 | | |
| 11 | 600 | 51 | 364 | 342 | 6 | 24 | | |
| 12 | 600 | 64 | 460 | 324 | 8 | 29 | | |
| 13 | 400 | 64 | 309 | 324 | 9 | 34 | | |
| 14 | 500 | 47 | 284 | 252 | 8. | 25 | | |
| 15 | 400 | 199 | 955 | 225 | 34 | 90 | | |
| 16 | | | | 2. | 12 | | | |
| 17 | 700 | 191 | 1604 | | 11 | | | |
| 18 | 900 | 57 | 617 | 216 | 7 | 19 | | |
| 19 | 338 | 27 | 109 | 270 | 8 | 27 | | |
| 20 | 397 | 37 | 177 | 252 | 8 | 25 | | |
| 21 | 338 | 21 | 87 | 280 | 11 | 36 | | |
| 22 | 338 | . 23 | 93 | 256 | 11 | 34 | | |
| 23 | 700 | 552 | 4637 | 238 | .8 | 21 | | |
| 24 | 650 | 29 | 227 | 238 | 7 | 19 | | |
| 25 | 367 | 13 | 57 | 238 | 6 | 18 | | |
| 26 | 397 | 12 | 57 | 324 | 7 | 28 | | |
| 27 | 367 | 138 | 608 | 324 | 13 | 52 | | |
| 28 | 462 | 95 | 524 | 288 | 21 | 74 | | |
| 29 | 429 | 217 | 1117 | 202 | 23 | l 55 , | | |
| 30 | | 104 | | 261 | 18 | 56 | | |
| 31 | | 67 | | 270 | 6 | 18 | | |
| Avg. | 522 | 124 | 867 | 225 | 21 | 43 | | |

MINERALS AND CHEMICAL DIVISION
P. D. BOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

| | | • | | |
|-------|----------|-----|------|------|
| MONTH | February | . · | YEAR | 1974 |

| | | T PLANT OUT | | EAST PLANT OUTFALL | | | |
|------|---------|-------------|---------|--------------------|---------|---------|--|
| Day | Gal/Min | ppm P | lbs/day | Gal/Min | ppm P | lbs/day | |
| | | (total) | P | | (total) | P | |
| | 400 | 391 | 1877 | 315 | 57 | 217 | |
| 2 | 450 | 209 | 1129 | 360 | -5 | 20 | |
| 3 | 425 | 61 | 310 | 360 | 4 | 17 | |
| 4 | 550 | 79 | 519 | 31.5 | 5 | 20 | |
| 5 | 550 | 64 | 423 | 324 | 11 | 43 | |
| 5 | 600 | 148 | 1065 | 279 | 16_ | 53 | |
| 7 | 600 | 52 | 376 | 279 | 1.6_ | 55 | |
| 3 | 500 | 71 | 428 | | 12 | 40 | |
| 9 | 650 | 90 | 701 | 275 | 5 | 16 | |
| LO | 525 | 38 | 237 | 225 | 8 | 22 | |
| 11 | 400 | 48 | 230 | 275 | 129 | 426 | |
| 1.2 | 600 | 37 | 263 | 300 | 24 | 88 | |
| 1.3 | 700 | 60 | 501 | 225 | 6 | 15 | |
| 4 | 750 | 5.5 | 496 | 250 | . 7 | 22 | |
| 1.5 | 700 | 46 | 388 | 275 | 13 | 43 | |
| 16 | 725 | 8 | 7.2 | 325 | 5 | 19 | |
| 17 | 725 | 1 | 8 | 325 | 11 | 43 | |
| 1.8 | | | | | | | |
| 19 | 800 | 3 | 25 | 350 | 16 | 69 | |
| 20 | 950 | 29 | 327 | 300 | 14 | 50 | |
| 21 | 450 | 19 | 102 | 320 | 9 | 33 | |
| 22 | 400 | 18 | 85 | 275 | 11 | 35 | |
| 23 | 135 | 86 | 139 | 300 | 13 | 48 | |
| 24 | 375 | 54 | 244 | 300 | 9 | 33 | |
| 25 | 400 | 32 | 155 | 350 | 8 | 34 | |
| 26 | 400 | 90 | 436 | 250 | 38 | 112 | |
| 27 | 400 | 41 | 196 | 300 | 18 | 65 | |
| 28 | 500 | 38 | 230 | | 134 | l | |
| 29 | | | | | | 1 | |
| 30 | | | | | | | |
| 31 | | | | | · | | |
| Avg. | 543 | 69 | 406 | 296 | 21 | 63 | |

MINERALS AND CHEMICAL DIVISION
P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH January YEAR 1974

| | | T PLANT OUT | | | EAST PLANT OUTFALL | | | |
|------|---------|---------------|--------------|---------|--------------------|---------------|--|--|
| Day | Gal/Min | ppm P (total) | lbs/day P | Gal/Min | ppm P (total) | lbs/day P. | | |
| 1 | 350 | 14 | 57 | 158 | 6 | 12 | | |
| 2 | 450 | 1.1 | 59 | 315 | 4 | 14 | | |
| 3 | 500 | | | 315 | 6 | 21 | | |
| 4 | 300 | | | 315 | 9 | 33 | | |
| 5 | | | | 315 | 13 | 49 | | |
| 6 | | | | 360 | 6 | 26 | | |
| 7 | 400 | | | 315 | 4 | 14 | | |
| 8 | 325 | 12 | 46 | 342 | 29 | 12 | | |
| 9 | 500 | 25 | 150 | 342 | 8 | 35 | | |
| 10 | 500 | 170 | 1020 | 342 | 4 | 14 | | |
| 11 | 500 | 59 | 354 | 342 | 280 | 1149 | | |
| 12 | 550 | 279 | 1841 | 333 | 3 | 10 | | |
| 13 | 650 | 116 | 905 | 315 | 40 | 151 | | |
| 1.4 | 200 | 127 | 305 | 243 | 113 | 330 | | |
| 15 | 850 | 170 | 1734 | 315 | 46 | 175 | | |
| 16 | 500 | 255 | 1530 | 320 | 8 | 31 | | |
| 17 | 500 | 233 | 1398 | 315 | 11 | 42 | | |
| 18 | .350 | 36 | 150 | 315 | 17 | 62 | | |
| 19 | 400 | 298 | 1430 | 212 | 66 | 167 | | |
| 20 | 500 | 147 | 882 | 360 | 19 | 83 | | |
| 21 | 300 | 231 | 832 | 342 | 21 | 88 | | |
| 22 | 600 | 127 | 914 | 360 | 14 | 61 | | |
| 23 | 575 | 167 | 1152 | 342 | 8 | 34 | | |
| 24 | 500 | 99 | 595 | 342 | 10 | 43 | | |
| 25 | 550 | 119 | 78,5 | 315 | 11 | 41 | | |
| 26 | 375 | 221 | 994 | 212 | 13 | 33 | | |
| 27 | 525 | 48 | 301 | 252 | 17 | 52 | | |
| 28 | 600 | 119 | 857 | 405 | . 47 | 1226 | | |
| 29 | 400 | 77 | 369 | 342 | 6 | 26 | | |
| 30 | 500 | 5 | 300 | 261 | 28 | 1 89 | | |
| 31 | 400 | 66 | 316 | 202 | 3 | 8 | | |
| Avg. | 471 | 124 | 731 | 309 | 28 | 105 | | |

MINERALS AND CHEMICAL DIVISION
P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH December YEAR 1973

| | WES | T PLANT OUT | FALL | | EAST PLANT OUTFALL | | | |
|------|---------|-------------|---------|---------|--------------------|---------|--|--|
| Day | Gal/Min | ppm P | lbs/day | Gal/Min | ppm P | lbs/day | | |
| _ | | (total) | P | | (total) | P, | | |
| 1 | 450 | 41 | 221 | 270 | 6 | 18 | | |
| 2 | 450 | 14 | 1 76 | 405 | 5 | 23 | | |
| 3 | 575 | 15 | 100 | 342 | 5 | 19 | | |
| 4 | 600 | 22 | 158 | 274 | 6 | 20 | | |
| 5 | 500 | 12 | 71 | 324 | 5 | 19 | | |
| 6 | 825 | 9 | 93 | 279 | 41 | 136 | | |
| 7 | 700 | 4 | 1 37 | 261 | 99 | 310 | | |
| 8 | 400 | 12 | 58 | 405 | 11 | 54 | | |
| 9 | 475 | 7 | 40 | 405 | . 7 | 34 | | |
| 10 | 500 | 3 | 17 | 238 | . 5 | 14 | | |
| 11 | 500 | 10 | 62 | 324 | 5 | 20 | | |
| 12 | 500 | 19 | 115 | 342 | 6 | 25 | | |
| 13 | 500 | 12 | 71 | 342 | 6 | 23 | | |
| 14 | 500 | 42 | 253 | 342 | 6 | 24 | | |
| 15 | 400 | 43 | 206 | 405 | 6 | 28 | | |
| 16 | 300 | 26 | 94 | 486 | ۷, | . 26 | | |
| 17 | 300 | 6 | 20 | 342 | 10 | 42 | | |
| 18 | . 300 | 113 | 407 | 342 | 19 | 80 | | |
| 19 | 300 | 30 | 109 | 342 | 6. | 23 | | |
| 20 | 300 | 25 | 90 | 342 | 3 | 14 | | |
| 21 | 300 | 192 | 691 | 342 | 7 | 28 | | |
| 22 | 450 | 78 | 420 | 450 | 44 | 239 | | |
| 23 | 350 | 256 | 1075 | 360 | 11 | 46 | | |
| 24 | | 1 | į | | | | | |
| 25 | | | | | | | | |
| 26 | 300 | 36 | 131 | 360 | 10 | 43 | | |
| 27 | 425 | 22 | 111 | 243 | 5 | 16 | | |
| 28 | 450 | 59 | 320 | 270 | 16 | 53 | | |
| 29 | 375 | 49 | 219 | 405 | 6 | 31 | | |
| 30 | 300 | 88 | 316 | 405 | 5 | i 26 ' | | |
| 31 | 325 | 5 | 21 | 315 | 7 | 26 | | |
| Avg. | 436 | 43 | 193 | 341 | 13 | 50 | | |

MINERALS AND CHEMICAL DIVISION

P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH November YEAR 1973

| | | LANT OUTFA | | | PLANT OU | | 10" DRAIN |
|------------|------------------|------------|--------------|---------------|----------|--------------|---------------------|
| DAY | ppm P (Total) | Gal/Min | lbs/day P | ppm P (Total) | Gal/Min | lbs/day P | ppm p (Total) ** |
| 1 | 20 | 700 | 167 | 78 | 490 | 460 | |
| 2 | 32 | 800 | 310 | 45 | 490 | 263 | |
| 3 | 5 | 775 | 44 | 19 | 1 575 | 128 | |
| 4 | | 800 | - | 59 | 650 | 463 | |
| 5 | 47 | 850 | 481 | 190 | 540 | 1231 | |
| 6 | 56 | 800 | 537 | 37 | 400 | 178 | |
| 7 | 44 | 750 | 400 | 19 | 400 | 91 | |
| 8 | 217 | 750 | 1953 | 21 | 350 | 86 | |
| 9 | 100 | 700 | 840 | 4 | 310 | 14 | |
| 10 | 44 | 650 | 342 | 7 | 450 | 36 | |
| 11 | 7 | 625 | 53 | 15 | 450 | 79 | |
| 12 | 9 | 675 | 75 | 5 | 310 | 17 | |
| F-13 | 131 | 600 | 943 | 49 | 355 | 210 | |
| 14 | 55 | 500 | 328 | . 5 | 380 | 21 | |
| 15 | 29 | 800 | 275 | 16 | 365 | 68 | |
| F16 | 12 | 1100 | 161 | 2 | 355 | 6 | |
| 18 7 1 | 171 | | _ | 24 | | | |
| 8 | 124 | ! 650 | 967 | +, | 410 | ! - | |
| 19 | 42 | 475 | 239 | 19 | 310 | 69 | |
| 20 | 33 | 500 | 196 | 19 | 360 | 83 | |
| 21 | 12 | 390 | 55 | 3 | 270 | 11 | |
| 22 | 35 | 400 | 167 | 98 | 310 | 364 | |
| 23 | 13 | 400 | 61 | 133 | 270 | 431 | |
| 24 | 5 | 400 | 24 | 164 | 280 | 551 | |
| 25 | 11 | 650 | 85 | 3 | 400 | 13 | |
| 2 6 | 7 | 420 | 35 | 5 | 270 | 15 | |
| 27 | 5 | ! 420 | 25 | 3 | i 280 | 10 | |
| 28 | 46 | 410 | 227 | 4 | 285 | 12 | · |
| 29 | 668 | 480 | 3848 | 3 | 290 | 10 | l |
| 30 | 31 | 450 | 168 | 3 | 280 | 11 | |
| 31 | | | | | 1 | | |
| ve. | 69 | 618 | 464 | . 36 | 375 | 176 | |

The FMC ditch was rerouted October 26, 1973. The east outfall now contains only the water previously reported at the 10" drain, except for occasional spills picked up from the reclaim water system.

MINERALS AND CHEMICAL DIVISION
P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH October YEAR 1973

| | WEST P | LANT OUTFA | | | PLANT OU | | 10" DRAIN |
|-----|------------------|------------|--------------|---------------|----------|--------------|------------------|
| DAY | ppm p (Total) | Gal/Min | lbs/day P | ppm P (Total) | Gal/Min | lbs/day P | ppm P (Total) |
| 1 | 10 | 800 | 96 | 13 | 2430 | 379 | 38 |
| 2 | 19 | 800 | 182 | 20 | 2295 | 551 | 82 |
| 3 | 61 | 800 | 586 | 6 | 2430 | 175 | 10 |
| 4 | 6 | 825 | 59 | 11 | 2295 | 303 | 31 |
| 5 | 15 | 875 | 158 | 7 | 1980 | 166 | 17 |
| 6 | 7 | 750 | 63 | 13 | 2295 | 358 | |
| 7 | 8 | 750 | 72 | 12 | 2430 | 350 | |
| 8 | 94 | 1000 | 1128 | 21 | 2430 | 612 | 34 |
| 9 | 489 | 950 | 5575 | 25 | 2160 | 648 | 458 |
| 10 | 25 | 900 | 270 | 4 | 2295 | 110 | 8 |
| 11 | 12 | 1000 | 144 | 10 | 2160 | 259 | 49 |
| 12 | 7 | 775 | 65 | 5 | 2295 | 138 | 8 |
| 13 | 8 | 650 | 62 | 6 | 1935 | 139 | |
| 14 | 7 | 675 | 57 | 8 | 2655 | 255 | |
| 15 | 3 | 800 | 29 | 3 | 1980 | 71 | 7 |
| , 6 | - | 800 | - | - | 1980 | | _ |
| 17 | 7 | 850 | 71 | 11 | 2295 | 303 | 7 |
| :18 | 8 | 850 | 82 | 3 | 1 2295 | 83 | 9 |
| 19 | 9 | 850 | 92 | 9 | 2295 | 248 | 16 |
| 20 | 5 | 700 | 42 | 7 | 1980 | 166 | _ |
| 21 | 5 | 750 | 47 | 7 | 1845 | 155 | - |
| 22 | 5 | 750 | 43 | 18 | 2000 | 432 | 10 |
| 23 | 18 | 650 | 140 | 19 | 2070 | 472 | 11 |
| 24 | 28 | ! 650 | 219 | 7 | 2160 | 181 | 6 |
| 25 | 20 | 750 | 184 | 6 | 1845 | 126 | 7 |
| 26 | 7 | 775 | 64 | 5 | 340 | 21 | Discontinued |
| 27 | 3 | 725 | ! 29 | 6 | 450 | 32 | -MC dita |
| 28 | 7 | 675 | 57 | 49 | 360 | 210 | removed |
| 29 | 6 | 850 | 56 | 40 | 340 | 164 | |
| 30 | 13 | ! 775 | 117 | 51 | 340 | 209 | |
| 31 | 22 | 700 | 183 | 31 | 340 | 125 | |
| ve. | 31 | 789 | 332 | 14 | 1839 | 248 | 45 |

MINERALB AND CHEMICAL DIVIBION

P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: SeptemberYEAR 1973

| | | | · | | · | | |
|------|--------------------------------------|--------------|---------|-----------------------------------|--|-------------------------------|---|
| | | PLATT CUTFAI | | | PLANT OUTF | | 10" DRAIN |
| DAY | ppm (P ₂ 0 ₅) | | lbs/day | ppm P ₂ O ₅ | | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P ₂ 0 ₅ | (Total) |
| 1 | 62 | 700 | 534 | 13 | 2150 | 344 | |
| 2 | 420 | 725 | 3745 | 67 | 2400 | 1978 . | |
| 3 | | | | |) | | |
| 4 | 30 | 950 | 351 | 10 | 2700 | 315 | 53 |
| 5 | 42 | 1000 | 517 | 13 | 2550 | 408 | 15 |
| 6 | 57 | 820 | 575 | 10 | 2550 | 298 | 8 |
| 7 | 30 | 850 | 314 | 15 _ | 800 | 148 | 7 |
| 8 | 200 | | _ | 50 | 2550 | 1568 | |
| 9 | 340 | 700 | 2927 | 40 | 2300 | 1132 | |
| 10 | 35 | 800 | 344 | 20 | 2550 | 627 | 105 |
| 11 | 28 | 875 | 301 | 14 | 2550 | 439 | 14 |
| .12 | 20 | 750 | 184 | 17 | 2700 | 565 | 18 |
| 13 | 19 | 850 | 199 | 13 | 2550 | 408 | 5 |
| 14 | 17 | 975 | 204 | 15 | 2550 | 470 | 8 |
| 15 | 17 | 650 | 136 | 13. | 2400 | 384 | |
| 16 | 15 | 675 | 125 | 25 | 2200 | 676 | |
| 17 | 18 | 850 | 188 | 16 | 2550 | 502 | 8 |
| 18 | 14 | 875 | 151 | 15 | 2:550 | 470 | 15 |
| 19 | 11 | 850 | 115 | 7 ' | 2:550 | 220 | 17 |
| 20 | 15 | 850 | 157 | 11 | 2 7550 | 345 | 7 |
| 51 | 18 | 850 | 183 · | 13 | 2400 | 384 | 8 |
| 55 | 15 | 700 | 129 | 18 | 2 750 | 609 | <u> </u> |
| 23 | 127 | 675 | 1054 | 28 | 2150 | 740 | |
| 24 | 28 | 800 | 276 | 14 | 2700 | 465 | 19 |
| 25 | 120 | 800 | 1180 | 14 | 2550 | 439 | 23 |
| 26 | 460 | 850 | 4809 (| 15 | 2550 | 470 | 35 |
| 27 | 57 | 750 | 526 | 15 | 2400 | 443 | 18 |
| 58 | 150 | 750 | 1384 | 17 | 2700 | 565 | 23 |
| 29 | 173 | 725 | 1543 | 20 | 2200 | 541 | |
| 30 | 105 | 700 | 904 | 42 | 2500 | 1292 | |
| 31 | 1 | | | | | i | |
| AVE. | 91 | 771 | 823 | 20 | 2 353 | 595 | 21 |

POCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH: August YEAR 1973

| | ेश | | | · | | | | |
|-----|----------|---|--------------|-----------------|---|--------------|---------------------------------------|---|
| | | | PLANT CUTFAL | LL | | PLANT OUTF | | 10" DRAIL |
| | DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| | 1 | 27 | 750 | 243 | 8 | 2700 | 259 | 15 |
| | 2 | 17 | 800 | 163 | 9 | 2700 | 308 | 13 |
| | 3 | 198 | 750 | 1782 | 222 | 2550 | 6793 | 13 |
| | 4 | | 750 | | | 3000 | | |
| | 5 | | | | | | | |
| | . 6 | 57 | 800 | 547 | 8 | 2550 | 245 | 22 |
| | 7 | 61 | 600 | 439 | 11 _ | 2550 | 337 | 11 |
| | - 8 | 18 | 650 | 140 | 7 | 2300 | 193 | 11 |
| | 9 | 12 | 625 | 90 | 5 | 2550 | 153 | 3 |
| | 10 | 25 | 725 | 218 | 8 | 2500 | 240 | 13 |
| | 11 | | | i' | | 1 | | |
| | 12 | | 1 | <u> </u> | | | · · · · · · · · · · · · · · · · · · · | |
| | 13 | 13 | 750 | 117 | 11 | 2350 | 310 | 17 |
| | 14 | 17 | 700 | 143 | 1,3 | 2550 | 398 | 14 |
| | 15 | Ii | 700 | 92 | 9 | 2400 | 259 | 17 |
| | 16 | 55 | 750 | 495 | 25 | 2400 | 720 | 65 |
| • | 17 | 20 15 | 650 | 156 | 13 | 2700 1950 | 421 468 | 24 |
| | 18 | 5 | 440 500 | 79 30 | 20 | 2700. | 259 | |
| | 19 | 10 | <u> </u> | 68 | 8 | 2650 | 477 | 20 |
| ٠. | 50 50 | 53 | 600 650 | 413 | | <u> </u> | 390 | 27 |
| | 52 | 1350 | 725 | 11745 | 13 23 | 2500 2700 | 745 | 38 |
| | 23 | 86 | | 722 | 18 | 2500 | 540 | 42 |
| • | 54 | 87 | 700 1100 | 1148 | 20 | 2450 | 588 | 55 . |
| | 25 | 890 | 700 | 7476 | 13 | 2700 | 42.1 | |
| | 26 | 15 | 400 | 72 | 18 | -1900 | 410 | |
| 1 | 27 | 300 | 750 | 2700 | 102 | 3100 | 3794 | 54 |
| | 58 | 600 | 800 | 5760 | 200 | 2700 | 6480 | 37 |
| | 29 | 110 | 550 | 726 | 27 | 2950 | 956 | 9 |
| ۱ ا | 30 | 33 | 700 | 277 | 15 | 2400 | 432 | 17 |
| . | 31 | 135 | 700 | 1134 | 14 | 2550 | 428 | 17 |
| | AVE. | 156 | 690 | 1369 | 32 | 2555 | 1001 | 24 |

MINERALB AND CHEMICAL DIVIBION P. O. BOX 912 POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: JULY

YEAR 1973

| | | PLANT CUTFAI | | | PLANT OUTF | | 10" DRAI |
|------|--------------------------------------|--------------|---------|--|------------|------------|---|
| DAY | ppm (P ₂ 0 ₅) | | lbs/day | ppm P ₂ O ₅ | | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | ppm P ₂ O ₅ (Total) | Gal/Min | P205 | (Totāl) |
| 1 | 28 | . 525 | 176 | 7 | 2950 | 248 | |
| 2 | 18 | 600 | 130 | 9 | 3500 | 378 - | 15 |
| 3 | 22 | . 695 | 183 | 7 | - | | 2 |
| 4 | | - | - | _ | - | . <u>-</u> | |
| 5 | 16 | 700 | 134 | 6 | 3500 | 252 | |
| 6 | 13 | 900 | 140 | 8 | 2700 | 259 | 11 |
| 7 | 7 | 500 | 42 | 5 | 2500 | 150 | |
| - 8 | 12 | 550 | 79 | 8 | 2700 | 259 | } |
| 9 | 15 | 675 | 122 | 12 | 2950 | 425 | 8 |
| 10 | 14 | 650 | 109 | 7 | 3100 | 260 | 8 |
| . 11 | 15 | 650 | 117 | 13 | 3100 | 484 | 7 |
| .12 | 3 | 650 | 23 | 3 | 3300 | 119 | 6 |
| 13 | 27 | 600 | 194 | 14 | 3700 | 622 | 17 |
| 14 | 55 | 525 | 346 | II. | 3000 | 396 | |
| 15 | 13 | 500 | 78 | - '2 | 2700 | <u> </u> | |
| 16 | 12 | 600 | 86 | II | 3300 | 436 | 11 |
| 17 | .7 | 625 | 53 | 8 | 2750 | 264 | 8 |
| 18 | 8 | 625 | 60 | 9 | 2700 | 292 | 12 |
| 19 | 7 | 650 | 55 | | 2400. | - | 11 |
| 20 | - 1 | 700 | - | 31 | 2400 | . 893 | 169 |
| 21 | 310 | 525 | 1953 | _ | 2500 | - | |
| 22 | 86 | 525 | 542 | - | 2400 | | |
| 23 | 151 | 800 | 1450 | 28 | 2700 | 891 | - |
| 24 | 130 | 725 | 1131 | 7. | 2400 | 202 | 46 |
| 25 | 98 | 800 | 941 | 16 | 2700 | 518 | 27 |
| 26 | 16 | 650 | 125 | 8 | 2400 | 216 | 8 |
| 27 | 70 | 650 | 546 | 7 | 2400 | 202 | 15 |
| 28 | 236 | 590 | 1671 | 9 | 3150 | 340 | |
| 29 | 30 | 600 | 216 | 8 | 2150 | 206 | |
| 30 | 20 | 550 | 132 | 8 | 3500 | 336 | 8 |
| 31 | 139 | 750 | 1251 | 11 | 3100 | 409 | 27 |
| AVE. | 54 | 636 | 417 | 10 | 2848 | 362 | 21 |

MINERALB AND CHEMICAL DIVISION
P. D. QOX 912
POCATELLO, IDAHO 65201

WASTEWATER DATA

MONTH: June YEAR 1973

| F | VECCO : | nz Almi ormani | <u> </u> | 7.00 | | | 701 50457 |
|------|--------------------------------------|----------------|----------|-----------------------------------|------------|---------|---|
| 1 | | PLANT OUTFAL | | | PLANT OUTF | | 10" DRAIN |
| DAY | ppm (P ₂ 0 ₅) | 2 2 /4 2 | lbs/day | ppm P ₂ O ₅ | ! | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | | (Total) | Gal/Min | P205 | (Total) |
| 1 | 44 | 800 | 422 | 66_ | 3500 | 252. | 7 |
| 2 | 32 | 700 | 269 | 9 | 2400 | 259 . | |
| 3 - | 17 | 550 | 112 | 8 | 2950 | 283 | |
| 4 | 17 | 650 | 133 | 12 | 3500 | 504 | 9 |
| 5 | 19 | 975 | 222 | 12 | 3500 | 504 | 9 |
| 6 | | | | 9 | 3300 | 356 | |
| 7 | 13 | 600 | 94 | 8 - | 3700 | 355 | 13 |
| 8 | 17 | 800 | 163 | 8 | 3700 | 355 | 16 |
| 9 | 244 | 800 | 2342 | 13 | 3100 | 484 | |
| 10 | 95 | 430 | 490 | 8 | 2500 | 240 | |
| . 11 | 78 | 575 | 538 | 143 | 3300 | 5663 | 13 |
| .12 | 33 | 475 | 188 | 16 | 3300 | 634 | 5 |
| 13 | 50 | 500 | 300 | 8 | 2700 | 259 | 5 |
| 14 | 112 | 425 | 571 | 11 | 3500 | 462 | 12 |
| 15 | 720 | | _ | 23 | 3500 | 966 | 63 |
| 16 | 1130 | 250 | 3390 | 8 | 3000 | 288 | |
| 17 | 169 | | | 13 | 2650 | 413 | |
| 18 | 1170 | 450 | 6318 | 19 | 3700 | 844 | 35 |
| 19 | 80 | 450 | 432 | 12 | 3500 | 504 | 13 |
| 20 | 25 | 600 | 180 | 8 | 3700 | 355 | 7 |
| 21 | 42 | 450 | 227 | 5 | 3700 | 222 | 6 |
| 22 | 222 | 450 | 1199 | 13 | 3300 | 515 | 11 |
| 23 | 65 | 350 | 273 | 10 | 2500 | 300 | |
| 24 | 27 | 270 | 88 | 13 | 2200 | 343 | - |
| 25 | 8 | 450 | 43 | 9 | 3700 | 400 | 8 |
| 26 | 167 | 450 | 91 | 13 | 3700 | 57 7 | 16 |
| 27 | | - i | | 7 | 3100 | 260 | 9 |
| 58 | 390 | 575 | 2691 | 14 | 3100 | 521 | 8 |
| 29 | 280 | 550 | 1848 | 10 | 3100 | 372 | 8 |
| 30 | 362 | 500 | 2172 | 11 | 3000 | 396 | |
| 31 | | | | | 1 | | |
| AVE. | 201 | 541 | 985 | 15 | 3220 | 596 | 14 |

MINERALS AND CHEMICAL DIVISION
P. D. SOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: May YEAR 1973

| | WEST | PLANT OUTFAL | .T. | EAST | PLANT OUT | PALT. | 10" DRAIN |
|--------------|--------------------------------------|--------------|----------|-----------------------------------|---|---------------------------------------|---|
| DAY | ppm (P ₂ O ₅) | | lbs/day | ppm P ₂ O ₅ | 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | lbs/day | |
| | (Total) | Gal/Min | | (Total) | Gal/Min | P ₂ O ₅ | ppm P ₂ O ₅ (Total) |
| === | | <u> </u> | <u> </u> | | | · · · · · · · · · · · · · · · · · · · | |
| | 120 | 540 | 778 | 6 | 2950 | 212 | 5 |
| 5 | 215 | 550 | 1419 | 2 | 3100 | 744 | 2 |
| 3 | 18 | 650 | 140 | 11 | 2950 | 389 | 6 |
| 4 | 49 | 550 | 323 | 11 | 2950 | 389 | 9 |
| 5 | 54 | 920 | 596 | 15 | 3000 | 540 | |
| 6 | 23 | 310 | 86 | 15 | 3100 | 558 | |
| 7 | 8 | 550 | 53 | 16 _ | 3300 | 634 | 28 |
| 8 | 14 | 700 | 118 | 27 | 3500 | 1134 | 195 |
| 9 | 70 | 600 | 504 | 13 | 3700 | 577 | 20 |
| 10 | 6 | 600 | 43 | 11 | 3500 | 462 | 12 |
| 11 | 24 | 600 | 173 | 9 | 3300 | 356 | 66 |
| .12 | 19 | 1100 | 251 | 7 | 2700 | 227 | |
| 13 | 54 | 490 | 318 | 7 | 2950 | 248 | |
| 14 | 48 | 600 | 346 | 13 | 3300 | 515 | 8 |
| 15 | 62 | 1000 | 744 | 400 | 2700 | 12,960 | 15 |
| 16 | 23 | 750 | 207 | 9 | 3300 | 356 | 8 |
| 17 | 20 | 650 | 156 | 11 | 3300 | 436 | 13 |
| 18 | 16 | 650 | 125 | 8 | 2950 | 283 | 14 |
| 19 | 25 | 700 | 210 | 11 | 3100. | 409 | |
| 20 | 19 | 650 | 148 | 21 | 2950 | 743 | · |
| 51 | 13 | 800 | 125 | 28 | 2700 | 907 | |
| 22 | 11 | 750 | . 99 | 9 | 3100 | 335 | 12 |
| 23 | 18 | 600 | 130 | 9 | 2950 | 319 | 9 |
| 24 | 13 | 800 | 125 | 14 | 3500 | 588 | 25 |
| 25 | 80 | 850 | 816 | 13 | 3500 | 546 | 39 |
| 26 | . 342 | 600 | 2462 | 7 | ·2700 | 227 | |
| 27 | 70 | 700 | 588 | 8 | 2550 | 245 | |
| 28 | | | | | | | |
| 29 | 31 | 1300 | 484 | 12 | 3100 | 446 | 7 |
| 30 | 17 | 850 | 173 | 9 | 3100 | 335 | 9 |
| 31 | 11 | 800 | 106 | 8 | 3500 | 336 | 8 |
| AVE. | 50 | 707 | 395 | 25 | 3110 | 856 | 21 |

MINERALB AND CHEMICAL DIVIBION
P. D. BOX 912
POCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH: April

YEAR 1973

| | | | | | | · | | |
|-----|------|--------------------------------------|--------------|---------|---|------------|--|---|
| | | WEST | PLANT OUTFAI | I | EAST | PLANT OUTF | | 10" DRAIN |
| - 1 | DAY | ppm (P ₂ O ₅) | | lbs/day | ppm P ₂ O ₅ | ! | lbs/day | ppm P ₂ O ₅ (Total) |
| ١ | i | (Total) | Gal/Min | P205 | ppm P ₂ O ₅ (Total) | Gal/Min | P205 | (Total) |
| f | 1 | 97 | 1350 | 1571 | 7 | 2750 | 231 | 11 |
| 1 | 2 | 137 | 325 | 534 | 10 | 3100 | 372 | 18 |
| : [| 3 | 115 | 400 | 552 | 13 | 2400 | 374 | 13 |
| • | 4 | 55 | 450 | 297 | 13 | 3100 | 484 | 15 |
| | 5 | 198 | 500 | 1188 | 17 | 2550 | 520 | 9 |
| : [| 6 | 57 | 450 | 308 | 10 | 3000 | 360 | |
| | 7 | 53 | 640 | 407 | 37 _ | 2950 | 1310 | |
| | 8 | 30 | 640 | 230 | 12 | 2050 | 295 | |
| . | 9 | 25 | 640 | 192 | _ | 3300 | - | 18 |
| - | 10 | 8 | _ | | 8 | 3700 | 355 | 8 |
| ٠ | 11 | 15 | 800 | 144 | 7 | 3700 | 311 | 4 |
| | .12 | 236 | 775 | 2195 | 1.0 | 3500 | 420 | 8 |
| | 13 | 190 | 600 | 1368 | 12 | 3100 | 446 | 25 |
| ٠ | 14 | 72 | 590 | 510 | 8 | 2200 | 211 | |
| . | 15 | 11 | 440 | · 58 | 29 🔪 | 2550 | 887 | |
| | 16 | 12 | 440 | 63 | 6 | 2550 | 184 | 8 |
| : | 17 | 57 | 400 | 274 | 15 | 3300 | 594 | 21 |
| | 18 | 87 | 500 | 522 | 13 | 3100 | 484 | 14 |
| | 19 | 18 | 400 | 86 | 11 | 3500 | 462 | 10 |
| . | 20 · | 27 | 500 | 162 | 8 | 3100 | 298 | 6 |
| | 21 | 48 | 490 | 282 | 10 | 300 | 36 | |
| | 22 | 15 | 270 | 49 | 12 | | 432 | |
| ļ | 23 | 9 | 270 | 29 | 14 | 3000 | 504 | 12 |
| | 24 | 18 | 850 | 184 | 14 | 3400 | 571 | 13 |
| | 25 | . 28 | 850 | 286 | 8 | 3500 | 336 | 6 |
| } | 26 | 12 | 400 | 58 | . 8 | · 2650 | 254 | \/ |
| 1 | 27 | 18 | 600 | 130 | 8 | 2700 | 259 | 5 |
| ļ | 28 | 25 | 760 | 228 | 16 | 2500 | 480 | |
| | 29 | 36 | 1050 | 454 | 8 | 3300 | 317 | |
| 1 | 30 | 17 | 450 | 92 | 8 | 3300 | 317 | 7 |
| | 31 | | | | | | l Lateria de parte de la c | |
| | AVE. | 58 | 580 | 429 | 12 | 2905 | 417 | 11 |

MINERALS AND CHEMICAL DIVISION
P. D. SOX 912
POCATELLO, IDAHO 89201

WASTEWATER DATA

MONTH: MARCH YEAR 1973

| | WEST | PLANT OUTFAL | T | EAST | PLANT OUTF | | 10" DIMIN |
|------|------------|--------------|---------|-----------------------|------------|---------|---|
| DAY | ppm (P205) | | lbs/day | ppm P ₂ 05 | | lbs/day | ppm P ₂ O ₅ |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | ppm P ₂ O ₅ (Total) |
| 1 | 22 | 700 | 185 | 35 | 2550 | 1071 | 10 |
| 2 | 155 | 150 | 279 | 21 | 2400 | 605 · | 46 |
| 3 | 82 | 350 | 344 | 73 | 2400 | 2102 | |
| 14 | 29 | 1100 | 383 | 12 | 2500 | 360 | |
| 5 | 17 | 900 | 184 | 17 | 2550 | 520 | 8 |
| 6 | 17 | 150 | 31 | 17 | 2950 | 602 | 8 |
| 7 | - | 850 | _ | 12 - | 2550 | 367 | 8 |
| 8 | 11 | 350 | 46 | 7 | 3150 | 265 | 7 |
| 9 | 28 | 800 | 269 | 11 | 2550 | 337 | 8 |
| 10 | - | 400 | - | 27 | 2550 | 826 | |
| . 11 | 115 | 1650 | 2277 | 13 | 2700 | 421 | |
| 12 | 108 | 600 | 778 | 15 | 3000 | 540 | 18 |
| 13 | 28 | 1200 | 403 | 13 | 3150 | 491 | 11 |
| 14 | 74 | 200 | 178 | 11* | 3400 | 449 | 17 |
| 15 | 42 | 950 | 479 | 8 | 3400 | 326 | 13 |
| 16 | 18 | 900 | 194 | 9 | 2650 | 286 | 11 |
| 17 | 5.0 | 920 | 552 | 13 | 3100 | 484 | |
| 18 | 115 | 980 | 1352 | 20 | 2550 | 612 | |
| 19 | 48 | 400 | 230 | 19 | 2700 | 616 | 17 |
| 20 | 39 | 600 | 281 | 10 | 2950 | 354 | 6 |
| 51 | 7 | 1200 | 101 | 10 | 3300 | 396 | 8 |
| 22 | 45 | 300 | 162 | 14 | 3300 | 554 | 8 |
| 23 | 75 | 400 | 360 | 13 | 0.5.5.0 | 398 | 17 |
| 24 | 45 | 310 | 167 | 15 | 2300 | 414 | - |
| 25 | 12 | 980 | 141 | 16 | 2050 | 394 | |
| 26 | 6 | 250 | 18 | 7 | 3500 | 294 | 17 |
| 27 | 8 | 375 | 36 | 7 | 3500 | 294 | 7 |
| 28 | 18 | 325 | 70 | 295 | 3100 | 10974 | 5 |
| 29 | 20 | 500 | 120 | 173 | 2950 | 6124 | 11 |
| 30 | 15 | 850 | 153 | 19 | 2700 | 616 | 11 |
| 31 | 252 | 940 | 2843 | 8 | 2750 | 264 | |
| AVE. | 52 | 664 | 435 | 30 | 2831 | 1044 | 12 |

MINERALB AND CHEMICAL DIVIBION
P. D. BOX 912
POCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH: FEBRUARY

YEAR 1973

| | · | | | | | | · |
|------|---|--------------|-------------|---|------------|---------|---|
| | | PLANT OUTFAI | | | PLANT OUTF | | 10" DRAIN |
| DAY | ppm (P ₂ 0 ₅) (Total) | | lbs/day | ppm P ₂ O ₅ (Total) | | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | (Total) |
| 1 | 17 | 275 | 56 | 22 | 2050 | 541 | 78 |
| 2 | 15 | 300 | 54 | 27 | 2950 | 956 | 171 |
| 3 | 39 | 400 | 187 | 65 | 2500 | 1950 | · |
| 4 | 35 | 490 | 206 | 33 | 2150 | 851 | |
| 5 | 17 | 875 | 178 | 50 | 2050 | 1230 | 276 |
| 6 | 50 | 500 | 300 | 65 | 2400 | 1872 | 233 |
| 7 | 27 | 800 | 259 | 18 _ | 2400 | 518 | 58 |
| 8 | 35 | 850 | 357 | 13 | 2400 | 374 | 18 |
| 9 | 135 | 850 | 1377 | 15 | 2500 | 450 | 38 |
| 10 | 168 | 230 | 464 | 18 | 2500 | 540 | |
| . 11 | 244 | 760 | 2225 | 27 | 2400 | 778 | |
| .12 | 145 | 700 | 1218 | . 25 | 2200 | 660 | 39 |
| 13 | 95 | 12 | 13 | 15 | 2550 | 459 | 52 |
| 14 | 35 | 750 | 315 | 18 | 2700 | 583 | 44 |
| 15 | 36 | 775 | 335 | 13 | 2550 | 398 | 13 |
| 16 | 10 | 950 | 114 | 6 | 2550 | 184 | 13 |
| 17 | 30 | 1050 | 378 | , 33 | 2550 | 1010 | |
| 18 | 18 | 310 | 67 | 3 | 2300 | 83 | |
| 19 | | | | | | ! ! | |
| 20 | 16 | 500 | 96 | 18 | 2950 | 637 | 53 |
| 51 | 13 | 700 | 74 | 13 | 3000 | 468 | 34 |
| 55 | 49 | 12 | 7 | 8 | 2700 | 259 | 34 |
| 23 | 23 | 600 | 166 | 19 | 2400 | 547 | 53 |
| 24 | 18 | 80 | 17 | 55 | 2400 | 1584 | |
| 25 | 19 | 400 | 91 | 89 | 2500 | 2670 | |
| 20 | 157 | 250 | 471 | 28 | 2550 | 857 | . 16 |
| 27 | 290 | J. 0 | 35 | 155 | 2650 | 4931 | 46 |
| 58 | 22 | 250 | 66 | 35 | 2550 | 1071 | 10 |
| 29 | | | | | | 1 | 1 |
| 30 | | | | | 1 | i | |
| 31 | -3. | | | | i | i | |
| AVE. | 65 | 507 | 338 | 33 | 2496 | 980 | 67 |

MINERALB AND CHEMICAL DIVIBION
P. D. BOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH:January

YEAR 1973

| | WEST I | PLANT OUTFAI | L | EAST | PLANT OUTF | | 10" DRAI |
|------|--------------------------------------|--------------|---------|-----------------------------------|------------|---------|-----------------------------------|
| DAY | ppm (P ₂ O ₅) | | lbs/day | ppm P ₂ O ₅ | • | lbs/day | ppm P ₂ 0 ₅ |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | (Total) |
| 1 | 92 | 1150 | 1270 | 28 | 2700 | 907 | |
| 2 | 35 | 950 | 399 | 11 | 2550 | 337 | 8 |
| 3 | 215 | . 1000 | 2580 | 3 | 3500 | 126 | 3 |
| 4 | 33 | 1100 | 436 | 11 | 2400 | 317_ | 18 |
| 5 | | 1000 | | | 2950 | | 204 |
| 6 | 1 | 310 | | | 2700 | | |
| 7 | 20 | 930 | 223 | 49 | 2200 | 1294 | |
| 8 | 61 | 950 | 695 | 20 | 2550 | 612 | 105 |
| 9 | 46 | 1200 | 662 | 15 | 2700 | 486 | 13 |
| 10 | 315 | 1000 | 3780 | 20 | 2700 | 648 | 83 |
| 11 | 490 | 950 | 5586 | 14 | 2700 | 454 | 28 |
| · 12 | | 300 | · | | 2550 | | 90 |
| 13 | | 440 | | | 2050 | | |
| 14 | 270 | 1050 | 3402 | 7 | 1850 | 155 | |
| 15 | 170 | 600 | 1224 | 37 | 2300 | 1021 | 200 |
| 16 | 234 | 700 | 1966 | 23 | 2400 | 662 | 35 |
| 17 | 320 | 700 | 2688 | 1.3 | 2400 | 374 | 20 |
| 18 | 44 | 300 | 158 | 11 | 2550 | . 337 | 13 |
| 19 | | 600 | | | 1950 | | 13 |
| 20 | | 800 | | | 2400 | | |
| 21 | 36 | 920 | 397 | 13 | 1850 | 289 | |
| 22 | 38 | 12 | 5 | 17 | 2700 | 551 | 15 |
| 23 | 37 | 1050 | . 466 | 11 | 2550 | 337 | 8 |
| 24 | 62 | 800 | 595 | 12 | 2700 | 389 | 17 |
| 25 | 222 | 350 | 932 | 17 | 2950 | 602 | 44 |
| 26 | | 875 | | | 2700 | | 18 |
| 27 | | 920 | | | 2300 | | |
| 28 | 160 | 810 | 1555 | 15 | 2550 | 459 | |
| 29 | 60 | 175 | 126 | 11 | 2550 | 337 | 8 |
| 30 | 78 | 200 | 187 | 17 | 2550 | 520 | 18 |
| 31 | 44 | 700 | 370 | 35 | 2550 | 1071 | 151 |
| AVE. | 134 | 723 | 1291 | 18 | 2482 | 487 | 51 |

MINERALS AND CHEMICAL DIVISION
P. D. SOX 912
PDCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH: December YEAR 1972

| | | | PLANT OUTFAI | T | EAST | PLANT OUTF | ALL | 10" DRAIN |
|-----|------|------------|--------------|---------|-----------|------------|----------|---|
| - | DAY | ppm (P205) | | lbs/day | ppm. P205 | | lbs/day | ppm P ₂ O ₅ (Total) |
| L | | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | (Total) |
| | 1 | 1 | 1000 | | | 2550 | - | 33 |
| | 5 | - | 540 | - | - | 2550 | <u> </u> | |
| L | 3 | 380 | . 230 | 1049 | 18 | 2400 | 518 | |
| | 4 | 20 | 925 | 222 | - | 2400 | _ | 48 |
| L | 5 | | 545 | - | 28 | 2200 | 739 | 74 |
| | 6 | | | | 18 | 2400 | 518 | 52 |
| | 7 | 670 | _ | - | 24 | 2400 | 691 | 37 |
| | 8 | - | 500 | - | 25 | 2400 | 720 | 112 |
| | 9 | | | | 2 | 2700 | 65 | |
| | 10 | 1 | | | 16 | 2700 | 518 | |
| | 11 | 1270 | - | _ | 20 | 2550 | 612 | 15 |
| | 1.2 | 570 | 475 | 3249 | 20 | 2700 | 648 | 5 |
| . [| 13 | 98 | 700 | 823 | 17 % | 2550 | 520 | 5 |
| | 14 | 65 | 700 | 546 | 18 | 2700 | 583 | 7 |
| . C | 15 | 20 | 650 | 156 | 13 | 2700 | 421 | 28 |
| | 16 | 25 | 920 | 276 | 11 | 3000 | 396 | |
| | 17 | 178 | 760 | 1623 | 27 | 2950 | 956 | |
| | 18 | 153 | 800 | 1469 | 24 | 2700 | 778 | 43 |
| | 19 | 87 | 900 | 940 | 59 ′ | 2650 | 1876 | 16 |
| | 20 | 25 | 1200 | 360 | 18 | 2400 | 518 | 53 |
| L | 21 | 30 | 1450 | 522 | 18 | 2700 | 583 | 31 |
| | 22 | 157 | 1400 | 2638 | 11 | 2700 | 356 - | 15 |
| | 23 | 20 | 920 | 221 | 5 | 2550 | 153 | |
| | 24 | 35 | 700 | 294 | 10 | 3300 | 396 | |
| | 25 | | · | | | | | |
| | 26 | 27 | 1125 | 364 | 11 | 2300 | 304 | 13 |
| L | 27 | 27 | 1150 | 373 | 20 | 2400 | 576 | 15 |
| | 28 | 64 | 300 | 230 | 19 | 2300 | 524 | 15 |
| | 29 | 160 | 1150 | 2208 | 23 | 2650 | 731 | 97 |
| | 30 | 440 | 700 | 3696 | 27 | 2700 | 875 | |
| | 31 | _ | | - | - | 2700 | _ | |
| | AVE. | 206 | 822 | 1063 | 19 | 2597 | 599 | 36 |

MINERALB AND CHEMICAL DIVIBION
P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: November YEAR 1972

| | WEST | PLANT OUTFA | IL | · · · · · · · · · · · · · · · · · · · | PLANT OUTF | | 10" DRAIN |
|----------------|--------------------------------------|-------------|---------|--|------------|---------|---|
| DAY | ppm (P ₂ 0 ₅) | | lbs/dey | ppm P205 | 1 | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | ppm P ₂ O ₅ (Total) | Gal/Min | | 1 |
| 1 | 13 | 920 | 143 | 10 | 3100 | 372 | 9 , |
| 2 | 41 | 1075 | 529 | 9 | 2750 | 297 | 7 |
| 3 | 15 | . 1375 | 248 | 13 | 2950 | 460 | 65 |
| J [†] | 57 | 700 | 479 | 23 | 300 | 83 | |
| 5 | 34 | 700 | 286 | 17 | 300 | 61 | |
| 6 | 11 | 950 | 125 | 13 | 2700 | 421 | 41 |
| 7 | 30 | 900 | 324 | 14 | 2950 | 496 | 42 |
| 8 | 33 | 1275 | 505 | 183 | 2950 | 6478 | 7 |
| 9 | 8 | 850 | 82 | 14 | 3000 | 504 | 3.3 |
| 10 | 11 | 900 | 119 | 13 | 2950 | 460 | 20 |
| 1.1. | 11 | 1100 | 145 | 16 | 2400 | 461 | |
| 1.2 | 15 | 760 | ; 137 | 13 | 2550 | 398 | |
| 13 | 15 | 900 | 162 | 13 | 2550 | 398 | 13 |
| 14 | 17 | 500 | 102 | 13 % | 2550 | 398 | 12 |
| 15 | 17 | 600 | 122 | 10 | 2700 | 324 | 8 |
| 16 | 33 | 550 | 218 | 11 | 2750 | 363 | 3 |
| 17 | 25 | 500 | 150 | 9 | 2550 | 275 | 13 |
| 18 | 27 | 1050 | 340 | 11 | 2500 | 330 | |
| 19 | 193 | | 1621 | 11 | 2700 | 356 | |
| 20 | 32 | 700 | 269 | 13 | 2700 | 421 | 18 |
| 21 | 18 | 925 | 200 | 8. | 2700 | 259 | 8 |
| 22 | 8 | 1175 | 113 | 13 | 2700 | 421 | 7 |
| 23 | Holiday | | T | | | | <u></u> |
| 24 | 115 | | 1140 | 13 | 2700 | 421 | 36 |
| 25 | 86 | 490 | 506 | 1.3 | 2700 | 421 | |
| 26 | 20 | 800 | 192 | 17 | 2550 | 520 | |
| 27 | 8 | 700 | 67 | 8 | 2500 | 240 | 11 |
| 29 | 92 | 725 | 800 | 12 | 2550 | 367 | 11 |
| 29 | 162 | 600 | 1170 | 12 | 2550 | 367 | 18 |
| 30 | 123 | 1000 | 1480 | 8 | 2700 | 259 | 15 |
| 31 | | | | | 1 | | |
| AVE. | 44 | 836 | 406 | 18 | 2536 | 573 | 19 |

P. O. GOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: October YEAR 1972

| ~~~ | WEST | PLANT OUTFAI | | | EAST PLANT OUTFALL | | | |
|-----------------------|---|--------------|-----------------|--|--------------------|-----------------|--|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | |
| 1 | 8 | 920 | 88 | 10 | 3100 | 372 | 2.1 | |
| 2 | 10 | 675 | 81 | 12 | 2950 | 425 | 16 | |
| 3 | 10 | . 575 | 69 | 11 | 3000 | 363 | 2 | |
| | 18 | 675 | 146 | 12 | 3300 | 475 | 17 | |
| 5 | lii | 900 | 110 | 12 | 3300 | 475 | 15 | |
| 6 | 3 | 850 | 31 | + 7 | 3300 | 277 | 48 | |
| $\frac{\tilde{7}}{7}$ | 3 | 840 | 30 | 13 | 2950 | 460 | 15 | |
| 8 | 6 | 840 | 61 | 20 | 3180 | 763 | <u> </u> | |
| | 362 | 800 | 3475 | 26 | 3000 | 936 | 61 | |
| 10 | 57 | 745 | 510 | 17 | 3150 | 643 | 44 | |
| 11 | 16 | 750 | 144 | 13 | 3000 | 468 | 17 | |
| 12 | 18 | 675 | 146 | 13 | 3100 | 484 | 8 | |
| 13 | 13 | 735 | 147 | $\frac{1}{12}$ | 2700 | 389 | 7 | |
| 14 | 63 | 1170 | 855 | 13 % | 2550 | 398 | | |
| 15 | 44 | 920 | 486 | 111 | 3000 | 363 | | |
| 16 | 33 | 760 | 301 | 8 | 3000 | 288 | 8 | |
| 17 | 14 | 950 | 160 | 8 | 2950 | 283 | 6 | |
| 18 | 20 | 1050 | 252 | 15 | 2750 | 495 | 17 | |
| 19 | 27 | 730 | 237 | 27 - | 3100 | 1004 | 104 | |
| 20 | 11 | 975 | 118 | 25 | 2750 | 825 | 65 | |
| 21 | 5 | 920 | 55 | 15 | 3100 | 558 | | |
| 22 | 123 | 980 | 1446 | 17 | 3100 | 632 | | |
| 23 | Holiday- | | | | <u> </u> | | | |
| 24 | 15 | 950 | 171 | 11 | 3000 | 363_ | 8 | |
| 25 | 26 | 900 | 280 | | 3400 | 411 | 11 | |
| 26 | 19 | 900 | 205 | 11 | 3300 | 399 | 7 | |
| 27 | 11 | 950 | 115 | 13 | 2700 | 421 | 20 | |
| 28 | 49 | 590 | 347 | 11 | 2750 | 333 | <u></u> | |
| 29 | 23 | 640 | 177 | 15 | 1950 | 351 | 1 | |
| 30 | 20 | 1300 | 312 | 8 | 2950 | 283 | 21 | |
| 31 | 16 | 900 | 173 | 8 | 2700 | 259 | 9 | |
| AVE. | 35 | 852 | 359 | 14 | 2970 | 473 | 24 | |

MINERALS AND CHEMICAL DIVISION
P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: September YEAR 1972

| | WEST I | PLANT OUTFAL | | | PLANT OUTF | | 10" DRAIN |
|------|------------|--------------|---------|----------|------------|---------|---|
| DAY | ppm (P205) | . ! | lbs/day | ppm P2O5 | ! | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | (Total) |
| 1 | 1.63 | 1175 | 2298 | 18 | 2750 | 594 | 13 |
| 5 | 42 | 1050 | 529 | 15 | 2700 | 486 | |
| 3 | 83 | 1050 | 1046 | 7 | 1950 | 164 | <u> </u> |
| 4 | Holidar | | | Holiday | 1 | | <u> </u> |
| 5 | 127 | 1000 | 1524 | 11 | 3000 | 396 | 13 |
| 6. | 17 | 925 | 189 | Ą | 3000 | 144 | 5 |
| 7 | 18 | 925 | 200 | 8 | 2950 | 283 | 7 |
| 8 | 53 | 1025 | 652 | 13 | 2950 | 460 | 12 |
| 9 | No Sam | | | No Sampl | e | \ | |
| 10 | 18 | 750 | 162 | 8 | 3100 | 298 | <u> </u> |
| 11 | 30 | | 405 | 12 | 2700 | 389 | 29 |
| 12 | 11 | 950 | 125 | 10 | 2750 | 330 | 11 |
| 13 | 11 | 1100 | 145 | 78 | 2650 | 2480 | 7 |
| 14 | 16 | 925 | 178 | 36 ` | 3500 | 1512 | 8 |
| 15 | . 390 | 825 | 3861 | 13 | 2950 | 460 | 16 |
| . 16 | 42 | 1350 | 680 | 17 | 3100 | 632 | 1 |
| 17 | 15 | 1250 | 225 _ | 8 | 2700 | 259 | 1 |
| 18 | 215 | 1225 | 3160 | 15 | 2700 | 486 | 25 |
| 19 | 33 | | 317 | 8 | 2700 | 259 | 8 |
| 20 | · 18 | 825 | 178 | 11 | 2950 | . 389 | 23 |
| 21 | 13 | 865 | 141 | 9 | 2750 | 297 | 11 |
| 22 | 6 | 875 | 63 | 7 | 2750 | 231 | 8 |
| 23 | 5 | 840 | 50 | 7 | 2050 | 172 | |
| 24 | 8 ; | 920 | 88 | 8 | 2050 | 197 | |
| 25 | 15 | 850 | 153. | 13 | 1750 | 273 | 37 |
| 26 | 1270 | 800 | 12192 | 33 | 2700 | 1069 | 154 |
| 27 | 180 | 825 | 1782 | No Sampl | e | ! ; | 92 |
| 28 | 50 | 850 | 510 | 11 | 3300 | 436 | 15 |
| 29 | 48 | 740 | 426 | 8 | 3300 | 317 | 11 |
| 30 | 18 | 980 | 212 | 12 | 3150 | 454 | |
| 31 | | | | | 1 | 1 | |
| AVE. | 104 | 958 | 1125 | 15 | 2774 | 499 | 25 |

MINERALB AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: August YEAR 1972

| | | PLANT OUTFAI | Ţ | EAST | PLANT OUTF | ALL | 10" DRAIN |
|------|---|--------------|------------------------------|--|------------|------------------------------|---|
| DAY | ppm (P ₂ 0 ₅) (Total) | Gal/Min | lbs/day P ₂ 05 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ 05 | ppm P ₂ O ₅ (Total) |
| 1 | 55 | 920 | 607 | 11 | 2700 | 356 | 15 |
| 2 | 23 | 775 | 214 | 15 | 2700 | 486 | 17 |
| 3 | 11 | . 825 | 109 | 13 | 2650 | 413 | 17 |
| 74 | 24 | 700 | 202 | 19 | 2500 | 570 | 20 |
| 5 | 18 | 1100 | 238 | 16 | 3100 | 595 | |
| 6 | 25 | 920 | 276 | 204 | 3100 | 7589 | |
| 7 | 15 | 250 | 45 | 15 | 2200 | 396 | 25 |
| _ 8 | 13 | 800 | 125 | 11 | 2400 | 317 | 11 |
| 9 | 25 | 575 | 173 | 20 | 2950 | 708 | 27 |
| 10 | 8 | 600 | 58 | 11 | 3000 | 396 | 15 |
| 11 | 8 | 750 | 72 | 35 | 2650 | 1113 | 18 |
| 12 | 15 | 780 | 140 | 58 | 4300 | 2993 | |
| 13 | 215 | 980 | 2528 | 8 , | 2200 | 211 | |
| 14 | 950 | 600 | 6840 | 75 `` | 2650 | 2385 | 180 |
| 15 | 170 | 600 | 1224 | 11 | 2750 | 363 | 23 |
| 16 | 27 | 825 | 267 | 11 | 2950 | 389 | 15 |
| 17 | 20 | 650 | 156 . | 8 | 2950 | 283 | 11 |
| 18 | 15 | 575 | 104 | 15 | 2950 | 531 | 23 |
| 19 | 40 | 760 | 365 | 8 | 1900 | 182 | |
| 20 | 86 | 1170 | 1207 | 11 | 3300 | 436 | |
| 21 | 80 | | | 13 | 2550 | 398 | 8 |
| 22 | 17 | 650 | 133 | 15 | 2750 | 495 | 48 |
| 23 | 18 | 750 | 162 | 236 | 2550 | 7222 | 151 |
| . 24 | 11 | 1150 | 152 | 20 | 2950 | 708 | 92 |
| 25 | 13 | 875 | 137 | 25 | 33.00 | 930 | 198 |
| 26 | 18 | 980 | 212 | 42 | 3400 | 1714 | |
| 27 | 23 | 640 | 177 | . 25 | 3400 | 1020 | |
| 28 | 35 | 790 | 332 | 13 | 3150 | 491 | 33 |
| 29 | 37 | 1000 | 444 | 18 | 2950 | 637 | 70 |
| 30 | 25 | 950 | 285 | 70 | 3000 | 2520 | 440 |
| 31 | 147 | 800 | 1411 | 17 | 3100 | 632 | 65 |
| AVE. | 71 | 791 | 613 | 34 | 2865 | 1209 | 66 |

MINERALS AND CHEMICAL DIVIBION
P. D. BOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: JULY YEAR 1972

| | | PLANT OUTFAI | L | EAST | PLANT OUTF | | 10" DRAIN |
|------|---|--------------|-----------------|--|------------|-----------------|---|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | 15 | 920 | 166 | 18 | 2950 | 637 | 12 |
| 2 | 15 | 1050 | 189 | 18 | 3100 | 670 | |
| 3 | 8 | 650 | 62 | 11 | 2300 | 304 | 7 |
| 4 🐟 | Holiday | | | Holiday | t . | | |
| 5 | 13 | 590 | 92 | 11 | 2750 | 363 | 5 |
| 6 | 25 | 975 | 293 | 11 | 3100 | 409 | • 7 |
| 7 | 13 | 750 | 117 | 11 | 3150 | 416 | 5 |
| 8 | 15 | 920 | 166 | 13 | 2700 | 421 | |
| 9 | 8 | 700 | 67 | 13 | 2700 | 421 | |
| 10 | 8 | 1200 | 115 | 13 | 2700 | 421 | 5 |
| 11 | 18 | 1150 | 248 | 13 | 3100 | 484 | 8 |
| 12 | 11 | 350 | 46 | 17 | | 541 | 5 |
| 13 | 46 | 1175 | 649 | 17 | 2650 | 541 | 15 |
| 14 | 15 | 625 | 113 | 11 > | 2400 | 317 | 5 |
| 15 | 15 | 1050 | 189 | 13 | 2950 | 460 | |
| 16 | | no flow | _ | 13 | 2750 | 429 | |
| 17 | 11 | 1050 | 139 | 17 | 2550 | 520 | 11 |
| 18 | 23 | 675 | 186 | 15 | 3100 | 558 | 13 |
| 19 | 135 | 600 | 972 | 17 | 2650 | 541 | 5 |
| 20 | 139 | 1090 | 1818 | 15 | 3100 | . 558 | 28 |
| 21 | 57 | 200 | 137 | 8 | 2750 | 363 | 13 |
| 22 | 25 | 1170 | 351 | 14 | 3500 | 588 | |
| 23 | 65 ' | 1050 | 819 | 11 | 3500 | 462 | |
| 24 | 27 | 1325 | 429 | 11 | | 363 | 11 |
| 25 | 17 | 1060 | 216 | 18 | 2700 | 583 | 17 |
| 26 | 20 | 975 | 234 | 18 | 2750 | 594 | 17 |
| 27 | 15 | 1125 | 203 | 17 | 2950 | 602 | 15 |
| 58 | 13 | 1075 | 168 | 8 | 2950 | 283 | 17 |
| 29 | 35 | 700 | 294 | 8 | 3300 | 317 | |
| 30 | 160 | 700 | 1344 | 17 | 3550 | 724 | |
| 31 | 42 | 625 | 315 | 27 | 3000 | 972 | 25 |
| AVE. | 34 | 880 | 350 | 14 | 2940 | 495 | 12 |

MINERALB AND CHEMICAL DIVIBION
P. D. BOX 912

POCATELLO, IDAHO 93201

WASTEWATER DATA

MONTH: June YEAR 1972

| | WEST | PLANT OUTFA | LL | | EAST PLANT OUTFALL | | | |
|------|---|-------------|-----------------|--|--------------------|------------------------------|---|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ . (Total) | Gal/Min | lbs/day P ₂ 05 | ppm P ₂ O ₅ (Total) | |
| l | 5 | 815 | 49 | 11 | 2550 | 336 | 18 | |
| 2 | 17 | 800 | 163 | 20 | 31.50 | 756 | 23 | |
| 3 | 83 | No flow | 1 – | 46 | 31.00 | 1711 | | |
| 4 | 278 | 11 | - | 18 | 3500 | 756 | | |
| 5 | 102 | 11 | - | 17 | 2700 | 551 | 23 | |
| 6 | 42 | 475 | 239 | 15 | 2950 | 531 | 53 | |
| 7 | 65 | 1100 | 858 | 15 | 2950 | 531 | 86 | |
| 8 | 72 | 525 . | 454 | 17 | 3100 | 632 | 108 | |
| 9 | 34 | 575 | 235 | 25 | 2900 | 870 | 30 | |
| 10 | 13 | 800. | 125 | 17 | 2900 | 592 | | |
| 11 | 11 | 1600 | 211 | 13 | 3300 | 515 | | |
| 12 | 33 | 575 | 228 | 1.1 | 2950 | 390 | 7 | |
| 13 | 472 | 1050 | 5947 | 50. | 8500 | 2100 | 27 | |
| 14 | 147 | 575 | 1014 | 18 | 3400 | 734 | 72 | |
| 15 | 18 | 1.000 | 216 | 27 | 2400 | 778 | 173 | |
| 16 | 17 | 25 | 5 | 17 | 2400 | 490 | 46 | |
| 17 | 15 | 700 | ; 126 | 20 | 3100 | 744 | | |
| 18 | 53 | 800 | 509 | 11 | 3300 | 436 | | |
| 19 | 17 | 3000 | 612 | 18 | 2650 | 572 | 8 | |
| 20 | 18 | 5200 | 1123 | . 13 | 2300 | 359 | 17 | |
| 21 | 11 | 5200 | 686 | 11 | 2500 | 330 | 11 | |
| 22 | 408 | | 4896 | 11 | 2400 | 317 | 17 | |
| 23 | 1050 | 950 | 11970 | 35 | 2550 | 1113 | 230 | |
| 24 | 70 | 700 | 588 | 20 | 2400 | 576 | | |
| 25 | - | - | - | 13 | 2400 | 374 | | |
| 26 | 15 | 800 | 144 | 15 | 2050 | 369 | 17 | |
| 27 | 13 | 590 | 92 | 13 | 2650 | 413 | 8 | |
| 28 | 11 | 500 | 66 | 13 | 3000 | 468 | II | |
| 29 | 18 | 500 | 108 | 15 | 3150 | 567 | 8 | |
| 30 | 17 | 550 | 112 | 11 | 3400 | 449 | II | |
| 31 | | | 1 | | 1 | | | |
| AVE. | 108 | 1048 | 1184 | 19 | 2820 | 645 | 46 | |

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: MAY YEAR 1972

| | | PLANT OUTFAI | L | EAST | PLANT OUTF | | 10" DRAIN |
|------|--------------------------------------|--------------|---------|-----------------------------------|------------|---------|---|
| DAY | ppm (P ₂ O ₅) | | lbs/day | ppm P ₂ O ₅ | ! | lbs/day | ppm P ₂ O ₅ (Total) |
| | (Total) | Gal/Min | P205 | (Total) | Gal/Min | P205 | (Totāl) |
| 1 | 20 | 800 | 192 | 37 | 2550 | 1132 | 210 |
| 2 | 25 | 1260 | 378 | 15 | 2300 | 414 | 13 |
| 3 | 20 | 1050 | 252 | 39 | 2200 | 1030 | 193 |
| 14 | 27 | 1040 | 337 | 67 | 2500 | 2010 | 405 |
| 5 | 23 | 1000 | 276 | 42 | 2300 | 1159 | 169 |
| 6 | 23 | 1450 | 400 | 28 | 2750 | 924 | |
| 7 | 151 | 1600 | 2899 | 27 | 2750 | 891 | |
| 8 | 46 | 1050 | 580 | 25 | 2650 | 795 | 130 |
| 9 | 30 | · 975 | 351 | 25 | 3000 | 900 | 130 |
| 10 | 28 | 725 | 244 | 25 | 2750 | 825 | 151 |
| 11 | 25 | 925 | 278 | 15 | 2700 | 486 | 20 |
| 12 | 29 | 660 | 230 | 25 | 2550 | 765 | 78 |
| 13 | 67 | 840 | 676 | 50 | 3100 | 1860 | |
| 14 | 44 | 1050 | 554 | 15 | 2150 | 387 | |
| 15 | 70 | 1075 | 903 | 92 | 2400 | 2649 | 570 |
| 16 | 39 | 1150 | 538 | 30 | 2200 | 792 | 210 |
| 17 | 30 | 1025 | 369 | 11 | 2700 | 356 | 12 |
| 18 | 53 | 915 | 582 | 15 | 2500 | 450 | 42 |
| 19 | 120 | 1050 | 1512 | 13 | 2400 | 374 | 67 |
| 20 | 53 | 920 | 585 | 11 | 2700 | 356 | |
| 21 | 53 | 1050 | 668 | 33 | 2750 | 1089 | |
| 22 | 35 | 940 | 395 | 184 | 2650 | 5851 | 1930 |
| 23 | 70 | 775 | 651 | 18 | 2550 | 551 | 115 |
| 24 | 13 | 775 | 121 | 11 | 2950 | 425 | 3 |
| 25 | 30 | 660 | 238 | 11 | 2750 | 363 | 3 |
| 26 | 24 | 550 | 158 | 17 | 2950 | 602 | 7 |
| 27 | 20 | 920 | 221 | 17 | 3300 | 673 | |
| 28 | 18 | 980 | 212 | | 2750 | 429 | |
| 29 | 13 | 655 | 102 | 18 | 2700 | 583 | 86 |
| 30 | 27 | 780 | 253 | 17 | 2500 | · 510 | 13 |
| 31 | 13 | 875 | 137 | 17 | 2550 | 520 | 53 |
| AVE. | 40 | 952 | 493 | 31 | 2631 | 973 | 200 |

MINERALB AND CHEMICAL DIVIBION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: April YEAR 1972

| | | | PLANT OUTFAI | | EAST | PLANT OUTF | | 10" DRAIN |
|------------|------|---|--------------|-----------------|---------------------|------------|-----------------|--|
| | DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P205 (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| | l | 20 | 640 | 154 | 18 | 31.00 | 670 | |
| 1 | 5 | 17 | 640 | 131 | 8 | 2750 | 264 | |
| ال | 3 | 20 | 670 | · 161 | 30 | 2550 | 918 | 165 |
| L | 4 | 7 | 740 | 62 | 39 | 2650 | 1240 | 315 |
| - L | 5 | 196 | 675 | 1588 | 20 | 2300 | 552 | 86 |
| L | 6 | 115 | 800 | 1104 | 27 | 2550 | 826 | 135 |
| $^{-}$ [| 7 | 61 | 850 | 622 | 111 | 2550 | 3397 | 244 |
| . [| 8 | 315 | 50 | 189 | 48 | 2700 | 1555 | |
| | 9 | 25 | 640 | 192 | 27 | 2950 | 956 | |
| - [| 10 | 120 | 580 | 835 | 53 | 2550 | 1622 | 390 |
| | 11 | 156 | 700 | 1310 | 60 | 2500 | 1800 | 246 |
| | 12 | 305 | 925 | 3384 | 89 | 2750 | 2937 | 672 |
| . | 13 | 127 | 690 | 1052 | 78 | 2750 | 2574 | 86 . |
| ſ | ′14 | 62 | 700 | 521 | 11 | 2500 | 330 | 30 |
| - [| 15 | 35 | 760 | 319 | 15 | 2700 | 416 | |
| _ | 16 | 35 | 700 | 294 | 17 | 3000 | 612 | |
| ٦ | 17 | 70 | 775 | 651 | 35 | 2550 | 1071 | 236. |
| . [| 18 | 44 | 1190 | 628 | 37 | 2550 | 1132 | 254 |
| ` - - | 19 | 25 | 800 | 240 | 65 | 2550 | 1989 | 286 |
| ٠ ٢ | 20 | 11 | 625 | 83 | 17 | 2700 | 551 | 127 |
| Γ | 21 | 65 | 600 | 468 | 50 | 2400 | 1440 | 430 |
| | 22 | 23 | 105 | 29 | 57 | 2700 | 1847 | |
| | 23 👁 | 33 | 700 | 277 | 62 | 3150 | 2344 | |
| Γ | 24 | 280 . | 715 | 2402 | 48 | 2300 | 1325 | 100 |
| : | 25 | 246 | 1150 | 3395 | 25 | 2150 | 645 | 123 |
| | 26 | 127 | 1350 | 2057 | 28 | 2400 | 806 | 108 |
| - - | 27 | 48 | 1400 | 403 | 17 | 2200 | 224 | 95 |
| ٦, | 28 | 25 | 1400 | 210 | 18 | 2300 | 248 | 53 |
| | 29 | 20 | 920 | 110 | 13 | 2700 | 211 | |
| , | 30 | 15 | 920 | 83 . | 17 | 2700 | 275 | |
| Ĺ | 31 | | | | | | 1 | 1 |
| | AVE. | 88 | 781 | 766 | 68 | 2607 | 1162 | 209 |

MINERALB AND CHEMICAL DIVIBION ...

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: MARCH YE

YEAR 1972

| | WEST | PLANT OUTFAI | | EAST | PLANT OUTF | | 10" DRAIN |
|------|---|--------------|-----------------|--|------------|-----------------|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | 70 | 750 | 630 | 460 | 2750 | 15180 | 224 |
| 2 | 150 | 835 | 1503 | 300 | 2750 | 9900 | 65 |
| 3 | 85 | 790 | 805 | 25 | 2550 | 765 | 70 |
| 4 | 39 | 105 | 49 | 23 | 2950 | 814 | |
| 5 | 30 | 840 | 302 | 15 | 2650 | 477 | |
| 6 | 46 | 725 | 400 | 17 | 2750 | 561 | 30 |
| 7 | 102 | 1015 | 1242 | 15 | 2650 | 477 | 42 |
| 8 | 178 | 740 | 1580 | 35 | 2750 | 1155 | 130 |
| 9 | 570 | 700 | 4788 | 83 | 2750 | 2739 | 780 |
| 10 | 405 | 950 | 4617 | 127 | 2950 | 4495 | 472 |
| 11 | 570 | 760 | 5198 | 102 | 2700 | 3304 | |
| 3.2 | 1120 | ·200 | 2688 | 130 | 2750 | 4290 | |
| 13 | 550 | 835 | 551.1 | 39 | 2700 | 1.263 | 120 |
| J)! | 44 | 740 | 390 | 25`\ | 2550 | 765 | 53 |
| 15 | 135 | 830 | 1344 | 42 | 2950 | 1486 | 150 |
| 16 | 74 | 855 | 759 | 88 | 2700 | 2851 | 420 |
| 17 | 70 | 935 | 785 | 42 | 2950 | 1486 | 166 |
| 18 | 268 | 1250 | 4020 | 39 | 2700 | . 1263 | |
| 19 | 50 | 930 | 558 | 74 | 3100 | 2752 | |
| 20 | 166 | 800 | 1593 | 172 | 2400 | . 4953 | 460 |
| 21 | 57 | 865 | 591 | 39 | 2650 | 1240 | 160 |
| 22 | 30 | 755 | 271 | 28 | 2700 | 907 | 86 |
| 23 | 55 | 1090 | 719 | 67 | 2550 | 2050 | 346 |
| 24 | 125 | 750 | 1125 | 23 | · 2650 | 731 | |
| 25 | 103 | 800 | 988 | 27 | 2400 | 777 | |
| 26 | 23 | 700 | 193 | 20 | 2550 | 612 | |
| 27 | 28 | 845 | 283 | 15 | 2200 | 396 | 50 |
| 28 | 48 | 980 | 493 | 15 | 2700 | 486 | 46 |
| 29 | 30 | 825 | 297 | 13 | 2950 | 460 | 27 |
| 30 | 20 | 870 | 208 | 20 | 2550 | , 612 | 95 |
| 31 | 23 | 1250 | 345 | 15 | 2400 | 432 | |
| AVE. | 170 | 817 | 1428 | 69 | 2687 | 2248 | 181 |

MINERALB AND CHEMICAL DIVIBION P. O. BDX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: February YEAR 1972

| | WEST | PLANT OUTFA | LL | EAST | PLANT OUTF | 'ALL | 10" DRAIN |
|------|---|-------------|----------|--|------------|------------------------------|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P2 ⁰ 5 | ppm P ₂ O ₅ (Total) |
| 1 | 60 | 920 | 662.4 | 11 | 2650 | 349.8 | 46 |
| 2 | 25 | 980 | 294.0 | 13 | 2700 | 421.2 | 53 |
| 3 | 33 | 1050 | 415.8 | 8 | 2750 | 264.0 | 39 42 |
| 4 | 25 | 980 | 294.0 | 15 | 2650 | 477.0 | 42 |
| 5 | 57 | 1100 | 752.4 | 17 | 2700 | 440.8 | |
| 6 | 80 , | 840 | 806.4 | 11 | 2500 | 330.0 | |
| 7 | . 65 | 800 | 624.0 | 20 | 2550 | 612.0 | 60 |
| 8 | 37 | 800 | 355.2 | 13 | 2400 | 374.4 | 55 |
| 9 | 40 | 800 | 441.6 | 8 | 2400 | 230.4 | 44 |
| • 10 | 198 | 920 | 2185.9 | 11 | 2650 | 349.8 | 44 |
| 11 | 133 | 920 | 1468.3 | 18 | 2550 | 550.8 | 50 |
| 12 | 86 | 840 | 866.9 | 17 | 2950 | 601.8 | |
| 13 | 295 | 700 | 2478.0 | 15 | 2950 | 531.0 | |
| 14 | 98 | 800 | 940.8 | 13 | 2700 | 421.2 | 37 |
| 15 | 39 | _760 | 355.7 | 13 | 2700 | 421.2 | 46 |
| 16 | · 23 | 840 | 231.9 | 15 | 2950 | 531.0 | 44 |
| 17 | 35 | 840 | 352.8 | 15 | 2950 | 531.0 | 42 |
| 18 | 44 | 800 . | 422.4 | 27 | 2750 | . 891.0 | 42 |
| 19 | 44 | 840 | 443.5 | 17 | 3000 | 612.0 | |
| 20 | 25 | 800 | 240.0 | 13 | 3100 | 483.6 | |
| 21 * | Stream Di | verted to P | | | 1 | 1 | |
| 22 | 25 | 800 | 240.0 | 15 | 2750 | 495.0 | 53 |
| 23 | 75 | 800 | 720.0 | 15 . | 2550 | 459.0 | 53 |
| 5/1 | 173 | 350 | 726.6 | 18 | 2950 | 637.2 | 86 |
| 25 | .1 _j t0 | 700 | 9211.0 | 17 | 2650 | 540.6 | 40 |
| 26 | 39 | 540 ` | 252.7 | 44 | 2950 | 1557.6 | |
| 27 | 315 | 1300 | 4914.0 | 20 | 2950 | 708.0 | |
| 28 | 270 | 1190 | 3855.6 | 130 | 2750 | 4290.0 | 305 |
| 29 | 150 | 810 | 1458,0 | 830 | 3000 | 29880.0 | 95 |
| 30 | |). | <u> </u> | | ! | ! | |
| 31 | | | 1 | | | | |
| AVE. | 93 | 851 | 990.1 | 49 | 2754 | 1718 | 65 |

^{*} Flow being diverted through treatment system West Outfall only flow diverted.

MINERALB AND CHEMICAL DIVIBION
P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: January YEAR 1972

| | WEST | PLANT OUTFAI | L L | EAST | PLANT OUTF | 'ALL | 10" DRAIN |
|------------|---|--------------|---------|---|------------|---------|--|
| DVA 📀 | ppm (P ₂ 0 ₅) (Total) | | lbs/day | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day | ppm P ₂ O ₅ (Total) |
| 1 | 30 | 840 | 302 | 17 | 2950 | 602 | |
| 2 | 30 | 840 | 302 | 23 | 2950 | 814 | |
| 3 | 18 | 760 | 164 | 336 | 2650 | 10685 | 25 |
| 14 | 48 | 760 | 438 | 8 | 2700 | 259 | 23 |
| 5 | 20 | 800 | 192 | 20 | 2960 | 708 | 23 |
| ó | 42 | 800 | 403 | 13 | 2750 | 429 | 23 |
| 7 | 44· | 920 | 486 | 42 | 3500 | 1663 | 86 |
| 8* | 28 | 230 | 77 | 15 | 3000 | 540 | |
| <i>y</i> * | 17 | 270 | 55 | 25 | 2950 | 885 | |
| 10* | 27 | 270 | 88 | 420 | 2950 | 14868 | 390 |
| 11* | 123 | 350 | 517 | 78 | 3300 | 3089 | 28 |
| 12* | 70 | 440 | 370 | 102 | 2950 | 3610 | 120 |
| 13 | 42 | 900 | 454 | 105 | 2950 | 2343 | 78 |
| 14* | 32 | 540 | 207 | 715 | 2750 | 3717 | 55 |
| 15* | 22 | 490 | 129 | 17 | 2950 | 602 | |
| 16* | 46 | 490 | 271 | 550 | 2950 | 19470 | |
| 17* | 89 | 440 | 470 | 83 | 2500 | 2490 | 57 |
| 18* | 155 | 440 | 818 | 27 | 2400 | 778 | 89 |
| 19* | 210 | 490 | 1235 | 15 | 2650 | 477 | 67 |
| 20 | | iverted to | Pond | 20 | 2700 | . 648 | 62 |
| 21 | 213 | 980 | 2505 | 25 | 2700 | 810 | 147 |
| 22 | 232 | : 1170 | 3257 | 28 | 3150 | 1058 | |
| 23 | 102 | 1170 | 1432 | 305 | 2950 | 10797 | |
| 24 | 39 | 1100 | 515 | 1270 | 2750 | 41910 | 325 |
| 25 | 37 | 1170 | 520 | 18 | 2550 | 551 | 48 |
| 26 | 39 | 1050 | 491 | 173 | 2750 | 5715 | 42 |
| 27 | 35 | 920 | 386 | 98 | 2550 | 2999 | 48 |
| 28 | 336 | 980 | 3951 | 13 | 2750 | 429 | 55 |
| 29 | 13 | 840 | 131 | 70 | 2700 | 2268 |] |
| 30 | 325 | 920 | 3588 | 13 | 2950 | 460 | |
| 31 | 35 | 980 | 412 | 13 | 2700 | 421 | 50 |
| AVE. | 83 | 745 | 806 | 130 | 2831 | 4390 | 86 |

Partially diverted to spill control pond.
West Outfall only flow diverted.

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: December YEAR 1971

| | WEST | PLANT OUTFA | LI. | EAST | PLANT OUT | PALL | 10" DRAIN |
|------|---|-------------|-----------------|--|-----------|-----------------|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | | 230 | I | 362 | 2550 | 11077 | 720 |
| 2 | | RTED TO EXP | | 105 | 2700 | 3402 | 1120 |
| 3 | | OND ON 1st, | 2nd & 3rd | 115 | 2700 | 3726 | 1120 |
| 14 | 72 | | | 115 | 3300 | 4554 | |
| . 5 | 108 | 920 | 1192 | 86 | 3000 | 3096 | |
| 6 | 83 | 760 | 757 | 67 | 2750 | 2211 | 980 |
| 7 | 27 | 800 | 259 | 15 | 2700 | 486 | 390 |
| 8 | 17 | 200 | 21 | 600 | 2750 | 19800 | 1.8 |
| 9 | 42 | 200 | 101 | 13 | 2700 | 421 | 46 |
| 10 | 50 | 200 | 120 | 11 | 2650 | 350 | 102 |
| 11 | 327 | 160 | 628 | 18 | 3000 | 648 | |
| 12 | 50 | 105 | 63 | 25 | 2950 | 885 | |
| 13 | 30 | 200 | 72 | ° 18 | 2650 | 572 | 130 |
| 14 | 178 | 200 | 427 | 25 | 2650 | 795 | 123 |
| 15 | 193 | 200 | 463 | 67 | 2650 | 2131 | 86 |
| 16 | 33 | 200 | . 79 | 42 | 2700 | 1361 | 183 |
| 17 | 70 | 160 | 134 | 27 | 2650 | 859 | 102 |
| 18 | 28 | 230 | 77 | 25 | 3000 | 648 | |
| 19 | 3.8 | 160 | 35 | 17 | 3100 | 632 | |
| 50 | 27 | 1100 | 356 | 11 | 2950 | 389 | 44 |
| 21 | 165 | 840 | 1663 | 17 | 2700 | 551 | 50 |
| 22 | 147 | 800 | 1411 | 37 | 3000 | 1332 | 155 |
| 23 | | 760 | | | 1 | | 92 |
| 24 | | | | | i | ĺ | |
| 25 | 74 | | | 32 | 2950 | 1.1.33 | |
| 26 | 83 | 800 | 797 | 78 | 2950 | 2761 | |
| 27 | 35 | 800 | 336 | 39 | 2950 | 1381 | |
| 28 | 18 | 800 | 173 | 39 | 2650 | 1240 | 25 |
| 29 | 92 | 800 | 883 | 17 | 2750 | 561 | 35 |
| 30 | 48 | 800 | 461 | 38 | 2550 | 1163 | 48 |
| 31 | | 840 | 1 | | 2950 | | |
| AVE. | 81 | 521 | 458 | 74 | 2812 | 2434 | 278 |

MINERALS AND CHEMICAL DIVISION P. D. BOX 912

POCATELLO, IDAHO 85201

WASTEWATER DATA

MONTH: October YEAR 1971

| | WEST | PLANT OUTFAI | T | EAST | PLANT OUTF | ALL | 10" DRAIN |
|------|---|--|--------------------------------|--|--------------------|---------------------|---|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | 263 | 920 | 2959 | 30 | 2050 | 850 | 105 |
| 2 | 142 | 1850 | 932 | 10 | 700 | 84 | |
| 3 | 700* | 700* | 5880 * | 25 | 1750 | 525 | |
| 4 | 11 | 540 | 71 | 13 | 1950 | 30/1 | . 13 |
| 5 | 23 | 760 | 210 | 11 | 1500 | 198 | 20 |
| 6 | 376 | 980 | 4422 | 17* | 1900* | 388∗ | 27 |
| 7 | 20 | 13.00 | 264 | 13* | 2200* | 343* | 23 |
| 8 | 55 | 1050 | 63 | 3.1 | 1950 | 257 | 39 |
| 9 | 22 | 700 | 1.85 | 13 | 2500 | 390 | |
| 10 | 23 | 1170 | 323 | 20 | 2150 | 510 | |
| 11 | 42 | 980 | 494 | 8 | 2150 | 20ύ | 17 |
| 12 | 13 | 1050 | 164 | 11 | 2050 | 271. | 15 |
| 13 | 8 | 980 | 94 | 8 | 2050 | _197 | 13 |
| 14 | 1.3 | 640 | 131 | 11 ' . | 2150 | 284 | 20 |
| 15 | 11 | 760 | 100 | 13 | 2200 | 343 | 30 |
| 16 | 260 | 490 | 1529 | 20 | 2400 | 576 | |
| 17 | 72 . | 760 | 657 | 15 | 2550 | 459 | |
| 18 | 210 | 800 | 2016 | 25 | 2150 | , 6l ₄ 5 | 1414 |
| 19 | 20. | 800 | 192 | 17 | 2150 | 1439 | 27 |
| 20 | 39 | 800 | 374 | 23 | 2150 | . 593 | 46* - |
| 51 | 20 | 840 | 202 | 3.7 | 2300 | 469 | 44 |
| 22 | 27 | 1050 | 340 | 20 | 2400 | 576 | 05 |
| 23 | Jįt | 920 | 155 | 24 | 2700 | 778 | |
| 24 | 13 | 920 | 144 | 18 | 2700 | 583 | |
| 25 | HOLIDAY * | * | * * * * * * * * * * | ****** | ******* | | ***** |
| 26 | 28 | 920 | 309 | 20 | 2050 | 492 | 173* |
| 27 | 13 | 920 | 144 | 17 | 5500 | 14149 | 78 |
| 28 | 127 | 81 ^t O | 1280 | 8 | 2550 | 245 | 30 |
| 29 | 18 | 980 | 212 | 15 | 2150 | 387 | 15 |
| 30 | 18 | 980 | 212 | 16 | 2550 | 490 | |
| 31 | 28 | 1170 | 393 | 8 | 2700 | 259 | |
| AVE. | 83 | 919 | 815 | 16 | 2165 | 421 | 41 - |

^{*}Grab Samples

MINERALB AND CHEMICAL DIVISION
P. D. BOX 912
POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: September YEAR 1971

| | | PLANT OUTFAI | | | PLANT OUTF | | 10" DRAIN |
|------|---|--------------|-----------------|--|--------------------|------------------------------|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P2 ⁰ 5 | ppm P ₂ O ₅ (Total) |
| 1 | 11 | 1050 | 139 | 11 | 2200 | 290 | 11 |
| 2 | 236 | 700 | 1982 | 15 | 2300 | 432 | 20 |
| 3 | | . 980 | | 20 | 2550 | 612 | 33 |
| 14 | 11 | 700 | 92 | 9 | 2500 | 270 | |
| 5 | 46 | 980 | 540 | 15 | 2700 | 486 | |
| 6 | | | | | 1 | | |
| 7 | 48 | 920 | 530 | 17 | 5jt00 | 490 | 35 |
| 8 | 18 | 920 | 199 | 23 | 2400 | 662 | 46 |
| 9 | 18 | 920 | 199 | 13 | 2300 | 359 | 27 |
| 10 | 23 | 1100 | 304 | 18 | 2050 | 443 | 23 |
| 11 | 20 | 1300 | 312 | 21 | 2 ¹ 100 | 605 | |
| 1.2 | 8 | 1250 | 120 | 11 | 2)+00 | 317 | |
| 13 | <u> </u> | 1300 | | 13 | 2300 | 359 | 33 |
| 14 | 13 | 1170 | 183 | 18 - | 5400 | 518 | 23 |
| 15 | 13 | 1170 | 183 | 13 | 2050 | 320 | 27 |
| 16 | 11 | 1170 | 154 | 13 | 2200 | 343 | 39 |
| 17 | 20 | 980 | 235 | 104 | 2400_ | 2995 | 30 |
| 18 | - 8 | 1170 | 112 | 75 | 2700 | 2430 | <u></u> |
| 19 | 7 | 1100 | 92 | 11 | 2500 | 330 | |
| 20 | 7 | 1050 | 88 | 8 | 2500 | . 240 | 25 |
| 21 | 11 | 1100 | 145 | 11 | 2200 | 290 | 23 |
| 22 | 11 | 920 | 121 | 13 | 2300 | 359 | 27 |
| 23 | 11 | 920 | 121 | 11 | 2050_ | 271 | 30 |
| 24 | 19 | 920 | 210 | 27 | 2200 | 713 | 13 |
| 25 | 17 | 1100 | 224 | 35 | 2300 | 966 | |
| 26 | 5 | 980 | -59 | 7 | 2400 | 202 | |
| 27 | 13 | 840 | 131_ | 295 | 1900 | 6726 | 20 |
| 28 | 11 | 760 | 100 | 13 | 2200 | 343 | 11 |
| 29 | 53 | 640 | 407 | 15 | 1850 | 333 | 17 |
| 30 | 530 | 800 | 5088 | 50 | 1900 | 1140 | 53 |
| 31 | | | | | i | | |
| AVE. | 44 | 1032 | 447 | 31. | 2298 | 822 | 27 |

MINERALB AND CHEMICAL DIVIBION P. D. BOX 912

POCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH: August YEAR 1971

| | | PLANT OUTFAI | T | | PLANT OUTF | | 10" DRAIN |
|------|---|--------------|--|--|------------|-----------------|--|
| DAY | ppm (P ₂ O ₅) (Total) | Gal/Min | lbs/day P ₂ O ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P205 | ppm P ₂ O ₅ (Total) |
| 1 | 11 | 1170 | 154 | 11. | 2950 | 389 | |
| 2 | 8 | 1050 | 101 | 18 | 2700 | 583 | 11 |
| 3_ | 18 | 980 | 212 | 13 | 2950 | 460 | 11 |
| 4 | 13 | 980 | 153 | 11. | 2950 | 389 | 18 |
| 5 | 33 | 980 | 398 | 11 | 2700 | 356 | 23 |
| 6 | 12 | 980 | 141 | 11 | 2700 | 356 | 13 |
| 7 | 11 | 1170 | 154 | 11 | 3100 | 409 | |
| 8 | 15 | 1050 | 189 | 18 | 2700 | 583 | |
| 9 | 13 | 980 | 153 | 8 | 2550 | 245 | 17 |
| 10 | 10 | 980 | 118 | 11 | 2700 | 356 | 13 |
| 11 | 25 | 1100 | 330 | 18 | 2750 | 594 | 62 |
| 12 | 15 | 1050 | 189 | 11 | 2700 | 356 | 23 |
| 13 | 20 | 1050 | 252 | 18 | 2550 | 1490 | 17 |
| 14 | | | | 16 > | 2550 | 540 | |
| 15 | 15 | 1050 | 189 | 13 | 2500 | 390 | |
| . 16 | 15 | 1050 | 189 | 15 | 2400 | 432 | 13 |
| 17 | 13 | 1050 | 164 | 15 | 2400 | 432 | 13 |
| 18 | 5 | 1100 | 66 | 8 | 2650 | 254 | 11 |
| 19 | 15 | 1100 | 198 | 11 | 2400 | 317 | 13 |
| 20 | 23 | 1170 | 323 | 20 | 2500 | 600 | 11 |
| 21 | 23 | | | 46 | 2700 | 1490 | |
| 22 | 25 | | | 11 | 2500 | 330 | |
| 23 | 20 | 1170 | 281 | 17 | 2200 | 449 | 15 |
| 24 | . 15 | 1100 | 198 | 15 | 2050 | 369 | 13 |
| 25 | 13 | 1170 | 153 | li | 2200 | 290 | 8 |
| 26 | 11 | 1170 | 154 | 11 | 2200 | 290 | 18 |
| 27 | 149 | 1170 | 1967 | 15 | 2150 | 387 | 20 |
| 28 | 17 | 1 | | 14 | 2400 | 403 | |
| 29 | 53 | | | 11 | 2550 | 337 | |
| 30 | 13 | 1100 | 172 | 11 | 2500 | 330 | 8 |
| 31 | · 95 | .980 | 1117 | 13 | 2050 | 320 | 13 |
| AVE. | 25 | 1070 | 296 | 14 | 2544 | 436 | 16 7 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: July

| | | PLANT OUT | ALL | EAST | PLANT OUT | TALL | 10" DRAIN |
|------|---|-----------|-------------------------------|---|-----------|---------|--|
| DAY | ppm (P ₂ O ₅) | | lbs/day | ppm PoOs | | lbs/day | ppm P ₂ O ₅ |
| | ppm (P ₂ 0 ₅) (Total) | Gal/Min | P ₂ 0 ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | | ppm P ₂ O ₅ (Total) |
| 1 | | 980 | 412 | 11. | 2550 | 367 | 15 |
| 2 | 20 | 700 | 168 | 18 | 2300 | 1+97 | 33 |
| 3 | 2ό | 840 | 262 | 14 | 2500 | 420 | |
| 14 | | 700 | | | 2400 | | |
| 5 | 37 | 760 | 337 | 27 | 2400 | 778 | |
| 6 | կկ | 760 | 401 | 42 | 2750 | 1386 | 42 |
| 7 | 48 | 920 | 530 | 30 | 2500 | 900 | 35 |
| 8 | 42 | 980 | 494 | 35 | 2050 | 861 | 39 |
| 9 | 39 | 920 | 431 | 44. | 1850 | 977 | 18 |
| 10 | 29 | 1170 | 407 | 33 | 2400 | 950 | |
| 11 | 11 | 980 | 129 | 17 | 2200 | 449 | |
| 12 | 20 | 980 | 235 | 8 | 2200 | 211 | 15 |
| 13 | 20 | 980 | 235 | 15 | 2050 | 369 | 15 |
| 14, | 15 | 1170 | 211 | 13 | 2050 | 320 | 13 |
| 15 | 17 | 1100 | 224 | 13 | 2150 | 335 | 13 |
| ló | 17 | 1050 | 214 | 14 | 2200 | 370 | 5 |
| 17 | 53 | 1050 | 668 | 15 | 2500 | 450 | |
| 18 | 30 | 1050 | 378 | · 5 | 2200 | 132 | |
| 19 | 15 | 1100 | 198 | 8 | 2200 | 211 | 11 |
| 20 | 65 | 920 | 718 | 17 | 2300 | 469 | 60 |
| 21 | 11 | 920 | 121 | 11 | 2400 | 317 | 11. |
| 22 | 53 | 920 | 585 | 15 | 2500 | 450 | 18 |
| 23 | 15 | 920 | 166 | 17 | 2200 | 449 | 17 |
| 24 | 17 | 1100 | 55 _J t | 18 | 2550 | 551 | |
| 25 | 11 | 1100 | 145 | 8 | 2500 | 2/10 | |
| 20 | 17 | 980 | 200 | 8 | 2400 | 230 | 15 |
| 27 | 15 | 980 | 176 | 18 | 2700 | 583 | 20 |
| 28 | 18 | 920 | 199 | 17 | 2650 | 541 | 13 |
| 29 | 15 | 1050 | 189 | 23 | 2650 | 731 | 23 |
| 30 | 25 | 1050 | 315 | 33 | 2400 | 950 | 11 |
| 31 | 20 | 1170 | 281 | 5 | 2750 | 165 | |
| AVE. | 27 | 975 | 309 | 18 | 2369 | 521 | 21 |

MINERALS AND CHEMICAL DIVISION
P. G. BOX 912

POCATELLO, IDAHO 8320

WASTEWATER DATA

Month: JUNE

| | WEST | PLANT OUTF | ALL | EAST | PLANT OUT | ALL | 10" DRAIN |
|------|--------------------------------------|------------|-------------------------------|---|-----------|-------------------------------|--|
| DAY | ppm (P ₂ O ₅) | | lbs/day | ppm P ₂ O ₅ (Total) | | lbs/day | ppm P ₂ O ₅ |
| | (Total) | Gal/Min | P ₂ 0 ₅ | (Total) | Gal/Min | P ₂ 0 ₅ | ppm P ₂ O ₅ (Total) |
| 1 | 18 | 800 | 173 | 8 | 2400 | 230 | 18 |
| 2 | 17 | 920 | 188 | 11 | 2300 | 304 | 28 |
| / 3 | 28 | 980 | 329 | 18 | 2550 | 551 | 30 |
| 4 | 47 | 1050 | 592 | 20 | 2300 | 552 | 28 |
| 5 | 48 | 1050 | 605 | 27 | 2400 | 778 | |
| 6 | 27 | 1300 | 421 | 20 | 5,400 | 576 | |
| 7 | 27 | 1050 | 340 | 8 | 2550 | 245 | 28 |
| 8 | 30 | 1250 | 450 | 15 | 2550 | 459 | 27 |
| 9 | 57 | 1250 | 855 | 15 | 2500 | 450 | 25 |
| 10 | 39 | 1100 | 515 | 13 | 2300 | 359 | 27 |
| 11 | 20 | 1250 | 300 | 17 | 2200 | 449 | 1730 |
| 12 | 23 | 1250 | 345 | 20 | 2400 | 576 | |
| 13 | 700 | 1300 | 10920 | 11 ~ | 2050 | 271 | |
| 14 | 98 | 1170 | 1376 | 13 | 1900 | . 296 | 42 |
| 15 | 112 | 1250 | 1680 | 8 | 2050 | 197 | 35 |
| 16 | 139 | 1170 | 1952 | 11 | 2400 | 317 | 35 |
| 17 | 44 | 980 | 517 | 15 | 2200 | 396 | 30 |
| 18 | 65 | 980 | 764 | 13 | 2150 | 335 | 780 |
| 19 | 15 | 980 | 176 | 8 | 2400 | 230 | |
| 20 | 17 | 980 | 200 | 405 | 2400 | 12150 | <u> </u> |
| 21 | 15 | 980 | 176 | 550 | 1900 | 12540 | 500 |
| 22 | 18 | 1050 | 227 | 37 | 2300 | 1021 | 62 |
| 23 | 236 | 840 | 2379 | 13 | 1950 | 304 | 27 |
| 24 | 46 | 920 | 508 | 35 | 2550 | 1071 | 17 |
| 25 | 20 | 920 | 221 | 15 | 2550 | 459 | 17 |
| 26 | 52 | 1170 | 744 | 7 | 2700 | 227 | |
| 27 | 420 | 700 | 3528 | 8 | 2400 | 230 | |
| 28 | 42 | 980 | 494 | 8 | 2700 | 259 | 15 |
| 29 | 17 | 1100 | 224 | 10 | 2550 | 300 | 13 |
| 30 | 30 | 1050 | 378 | 10 | 2550 | 300 | 18 |
| AVE. | 82 | 1029 | 1052 | 46 | 2355 | 1214 | 161 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: May

| | | Plant Outfe | 11 | East | Plant Outf | all | 10" Drain |
|-----------|---|-------------|------------------------------|---|------------|--|---------------------|
| DAY | ppm (P ₂ 0 ₅) (Total) | Gal/Min | lbs/day P ₂ 05 | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ O ₅ | pom P205 (Total) |
| | 57 | 1300 | 889 | 8 | 2400 | 230 | |
| <u>2</u> | 17 | 1300 | 265 | 13 | 2550 | 398 | |
| 3 | 33 | 1300 | 515 | 11 | 2650 | 350 | 17 |
| į į | 17 | 1450 | 296 | 27 | 2750 | . 891. | 30 |
| 5 | 60 | 1450 | 1044 | 15 | 2500 | 450 | 33 |
| ó | 15 | 1450 | | 15 | 2500 | 1:50 | 30 |
| 7 | 15 | 1450 | 201 | 23 | 2150 | 593 | 42 |
| - 8. | 20 | 1600 | 384 | 11 | 2200 | 290 | |
| 9 | | | | | | | |
| 10 | 17 | 1500 | 30ó | 1.7 | 2050 | 41.8 | 37 |
| 11 | 30 | 1300 | 468 | 8 | 2050 | 1.97 | 37 |
| 12 | 35 | 980 | 412 | 11 | 1950 | 257 | 15 |
| 13 | 27 | 920 | 298 | 13. | Sj+00 | 31.7 | 33 |
| 14 | 23 | 980 | 270 | 12 | 2300 | 331. | 30 |
| 15 | <u> </u> | 920 | | | 2650 | | |
| 16 | 60 | 840 | 605 | 11 | 2300 | 304 | |
| 17 | 65 | 840 | | 1.3 | ,×5300 | 359 | 20 |
| 7 18 | 23 | 800 | | 13 , | 2200 | 343 | 23 |
| <u>19</u> | 23 | 980 | 270 | 15 | 2550 | 459 | 20 |
| 20 | 27 | 800 | <i>∠</i> | 17 | 2300 | 469 | 92 |
| 21 | 44 | 840 | TTT 1 | 18 | 5/1:00 | 518 | 58 |
| 22 | 75 | 980 | පිරි2 | 2.4 | 2400 | 403 | |
| 23 | 17 | 920 | 188 | 13 | 2500 | 390 | |
| 24 | 11 | 1050 | 139 | 11 | 2200 | 290 | . 37 |
| 25 | 23 | 920 | 254 | 13 | 5500 | 343 | 28 |
| 26 | 18 | 920 | | 17 | 21.50 | 439 | 30 |
| 27 | 30 | 920 | 331 | 13 | 2300 | 359 | 60 |
| 23 | 20 | 920 | 287 | 23 | 5400 | 668 | 35 |
| 29 | 83 | 920 | 916 | 57 | 2750 | 1881. | |
| 30 | | 920 | | | 2950 | | |
| 31 | 95 | 800 | 912 | 1.1 | 2400 | 317 | |
| AVE. | 35 | 1076 | 437 | ló | 2380 | 439 | 34 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: April

| | West | Plant Outfa | | | Plant Outf | all | 10" Drain |
|-----------------|---------------------|-------------|--|---|---------------|------------------------------|---|
| DAY | ppm P205 (Total) | Gal/Min | lbs/day P ₂ O ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | los/day P ₂ 05 | ppm P ₂ O ₅ (Total) |
| l | 15 | 700 | 1 126 | = 10001/ | 2300 | 527 | 17 |
| 2 | 33 | 980 | 368 | 29 | 2300 | 500 | 1 20 |
| -2 3 | 17 | 1100 | 200 | 23 | | 995 | |
| <u> </u> | 15 | 1170 | 1 211 | 15 | 5400 | F35 605 | |
| -5 | 1.1 | 1050 | 1 139 | 11 | 2300 2300 | 304 | 17 |
| - | 30 | 1050 | 378 | 11 | 2200 | 250 | 20 |
| 7 | 53 | 1050 | 1 568 | 11 | 2200 | 1 200 | 1 20 |
| | 25 | 1170 | 351 | 13 | 1750 | 273 | 23 |
| 9 | 25 | 1300 | 390 | 17 | 1450 | 290 | <u> </u> |
| 10 | 30 | 1.250 | 450 | 25 | 1850 | 555 | 1 <u></u> 0 |
| 11 | 1.1 | 1300 | 172 | 13 | 1050 | 257 | |
| 12 | 1.1 | 1170 | 154 | 15 | 1500 | 270 | 1.8 |
| 13 | 1.8 | 1170 | 253 | 17 | 1500 | 300 | 1 20 |
| 14 | 25 | 1170 | 351 | 13 | 1650 | 257 | 20 |
| 15 | 18 | 1170 | 253 | 650 | 1350 | 10530 | F050 |
| 16 | 24 | 1.250 | 360 | 78 | 1900 | 1773 | 350 |
| 17 | 236 | 1250 | 3540 | 19 | 2500 | 570 | |
| 18 | 1,8 | 1300 | 748 | 11 | 2200 | 290 | |
| 19 | 46 | 1250 | 1 690 | 13 | 1950 | 301 | 3,0 |
| 20 | 127 | 1170 | 1783 | 7 | 1 2050 | 172 | 30 |
| 21 | 143 | 1300 | 2231 | 27 | 1 1750 | 507 | 89 |
| 22 | 23 | 1250 | 345 | 11 | 2050 | 271 | 50 |
| 23 | 36 | 1300 | 1342 | 13 | i 2050 | 320 | 95 |
| 5/1 | 102 | 1450 | 1775 | 17 | 2050 | 418 | |
| 25 | 183 | 1450 | 3182 | 62 | 2400 | 1785 | |
| 26 | 15 | 1250 | 225 | 8 | 1950 | 187 | 39 |
| 27 | 15 | 1250 | 225 | 8 | 2300 | 221 | 3.7 |
| 28 | 1+2 | 1250 | 630 | 13 | 2050 | 320 | 18 |
| 29 | 7 | 1350 | 1113 | 8 | S/i00 | 230 | 1.7 |
| 30 | 17 | 1300 | 265 | 13 | 2050 | 320 | 20 |
| AVERA | | 1206 | 732 | 39 | 2015 | 783 | 180 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: March

Year: 1971

| - | West | Plant Out | fall | East 1 | Clant Outfa | 11 | 10" Drain |
|-------|--|-----------|-------------------------------|---|-------------|-------------------------------|-----------|
| DAY | ppm P ₂ O ₅ | | lbs/day | ppm P ₂ O ₅ | | lbs/day | ppm-P2O5 |
| | ppm P ₂ O ₅ (Total) | Gal/Min | P ₂ 0 ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | P ₂ 0 ₅ | (Total) |
| 1 | 11 | 1170 | 154 | 11 | . 2200 | 290 | 15 |
| 2 | 15 | 1250 | 225 | 15 | 2200 | 396 | 20 |
| 3 | 18 | 1170 | 253 | 11 | 2300 | 304 | 18 |
| 4 | 11 | 1170 | 154 | 11 | 2050 | 271 | 15 |
| 5 | 20 | 1.100 | 264 | 23 | 2550 | 704 | 33 |
| 6 | 20 | 1300 | 312 | 27 | 2700 | 875 | |
| 7 | 13 | 1170 | 183 | 15 | 2700 | 486 | |
| 8 | 65 | 1100 | 858 | 13 | 2400 | 274 | 20 |
| 9 | 67 | 1250 | 1005 | 11 | 2400 | 317 | 20 |
| 10 | 37 | 800 | 355 | 13 | 2300 | 559 | 17 |
| 11 | 50 | 1250 | 750 | 160 | 2500 | 4800 | 1230 |
| 12 | 151 | 1250 | 2265 | 27 | 2550 | 826 | 50 |
| 13 | ⁷ 36 | 1250 | 540 | 25 | 2550 | 765 | |
| 14 | 27 | 1250 | 405 | 13 | 2550 | 398 | |
| 15 | 11 | 1170 | 154 | 11 🗽 | 2750 | 363 | 25 |
| 16 | 39 | 760 | 356 | 11 | .2650 | 350 | 23 |
| 17 | 86 | 1300 | 1342 | 13 | 2500 | 390 | 46 |
| 18 | 42 | 1250 | 630 | 13 | 2700 | 421 | 20 |
| 19 | 44 | 1250 | 660 | 26 | 2400 | 749 | 139 |
| 20 | 43 | 1050 | 542 | 27 | 2650 | 859 | |
| 21 | 28 | 1100 | 370 | 18 | 2650 | 572 | |
| 22 | 115 | 1170 | 1615 | 15 | 2400 | 432 | 44 |
| 23 | 544 | 1170 | 3426 | 44 | 2550 | 1346 | 70 |
| 24 | 23 | 1170 | 323 | 18 | 2650 | 572 | 20 |
| 25 | 92 | 980 | 1082 | 18 | 2300 | 497 | 53 |
| 26 | 93 | 1300 | 1451 | 28 | 2550 | 857 | 35 |
| 27 | 28 | 1250 | 420 | 17 | 2650 | 541 | |
| 28 | 17 | 1250 | 255 | 1.3 | 2650 | 413 | |
| 29 | 23 | 1250 | 345 | 11 | 2550 | 337 | 25 |
| 30 | 11 | 840 | 111 | 13 | 5500 | 343 | 33 |
| 31 | 17 | 540 | 110 | 11 | 2200 | 290 | 27 |
| AVER/ | AGE 48 | 1138 | 676 | 22 | 2482 | 661 | 43 |

MINERALS AND CHEMICAL DIVISION P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: February

| | We | st Plant 0 | utfall | £as | t Plant Ou | tfall | 10" Drain |
|---------|--|------------|--|--|------------|--|--|
| DAY | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ O ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ O ₅ | ppm P ₂ O ₅ (Total) |
| | | | | | | | |
| 1 | 62 | 800 | 595 | 15 | 5500 | 396 | 28 |
| 2 | 48 | 820 | 472 | 17 | 2050 | 418 | 35 |
| 3 | 143 | 800 | 1373 | 17 | 2050 | 418 | 25 |
| 4 | 127 | 800 | 1219 | 11 | 2050 | 271 | 15 |
| 5 | 930 | 800 | 8928 | 26 | 2300 | 718 | 80 |
| 6 | 39 | 1050 | 491 | 27 | 2300 | 745 | |
| 7 | 20 | 920 | 221 | 17 | 2050 | 418 | |
| 8 | 135 | 800 | 1296 | 244 | 1950 | 5710_ | 80 |
| 9 | 72 | 920 | 795 | 13 | 5500 | 343 | 23 |
| 10 | 315 | 920 | 3478 | 20 | 2050 | 492 | 135 |
| 11 | 30 | 840 | 302 | 60 | 5500 | 1584 | 500 |
| 12 | 27 | 800 | 259 | 60 | 2550 | 1836 | 75 |
| 13 | 20 | 920 | 551 | 18 | 2500 | 541 | |
| 14 | 70 | 920 | 773 | 13 | 2550 | 398 | |
| 15 | | | | | | | |
| 16 | 30 | 760 | 274 | 8 | 2400 | 230 | 17 |
| 17 | 42 | 800 | 403 | 11 | 2400 | 317 | 33 |
| 18 | 75 | 920 | 828 | 5 | 2550` | 153 | 18 |
| 19 | 178 | 590 | 1260 | 15 | 2200 | 396 | 15 |
| 20 | 42 | 800 | 403 | 14 | 2400 | 403 | |
| 21 | 28 | 700 | 235 | 8 | 2550 | 245 | |
| 22 | 33 | 640 | 253 | 13 | 2400 | 374 | 18 |
| 23 | 252 | 920 | 2782 | 15 | 2550 | 459 | 18 |
| 24 | 155 | 1170 | 2176 | 11 | 2550 | 367 | 25 |
| 25 | 39 | 1170 | 548 | 11 | 2400 | 346 | 20 |
| 26 | 15 | 1250 | 225 | 11 | 2550 | 267 | 17 |
| 27 | 11 | 1170 | 159 | 11 | 2550 | 367_ | |
| 28 | 11 | 1170 | 154 | 11 | 2650 | 382 | |
| AVERAGI | :109 | 875 | 1119 | 26 | 2339 | 692 | 62 |

MINERALD AND CHEMICAL DIVISION P. CLBOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

Month: January

Year: 1971

| | | | | | | | / |
|-------|---|-------------|-------------------------------|---|-----------|--------------------|--|
| | West | t Plant Out | | East | Plant Out | fall | 10" Drain |
| DAY | ppm PoOs | | lbs/day | ppm PoOc | | lbs/day | |
| | ppm P ₂ O ₅ (Total) | Gal/Min | P ₂ O ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | P ₂ 05 | ppm P ₂ O ₅ (Total) |
| | | | | | | | |
| 1.1 | 46 | 1170 | 646 | . 15 | 2550 | 454 | ₩ |
| 2 | 13 | 1450 | 226 | 25 | 2500 | 750 | |
| :3 | 13 | 1300 | 203 | 15 | 2700 | 986 | |
| 1 | 8 | 1170 | 112 | 1,5 | 2550 | 459 | 35 |
| 5 | 18 | 1170 | 253 : ∷ | 28 | 2550 | 857 | 100 |
| :6 | 15 | 1170 | 211 : | 139 | 2400 | 14003 | 53 |
| 7 | 33 | 1170 | 463 | 33 | 5/100 | 950 | 375 |
| 8 | 139 | 1170 | 1952 '' | _17 | 2550 | 520 | 1080 |
| ∵9 | 83 | 1300 | 1295 | 210 | 2950 | 7434 | |
| 10 | 127 | 1900 | 2896 | 28 | 3150 | 1058 | |
| . 11 | 70 | 1350 | 1134 | 17 | 2400 | 490 | 112 |
| 12 | 33 | 1050 | 416 | 13 | 2050 | 320 | 20 |
| 13 | 25 | 1170 | 351 | 50 | 2200 | 528 | 147 |
| 14 | 46 | 920 | 508 | 23 | 2400 | 662 | 147 |
| 15 | 5/10 | 1170 | 3370 🐺 | 50 | > 5500 | 1320 | 260 |
| 16 | 130 | 1050 | 1638 | 37 | 2550 | 1132 | |
| ::17 | 165 | 1170 | 2317 | 42 | 2900 | 1336 | |
| :: 18 | 23 | 800 | 221 | 89 | 2650 | 2830 | 650 |
| : 19 | 15 | 800 | 144 :: | 60 | 2200 | 158 ¹ 4 | 420 |
| : 20 | 15 | 920 | 166 | 18 | 2300 | 497 | . 78 |
| . 21 | 11 | 800 | 106 | 62 | 1950 | 1451 | 405 |
| 22 | 16 | 1050 | 202 | 46 | 2150 | 1187 | 295 |
| • 23 | 70 | 1050 | 882 | 1414 | 2550 | 1346 | |
| . 24 | 37 | 1050 | 466 | 33 | 2550 | 1010 | |
| : .25 | 15 | 1050 | 189 : | 33 | 5500 | 87). | 285 |
| 26 | 1,2 | 1170 | 590 | 50 | 2200 | 1320 | 295 |
| .27 | 35 | 1170 | 491 : . ; | 15 | 2050 | 369 | 15 |
| : 28 | 15 | 1170 | 211 : | 15 | 5500 | 396 | 28 |
| 29 | 15 | 1170 | 211 | 28 | 2200 | 739 | 165 |
| : 30 | 15 | 1250 | 211 | 35 | 5400 | 1008 | <u> </u> |
| .31 | 53 | 920 | 585 | 39 | 2650 | 1240 | |
| AVE. | 51 | 1136 | 731 | 42 | 2427 | 1245 | 251 |
| | | | | | | | |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: December

YEAR: 1970

| | | ANT OUTFAL | | // | PLANT OUTF | | 10" DRAIN |
|------|---|------------|-------------------------------|--|------------|-------------------------------|--|
| DAY | ppm P ₂ O ₅ (Total) | | lbs/day | ppm P ₂ O ₅ (Total) | | lbs/day | ppm P ₂ O ₅ (Total) |
| L | (Total) | Gal/Min | P ₂ 0 ₅ | (Total) | Gal/Min | P ₂ 0 ₅ | (Total) |
| | | | | | | | |
| 11 | 53 | 1300 | 827 | 23 | 2400 | 662 | 112 |
| 2 | 60 | 1050 | 756 | · 25 | 2200 | 607 | 178 |
| 3 | 169 | 1050 | 2129 | · 23 | 2400 | 662 | 120 |
| 4 | 42 | 980 | 494 | 23 | 2400 | 662 | 143 |
| 5 | 18 | 1300 | 281 | ··· 23 | 2150 | 593 | |
| 6 | 25 | 1450 | 435 | 35 | 2200 | 924 | |
| 7 | 139 | 1300 | 2168 | . 440 | 2200 | 11616 | 1270 |
| 8 | 72 | 1300 | 1123 | 15 | 2400 | 432 | 53 |
| 9 | 89 | 1450 | 1549 | . 55 | 2400 | 1584 | 330 |
| 10 | 37 | 1300 | 577 | . 11 | 2650 | 350 | 25 |
| 11 | 17 | 1300 | 265 | 11 | 2550 | 337 | 13 |
| 12 | | | | . 11 | 2700 | 356 | |
| 13 | 13 | 1300 | 203 | 11 | 2500 | 330 | |
| 14 | 28 | 1300 | 437 | 8 | 2400 | 230 | 1.8 |
| 15 | 135 | 1300 | 2106 | 11 | 2200 | 290 | 3.7 |
| 16 | 80 | 1300 | 1249 | 11 | ~2400 | 317 | 62 |
| 17 | 295 | 1450 | 5133 | 8 | 2050 | 197 | 15 |
| 18 | 17 | 1250 | 255 | 11 | 2200 | 290 | 27 |
| 1.9 | 17 | 1170 | 239 | 11 | 2550 | 337 | |
| 20 | 15 | 1300 | 234 | 13 | 2550 | 398 | |
| 21 | 28 | 1170 | 393 | 13 | 2400 | 374 | 18 |
| 22 | 23 | 1250 | 345 | 8 | 2400 | 230 | 15 |
| 23 | 30 | 1250 | 450 | 35 | 2550 | 1071 | 83 |
| 24 | 23 | 926 | 256 | | | | |
| 25 | | | · | | | | |
| 26 | 124 | 920 | 1369 | . 23 | 3000 | 828 | |
| 27 | 700 | 980 | 8232 | 18 | 2550 | 551 | |
| 28 | 83 | 920 | 915 | 17 | 2200 | 449 | 57 |
| 29 | 80 | 800 | 768 | 17 | 2550 | 520 | 00 |
| 30 | 95 | 1050 | 1197 | 33 | 2200 | 871 | 670 |
| 31 | | 1170 | | | 2550 | <u> </u> | 33 |
| AVE. | 90 | 1193 | 1228 | 34 | 2411 | 931 | 158 |

MINERALS AND CHEMICAL DIVISION P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH:

November

YEAR: <u>1.970</u>

| DAY | i west | PLANT OUTF | | | PLANT OUT | FALL | JO" DRAIN |
|---------|---|------------|--|--|--------------------|--|--|
| DAI | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ 0 ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | 1bs/day P ₂ 0 ₅ | ppm P ₂ 0 ₅ (Total) |
| 1 | 13 | 1170 | 180 | 00 | 0550 | 620 | 3.2 |
| | 13 | 1050 | 160 | 1 20 8 | 2550 2750 | 200 | 13 |
| 3 | 70 | 1170 | 980 | 1 8 | 2700 | | 46 |
| , | 13 | 1300 | 200 | 15 | 2650 | 480 | 7 |
| - 5 | 28 | 1170 | 400 | 13 | 2950 | 1+60 | 39 |
| 6 | 1 20 | 1300 | 400 | 11 | 2950 | 1 L;00 | i |
| 7 | <u> </u> | 1450 | | # | 2400 | | |
| × | 1 17 | 1450 | 300 | 17 | 2700 | 560 | 250 |
| 9 | 80 | 1300 | 1260 | 42 | 5,100 | | 80 |
| 10 | 420 | 1100 | 55 ¹ +0 | 23 | 2550 | | |
| 11 | 1 | 1100 | 7)0 | 1 2 | 2))0 | 100 |) |
| 12 | 362 | 1500 | 6520 | 1 23 | 2300 | 0:0 | 005 |
| \ | 108 | 1250 | 1620 | 60 | 2400 | 17 ¹ ;0 | 285 |
| 14 | 23 | 1170 | 320 | 20 - | 2500 | 600 | 1 |
| 15 | 15 | 1170 | 220 | 60 | 2500 | 1800 | 39 |
| 7.6 | 72 | 1450 | 1260 | 8 | 2400 | 240 | 42 |
| 17 | 13 | 1650 | 260 | 8 | 2400 | 5/iO | 143 |
| 78 | 260 | 1450 | 4520 | 25 | 2 ¹ +00 | | 1.5 |
| 19 | 35 | 1170 | 500 | 8 | 2550 | | 35 |
| 20 | 46 | 1300 | 720 | 13 | 2300 | | |
| 21. | 5 | 1300 | 80 | i 7 | 2500 | | |
| 22 | 30 | 1300 | 460 | 13 | 2550 | 4,00 | 57 |
| 23 | 120 | 1250 | 1800 | 18 | 2700 | 550 | 30 |
| 24 | 115 | 1250 | 1720 | 15 | 2700 | | 8 |
| 25 | ¥2 | 1250 | 640 | 20 | 2650 | ρĮŧΟ | |
| 26 | . , | | | | | | : ! |
| 27 | 25. | 1250 | 380 | 13 | 2200 | 340 | 37 |
| 28 | | 1250 | | 15 | 2500 | 460 | |
| 29 | 92 | 1450 | 1600 | 17 | 2200 | 460 | 1 |
| 30 | 70 | 1500 | 1260 | 23 | 2500 | 700 | 62 |
| AVERAGE | · 83 | 1300 | 1320 (^{A)} | 19 | 2530 | 590 ^{5,7,5} | 106 |

MINERALS AND CHEMICAL DIVISION P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH: October

YEAR: 1970

| | | LANT OUTF | | | LANT OUTFA | | 10" Drain |
|----------|--|-----------|--|---|------------|--|---------------------|
| DAY | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/Day P ₂ O ₅ | ppm P ₂ O ₅ (Total) | Gal/Min | lbs/day P ₂ 0 ₅ | ppm P2O5 (Total) |
| 1 | 5 | 1300 | 80 | 15 | 2400 | 440 | 53 |
| 2 | 13 | 1250 | 200 | 13 | 2500 | 400 | 17 |
| 3 | 3 | 1300 | 40 | 7 | 2550 | 220 | |
| 4 | 35 | 1300 | 540 | 8 | 2400 | 240 | |
| 5 6 | 62 | 920 | 680 | 7 | 2200 | 180 | 8 |
| 6 | 17 | 1050 | 220 | 13 | 2550 | 400 | 15 |
| 7 | 1.1 | 1050 | 140 | 17 | 2550 | 520 | 102 |
| 8 | 13 | 1250 | 200 | 35 | 2500 | 1060 | 44 |
| 9 | 169 | 1300 | 2640 | 15 | 2400 | 440 | 11 |
| 10 | 17 | 1300 | 260 | 13 | 2700 | 420 | |
| 11 | 13 | 1300 | 200 | 8 | 2700 | 260 | |
| | 11 | 1100 | 140 | 8 | 2550 | 240 | 20 |
| 1.3 | 53 | 1300 | 820 | 37 | 2400 | 1060 | jto. |
| 1.14 | 13 | 1250 | 200 | 8 | 5500 | -550 | 11 |
| 15 | 48 | 1300 | 760 | 13 | 5/100 | 380 | 18 |
| 16 | 17 | 1250 | 200 | 15 | 2300 | 420 | 18 |
| 17 | 7 | 1350 | 140 | 13 | ~2700 | 420 | |
| 18 | 18 | 1350 | 300 | 17 | 2700 | 560 | |
| 18 | 46 | 1300 | 720 | 18 | 2500 | 540 | 33 |
| 20 | 92 | 1350 | 1500 | 15 | 2650 | 480 | 18 |
| ., 21 | 65 | 1300 | 1020 | 13 | 2650 | 420 | 13 |
| 22 | 44 | 1300 | 680 | 11 | 2500 | 340 | 20 |
| 1 -2 | 83 | 1170 | 1160 | 11 | 2700 | 360 | 7 |
| 24 | 18 | 1300 | 280 | 17 | 2700 | 560 | |
| 25 26 | 8 | 1450 | 140 | 7 | 1350 | 120 | |
| | 70 | 1050 | 880 | 13 | 2700 | 420 | 5 |
| 27 | 57 | 490 | 340 | 8 | 2650 | 260 | 17 |
| 28 | 15 | 1170 | 220 | 15 | 2700 | 480 | 17 |
| 28 29 | 7 | 1100 | 100 | 8 | 2700 | 260 | 20 |
| 30 | 13 | 1170 | 180 | 7 | 2700 | 220 | 108 |
| 31 | 13 | 1250 | 200 | 23 | 2700 | 740 | |
| AVERAGE | 34 | 1220 | 490 491 | 14 | 2510 | 420 422 | 28 |
| | | | L | и | | 1 | <u> </u> |

MINERALS AND CHEMICAL DIVISION P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH September YEAR 1970

| DAY ppm P ₂ O ₅ (Total) Gal/Min (Total) ypm P ₂ O ₅ (Total) Gal/Min (Tot | ppm P ₂ 0 (Total) ⁵ |
|--|--|
| 2 1250 8 11 2300 3 1250 600 7 2550 4 1450 108 46 2150 5 1450 115 2650 6 1500 25 2150 | |
| 3 1250 600 7 2550 4 1450 108 46 2150 5 1450 115 2650 6 1500 25 2150 | 15 |
| 4 1450 108 46 2150 5 1450 115 2650 6 1500 25 2150 | 13 |
| 5 1450 115 2650 6 1500 25 2150 | 11 |
| 5 1450 115 2650 6 1500 25 2150 | 13 |
| c 1500 25 1 2150 | 17 |
| 7 | 8 |
| | |
| 8 1450 8 72 2200 | 13 |
| 9 1350 17 70 2550 | 50 |
| 10 1350 440 35 2700 | 35 |
| 11 1450 300 2220 2200 | 18 |
| 12 1050 53 2700 | 83 |
| 13 980 135 2400 | |
| 14 920 300 17 2400 | 11 |
| 15 920 250 11 2200 | 370 |
| 1.6 1350 42 23 2500 | 15 |
| 17 1450 17 46 2200 | 17 |
| 18 1350 118 37 2650 | 67 |
| 19 1300 48 3100 | 18 |
| 20 1650 170 . 2650 | 7 |
| 21 1170 127 15 2700 | 13 |
| 22 1450 108 57 2950 | 23 |
| 23 1450 1200 20 2650 | 13 |
| 24 1450 198 23 2700 | 17 |
| 25 1350 75 35 2750 | 15 |
| 26 1300 20 2700 | 23 |
| 27 1350 23 3100 | 25 |
| 25 1350 23 35 2550 | 7 |
| 29 1250 27 18 2300 | 13 |
| 20 1250 13 65 2400 | 20. |
| 31. · | _ |
| AVERAGE 1320 158 • 138 2533 | 33 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH August YEAR 1970

| | WASUT PLA | Mil Carre M.L. | | DRAIN | EAST PLA | WP OUTS THE |
|---------|-----------------|--------------------|---------|-----------------------------------|----------|---------------------|
| DAY | G-3 /** |) (106m) (106m) | Gal/Min | ppm P ₂ 0 ₅ | Gadi/Min | ppm Pa05 (Total) |
| 1 | j 1170 | 1 45 | !) | | , 2400 | 15 |
| 2 | 1050 | 62 | | | 1 2700 | 11 |
| 3 | 1050 | 18 | | 13 | 2500 | 15 |
| 4 | ; 1100 | 11 | | 35 | 2550 | 13 |
| 5 | <u> </u> 1450 | 23 | | 13 | 2400 | 20 |
| 5 | 1250 | 48 | | 28 | 2550 | 11. |
| 7 | 1300 | 18 | | 8 | 3100 | 13 |
| 8 | 1300 | 25 | Ì | | 2700 | 8 |
| 9 | 1300 | 13 | il | | 2550 | 11 |
| 10 | 1450 | 17 | .1 | 13 | 2550 | 13 |
| | 1250 | 67 | | 8 | 2550 | 15 |
| 12 | 1500 | 20 | | . 8 | 2550 | 17 |
| 13 | 1300 | 30 | | 8 | 2950 | 88 |
| 14 | 1300 | 20 | | 15 | 2950 | 13 |
| 15 | : 1350 | 11 | | | 2200 | 13 |
| 16 | 1500 | 53 | ii . | | 3100 | 7 |
| 17 | 1300 | 7 | | 11 | 2500 | 18 |
| 18 | 1170 | 11 | | 183 | 2550 | 27 |
| 19 | 1600 | 27 | | 139 | 2550 | 27 |
| 20 | 1300 | 17 | | 7 | 2550 | 7 |
| 51 | 1170 | 11 | | 5 | 2500 | 18 |
| 22 | 1500 | 15 | ļļ. | | 2950 | 23 |
| 23 | 1300 | 95 | | | 3100 | 8 |
| 21, | 1300 | 169 | | 20 | 2700 | 11. |
| 25 | 11+50 | 165 | | 25 | 2950 | 20 |
| 25 | 1450 | 25 | | 78 | 2400 | 15 |
| 27 | 700 | 53 ⁻ | | 2014 | 2550 | 23 |
| 23 | , 760 | 35 | | 8 | 2300 | 7 |
| 29 | 1450 | | | | 2050 | |
| 30 | 1600 | 35 | | | 2750 | 11 |
| 31. | 1500 | 44 | | 173 | 2400 | 30 |
| AVERAGE | 1296 | 40 | • | 47 | 2614 | 15 |

MINERALB AND CHEMICAL DIVIBION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH July YEAR 1970

| | WEST PLA | NT OUTFALL | 10" E | | EAST PLAN | T OUTFALL |
|---------|-------------|---|---------|--|------------------|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 1 | 1300 | 25 | | 390 | 2550 | 75. |
| 2 | 1500 | 15 | | | 2650 | 30 |
| 3 | 1500 | 92 | | | 2550 | 17 |
| 4 | 1100 | | | | 2650 | |
| 5 | 1300 | 30 | | 135 | 2400 | 17 |
| 6 | 1300 | 25 | | · | 2400 | 17 |
| 7 | 1250 | 17 | | 33 | 2950 | 1.8 |
| 88 | 1300 | 33 | | 30 | 3100 | 13 |
| 9 | 1250 | 230 | | 27 | 2750 | 13 |
| 10 | 1170 | 210 | | J+5 | 2950 | 37 |
| 11 | 1350 | 23 | | | 2950 | 17 |
| 12 | 1350 | 17 | | | 2500 | 18 |
| 13 | 1300 | 17 | | 336 | 2300 | 13 |
| 14 | 1900 | 37 | | 13 | 2300 | 18 |
| 15 | 1350 | 57 | | 15 | 2300 | 88 |
| 16 | 1350 | 35 | | 35 | 2650 | 15 |
| 17 | 1450 | 53 | | 13 | 2650 | 7 |
| 18 | 1450 | . 57 | | | 2550 | 13. |
| 19 | 1650 | 39 | | | 2700 | 25 |
| 20 | 1350 | 120 | | 7 | 2300 | 11 |
| 21 | 1350 | 55 | | <u> </u> | 2550 | 27 |
| 22 | 1300 | 17 | | 11 | 2650 | 17 |
| 23 | 1150 | 50 | | 3 | 2750 | 7 |
| 24 | 1350 | 35 | | 23 | 2300 | 7 |
| 25 | 1650 | 74 | | | 2750 | 13 |
| 26 | 1450 | -18 | | | 2650 | 8 |
| 27 | 1170 | 236 | | 17 | 3000 | 27 |
| 28 | 1300 | 83 | | 80 | 21+00 | 39 |
| 29 | 1170 | 67 | | 11 | 2400 | 23 |
| 30 | 920 | 39 | | 8 | 2650 | 17 |
| 31 | 980 | 55 | · | 7 | 2500 | 18 |
| AVERAGE | 1287 | 62 | | 61 | 2611 | 20 |
| | | | | | ~- | <u>-~</u> |

MINERALB AND CHEMICAL DIVISION

P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH June YEAR 1970

| , | WEST PLAN | NT OUTFALL | 10" I | | EAST PLA | WT OUTFAIL |
|----------------|-----------|---|---------|--|----------|---|
| • DVA | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) ⁵ |
| 1 | 1170 | 46 | | 78 | 2300 | 17 |
| 2 | 1350 | 65 | | 50 | 2550 | 18 |
| 3 | 1450 | 13 | | 28 | 2200 | 13 |
| 14 | 1250 | 35 | | 13 | 2750 | 15 |
| 5 | 1250 | 55 | | 44 | 2500 | 18 |
| 66 | 1450 | 37 | | | 2750 | 20 |
| 7 | 1170 | 95 | | | 2400 | 18 |
| . 8 | 1250 | 210 | | 193 | 2700 | 5 5 |
| 9 | 1750 | 53 | | 3 | 2700 | 33 |
| 10 | 1250 | 39 | | 127 | 2700 | 30 |
| 11 | 1450 | 11 | | 405 | 2700 | 70 |
| 12 | 2150 | 115 | | 3500 | 5500 | 236 |
| 13 | 1450 | 39 | | ** | 3300 | 53 |
| 14 | 1750 | 17 | | | 2950 | 86 |
| 15 | 1300 | 18 | · | 37 | 2500 | 13 |
| 16 | 1300 | 1414 | | 80 | 2700 | 15 |
| | 1170 | 105 | | 25 | 2400 | 13 |
| 18 | 1250 | 17 | | 17 | 2200 | 20 |
| 19 | 1450 | 35 | | 15 | 2400 | 127 |
| 20 | 1500 | 110 | | | 2550 | 8 |
| 21. | 1450 | 57 | | | 2500 | 13 |
| 22 | 1600 | 13 | | 39 | 2550 | - 17 |
| 23 | 1500 | 27 | | 30 | 2950 | 18 |
| 5/+ | 1500 | 25 | | 30 | 2550 | 15 |
| 25 | 1500 | 35 | | 78 | 2750 | 27 |
| 26 | 1500 | 37 | | 420 | 2300 | 108 |
| 27 | 1250 | 18 | | · | 2750 | 11 |
| 28 | 1250 | 46 | | | 2750 | 20 |
| 29 | 1350 | 50 | | 28 | 2950 | 20 |
| 30 | 1450 | 13 | | 69 | 2550 | 30 |
| 31 | | | | | | |
| AVERAGE | 1415 | - 46 | | 241 | 2635 | 39 |
| | | | | | - 11 | |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH May YEAR 1970

| <u>,</u> | WEST PLAN | T OUTFALL | 10" D | | EAST PLA | NT OUTFILL |
|------------------|-----------|---|---------|--|----------|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 11 | 1600 | 27 | | 11 | 2300 | 13 |
| 2 | 1850 | 86 | | | 2650 | 17 |
| 3 | 1600 | 16 | | | 2550 | 13 |
| 4 | 1600 | 72 | | 7 | 2650 | 17 |
| 55 | 1900 | 11 | | 5 | 2650 | 11 |
| <u></u> 6 | 1350 | 11 | | 7 | 2650 | 8 |
| - 7 | 1650 | 17 | | 11 | 2550 | 11 |
| 8 | 1300 | 204 | | 67 | 2400 | 20 |
| . 9 | 1350 | 127 | | | 3100 | 11 |
| 10 | 2150 | 46 | , | | 2950 | 11 |
| 11 | 1050 | 15 | | 5 | 2550 | 7 |
| <u> </u> | 1250 | 155 | | 18 | 2550 | 8 |
| 13 | 1250 | 80 | | 3 . | 2750 | 5 |
| 14 | 1250 | 15 | | 3 | 2950 | 5 |
| 15 | 1050 | 35 | | 13 | 3000 | 5 |
| 16 | 1100 | | | | 2950 | |
| 17 | 1300 | 44 | | | 2550 | 17 |
| 18 | 1900 | | | 8 | 2750 | 18 |
| . 19 | 1170 | 60 | | 20 | 2500 | 11 |
| 20 | 1450 | 350 | | 183 | 2550 | 37 |
| 21 | 1900 | 139 | | 20 | 3300 | 7 |
| 22 | 1100 | 83 | | 42 | 3150 | 25 |
| 23 | 1170 | 27 | | | 3100 | 8 |
| 2 ¹ ÷ | 1170 | 188 | | | 2700 | 18 |
| 25 | 980 | 11 | | 30 | 3000 | 13 |
| 26 | 1650 | 18 | | 62 | 2650 | 15 |
| 27 | 1650 | 8 | | • | 2550 | 13 |
| 20 | 1450 | 42 | | 33 | 2500 | 7 |
| 29 | | | | 4 - 4 - 4 - 4 - 4 | | |
| 30 | 1600 | 108 | | | 2700 | 15 |
| 31 | 1750 | - 27 | | | 3100 | 15 |
| AVERAGE | 1396 | 72 | | 29 | 2743 | 13 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 63201

WASTEWATER DATA

MONTH April YEAR 1970

| | WEST PLAN | NT OUTFALL | 10" D | | EAST PLAI | VT OUTFYLL |
|----------|-----------|---|-------------|--|-----------|---|
| • DVA | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 1 | 1450 | 72 | | 28 | 1850 | 17 |
| 2 | 1350 | 183 | | 28 | 1850 | 13 |
| 3 | 1500 | 86 | | 17 | 1650 | 23 |
| <u>}</u> | 1450 | 85 | | <u> </u> | 2050 | 23 |
| 5 | 1500 | 44 | | | 2050 | . 11 |
| 6 | 1350 | 67 | | 18 | 1900 | 13 |
| 7 | 1300 | 15 | | 20 | 1950 | 13 |
| 8 | 1500 | 11 | | 25 | 1950 | 13 |
| . 9 | 1500 | 11. | | 11 | 2200 | 8 |
| 10 | 1450 | रिर्म | | 11. | 2200 | 11 |
| 11 | 1500 | 35 | | | 2400 | 7 |
| 12 | 1500 | 3 | | | 2050 | 5 |
| 13 | 1500 | 20 | | `15 | 2150 | 8 |
| 714 | 1350 | 50 | | 30 | 2300 | 11 |
| 15 | 1250 | 15 | | 11 | 2200 | 8 |
| 16 | 1650 | 15 | | 15 | 2300 | 23 |
| 17 | 1500 | 17 | | 11 | 2500 | 15 |
| 18 | 1500 | 147 | | | 2700 | 17 |
| 19 | 1600 | 42 | | | 3150 | 8 |
| 20 | 1750 | 151 | | 60 | 2950 | 30 |
| 21 | 1650 | 33 | | 13 | 2550 | 17 |
| - 22 | 1650 | 13 | | 20 | 2700 | 8 |
| 23 | 2150 | 18 | | 18 | 2050 | 13 |
| 214 | 2200 | 25 | | 39 | 2750 | 15 |
| 25 | 1650 | 57 | | | 2550 | 13 |
| 26 | 1600 | 65 | | | 2750 | 8 |
| 27 | 1750 | 65 | | 18 | 2550 | 8 |
| 28 | 1600 | 86 | | 148 | 2750 | 33 |
| 29 | 1750 | 1414 | | 18 | 2550 | 20 |
| 30 | 1600 | 37 | | 11 | 2650 | 8 |
| 31 | | | · | | | |
| AVERAGE | 1535 | 52 | | 22 | 2340 | 14 |
| () | | | | | | |

MINERALB AND CHEMICAL DIVIDION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH March YEAR 1970

| | WEST PLAN | T OUTFALL | 10" D | | EAST PLA | VT OUTFYLL |
|---------|-----------|---|---------|--|----------|---|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (TotaI) | Gal/Min | ppm P ₂ O ₅ (Tote1) ⁵ |
| l | 1600 | 89 | | | | 18 |
| 22 | 1500 | 18 | | 325 | 2650 | 8 |
| 3 | 1650 | 11 | | 33 | 2150 | 1.8 |
| 4 | 1650 | 75 | | 86 | 1950 | 23 |
| 5 | 1650 | 48 | | 25 | 2050 | 25 |
| 6 | 1450 | 78 | | 92 | 2400 | 17 |
| 7 | 1500 | 135 | | | 2700 | 23 |
| 8 | 1350 | 178 | 1 | | 2950 | 62 |
| 9 | 1450 | 92 | | 30 | 2500 | 18 |
| 10 | 1500 | 60 | | 13 | 2500 | 8 |
| 11 | 1300 | 8 | | 25 | 5,100 | 13 |
| 12 | 1450 | 92 | | 20 | 2050 | 18 |
| 13 | 1300 | 20 | | <u> </u> | 2650 | 35 |
| 14 | 1500 | . 13 | | | 2950 | 17 |
| 15 | 1600 | 143 | | | 2650 | 18 |
| 16 | 1250 | 500 | | 67 | 2500 | 27 |
| 17 | 1500 | 98 | | 37 | 2650 | 30 |
| 18 | 1300 | 23 | | 15 | 2500 | 20 |
| 19 | 1500 | 173 | | 390 | 2500 | 30 |
| 20 | 1350 | 15 | | 151 | 2700 | 17 |
| 21 | 1600 | 83 | | | 2650 | 15 |
| 22 | 1450 | | | | 3000 | |
| 23 | 1250 | 165 | | 37 | 2650 | 15 |
| 214 | 1350 | 600 | | 18 | 2750 | 33 |
| 25 | 1300 | 23 | | 27 | 2650 | 7 |
| 26 | 1300 | 127 | | 42 | 2750 | 17 |
| 27 | 1500 | | 6 | •20 | 1900 | |
| 28 | 1350 | | | | 2550 | |
| 29 | 1600 | 62 | | | 2150 | 8 |
| 30 | 1350 | 143 | | 18 | 2300 | 13 |
| 31 | 1500 | 98 | | 11 | 2150 | 7 |
| AVERAGE | 2110 | 113 | | 70 | 2597 | 20 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH Feburary YEAR 1970

| | WEST PLAN | T OUTFALL | 10" D | | EAST PLA | NT OUTFYLL |
|---------|-----------|---|---------|--|----------|---|
| DVA | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) ⁵ |
| 1 | 1750 | | | | 31.00 | 28 |
| 2 | 1600 | 160 | | 460 | 2550 | 1 05 |
| 3 | 1450 | 460 | | 135 | 2550 | 37 |
| j 4 | 1450 | 67 | | 28 | 2400 | 15 |
| 5 | 1600 | 62 | | 50 | 2400 | 23 |
| ે ઇ | 1350 | 135 | | 143 | 2650 | 78 |
| 7 | 1.600 | 92 | | | 2550 | 23 |
| . 8 | 1500 | 102 | | | 2550 | 25 |
| . 9 | 1500 | 86 | | 39 | 2300 | 17 |
| 10 | 1300 | 72 | | 30 | 2200 | 18 |
| 11 | 1600 | 102 | | 102 | 2300 | 11 |
| 12 | 1850 | 50 | | . 86 | 2500 | 17 |
| 13 | 1650 | 95 | | <u> </u> | 2400 | 15 |
| _ 1կ | 1750 | 295 | | | 2700 | 15 |
| 15 | 1750 | 23 | | · · · · · · · · · · · · · · · · · · · | 3000 | 17 |
| 16 | 1850 | 105 | | 75 | 3000 | 88 |
| 17 | 1850 | 72 | | 23 | 2950 | 8 |
| 18 | 1500 | 33 | | 27 | 2750 | 17 |
| 19 | 1450 | 230 | | 950 | 2700 | 390 |
| 20 | 1170 | 80 | | 1230 | 2700 | 17 |
| 21 | 1450 | 147 | | | 2300 | 450 |
| 55 | 1750 | 75 | | | 2650 | 25 |
| 23 | | | | | | |
| 24 | 1500 | 204 | | 300 | 2550 | 72 |
| 25 | 1600 | 139 | | 215 | 2400 | 46 |
| 26 | 1600 | 92 | | 35 | 2050 | 18 |
| 27 | 1650 | 53 | | 178 | 2300 | 112 |
| 28 | | • | | | | |
| 29 | | | | | | |
| 30 | | | | | | |
| 31 | | · | | | | |
| AVERAGE | 1580 | 121 | | 218 | 2558 | 60 |

MINERALS AND CHEMICAL DIVISION

P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH January YEAR 1970

| | WEST PLAN | T CUTFALL | 10" D | | EAST PLAN | VT OUTFALL |
|------------|-----------|---|----------|--|-----------|---|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min. | ppm P ₂ O ₅ (TotaI) | Gal/Min | ppm P ₂ O ₅ (Total) ⁵ |
| 1 | ji | | | | | |
| 2 | 1600 | 147 | | . 55 | 2950 | 37 |
|] 3 | 1900 | 252 | | | 3100 | 20 |
| 4 | 1450 | 650 | | | 3100 | 13 |
| 5 | 1600 | 230 | | 75 | 2950 | 7 |
| 6 | 1500 | 173 | | 37 | 2750 | 17 |
| 7 | 1450 | 183 | | 120 | 3400 | 39 |
| 8 | 1500 | 150 | | 123 | 3400 | 37 |
| 9 | 1650 | 151 | | 350 | 3000 | 67 |
| 10 | 1750 | 570 | | | 3100 | 102 |
| <u>11</u> | 1750 | 362 | | | 3150 | 30 |
| 12 | 1850 | 270 | | 13 | 2950 | 17 |
| 13 | 1650 | 72 | | 20 | 3000 | 27 |
| <u> 14</u> | 1650 | 123 | | 55 | 3000 | 20 |
| 15 | 1500 | 98 | | 57 | 3100 | 28 |
| 7.6 | 1650 | 105 | | . 139 | 3000 | 33 |
| 17 | 1500 | 25 | | | 2700 | 20 - |
| 18 | 1500 | 18 | · | | 2950 | 57 |
| 19 | 1450 | 178 | | 37 | 2700 | 1.8 |
| 20 | 1500 | 95 | • | 18 | 2750 | 11 |
| | 1500 | 98 | | 46 | 2750 | 30 |
| 22 | 2150 | 15 | | 27 | 2750 | 11. |
| 23 | 1600 | 800 | | 570 | 2700 | 173 |
| 24 | 1300 | 23 | | | 3100 | 15 |
| 25 | 1850 | 17 | | | 3000 | 15 |
| 26 | 1600 | 200 | | 480 | 2750 | 127 |
| 27 | 1750 • | 252 | | 39 | 2950 | 17 |
| 28 | 1600 | 1780 | | 28 | 2300 | 13 |
| <u> </u> | 1750 | 67 | | 130 | 2700 | 25 |
| 30 | 1650 | 198 | | 165 | 2700 | 67 |
| 31 | 1750 | 75 | | | 2700 | 28 |
| AVERAGE | 1630 | 246 | | 123 | 2915 | 37 |

MINERALS AND CHEMICAL DIVIBION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH December YEAR 1969

| Cal/Min (Total) | | WEST PLAN | T OUTFALL | 10" I | | EAST PLA | NT OUTFILL |
|---|-------------|---------------------------------------|--|---------|--|----------|--|
| 2 | DVA | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 3 | 1 | 1450 | 169 | | 25 | 2700 | 8 |
| 4 | 1 2 | 1450 | 80 | | 23 | 2650 | 11 |
| 5 1450 48 30 2950 17 6 1600 25 2950 13 7 1600 120 2700 3 8 1450 62 35 2950 23 10 1450 200 3 2400 7 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 11 1600 18 13 1450 15 2950 11 11 1600 18 13 1450 55 2950 11 11 1600 10 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 8 18 1600 57 98 2700 33 19 1600 13 19 1600 | f 3 | | 23 | | 7 | 2400 | 33 |
| 6 1600 25 2950 13 7 1600 120 2700 3 8 1450 62 35 2950 23 9 1170 78 42 2700 13 10 1450 200 3 2400 7 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 300 300 17 | 4 | | 27 | | 27 | 2700 | 13 |
| 7 1600 120 2700 3 8 1450 62 35 2950 23 9 1170 78 42 2700 13 10 1450 200 3 2400 7 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 3000 15 3000 17 21 1600 3000 17 < | 5 | 1450 | 48 | | 30 | 2950 | 17 |
| 8 1450 62 35 2950 23 9 1170 78 42 2700 13 10 1450 200 3 2400 7 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 14 2950 18 20 1450 3300 15 21 1600 55 39 3100 17 23 1650 17 2400 23 | 66 | 1600 | 25 | | | 2950 | 13 |
| 9 1170 78 42 2700 13 10 1450 200 3 2400 7 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 8 18 1600 57 98 2700 8 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 3000 15 21 1600 55 39 3100 17 23 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | <u> 7</u> | 1600 | 120 | | | 2700 | 3, |
| 10 | 8 | 1450 | 62 | | 35 | 2950 | 23 |
| 11 1500 700 105 2500 25 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 14 2950 18 20 1450 3300 15 21 1600 3000 17 23 1650 2950 2950 24 25 25 27 1600 17 2400 23 28 1650 28 30 3100 20 30 1650 89 390 3100 67 < | . 9 | 1170 | 78 | | 42 | 2700 | 13 |
| 12 1500 39 25 2400 18 13 1450 55 2950 11 14 1600 110 3000 17 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 144 2950 18 20 1450 3300 15 21 1600 3000 17 23 1650 2950 17 24 25 24 25 26 27 1600 17 2400 23 23 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 | 10 | | 200 | | 3 | 2400 | 7 |
| 13 | 11 | 1500 | 700 | | 105 | 2500 | 25 |
| 1¼ 1600 110 3000 17 15 1600 80 33 2500 17 16 1¼50 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 ¼4 2950 18 20 1¼50 3300 15 21 1600 3000 15 21 1600 55 39 3100 17 23 1650 2950 2950 2950 24 25 26 27 1600 17 2¼00 23 23 1600 13 2¼00 23 23 23 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 | 12 | | 39 | | 25 | 2400 | 18 |
| 15 1600 80 33 2500 17 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 3300 15 21 1600 3000 15 21 1600 3000 17 23 1650 2950 2950 24 25 25 2950 24 25 24 2400 23 23 1600 17 2400 23 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | | · · · · · · · · · · · · · · · · · · · | 55 | | | 2950 | 11. |
| 16 1450 46 53 2700 27 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 3300 15 21 1600 3000 15 22 1600 55 39 3100 17 23 1650 2950 2950 2950 2950 24 25 26 24 24 29 2400 23 23 28 1600 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | | <u> </u> | | | | | 17 |
| 17 1500 55 15 2700 8 18 1600 57 98 2700 33 19 1600 13 14 2950 18 20 1450 3300 15 21 1600 3000 15 22 1600 55 39 3100 17 23 1650 2950 2950 2950 24 25 26 27 1600 17 2400 23 23 1650 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | | <u> </u> | } | _ | 33 | 2500 | 17 |
| 18 1600 57 98 2700 33 19 1600 13 44 2950 18 20 1450 3300 15 21 1600 3000 15 22 1600 55 39 3100 17 23 1650 2950 2950 2950 2950 24 25 26 29 2400 23 23 1600 17 2400 23 23 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | | 1 | · · · · · · · · · · · · · · · · · · · | | 53 | 2700 | |
| 19 1600 13 44 2950 18 20 1450 3300 15 21 1600 3000 3000 22 1600 55 39 3100 17 23 1650 2950 2950 2950 2950 24 25 29 2400 23 23 28 1600 17 2400 23 23 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | | · · · · · · · · · · · · · · · · · · · | | | | Ît | |
| 20 1450 3300 15 21 1600 3000 3000 22 1600 55 39 3100 17 23 1650 2950 | S | ' | | _ | | 2700 | |
| 21 1600 3000 22 1600 55 39 3100 17 23 1650 2950 | 19 | }} | 13 | _ | 1/4 | 2950 | 18 |
| 22 1600 55 39 3100 17 23 1650 2950 2950 24 25 39 2950 25 30 29 20 27 1600 17 2400 23 23 1600 13 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | 20 | } | | | | 3300 | 15 |
| 22 1600 55 39 3100 17 23 1650 2950 </td <td>21</td> <td>1600</td> <td></td> <td></td> <td></td> <td>3000</td> <td></td> | 21 | 1600 | | | | 3000 | |
| 24 25 30 31 1650 1120 30 330 330 300 120< | | 1600 | 55 | | 39 | 3100 | 17 |
| 25 | 23 | 1650 | | | | 2950 | |
| • 26 1600 17 2400 23 23 1600 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 144 | 24 | | | | | | |
| • 26 1600 17 2400 23 28 1600 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 144 | | | | | | | |
| 28 1600 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 144 | | | | | | | |
| 28 1600 13 29 1650 28 30 3100 20 30 1650 89 390 3100 67 31 1650 1120 70 3300 144 | 27 | 1600 | 17 | | | 2400 | 23 |
| 30 1650 89 390 3100 67 31 1650 1120 70 3300 44 | 23 | 1600 | · · · · · · · · · · · · · · · · · · · | | | | |
| 31 1650 1120 70 3300 44 | | 1650 | 28 | | 30 | 3100 | 20 |
| | 30 | 1650 | 89 | | 390 | 3100 | 67 |
| er ii II i l | 31 | 1650 | 1120 | • | 70 | | 44 |
| AVERAGE 1540 130 58 2768 20 | AVERAGE | 1540 | 130 | | 58 | [1] | 20 |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH November YEAR 1969

| ļ | | WT OUTFALL | 10" D | | EAST PLA | NT CUTEVIL |
|---------|----------|---|---------|--|----------|--|
| DAY | Gal/Min_ | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 11 | 1850 | 33 | | | 2400 | 57 |
| 2 | 1600 | 37 | | | 2750 | 123 |
| 3 | 2150 | 37 | | 102 | 2500 | 25 |
| 4 | 1650 | 336 | | 20 | 2300 | 8 |
| 5 | 2400 | 139 | | 236 | 2150 | 50 |
| · 6 | 1450 | 27 | | 260 | 2400 | 70 |
| 7 | 1600 | 102 | . | 276 | 2550 | 105 |
| 8 | 1600 | | | | 2950 | 57 |
| 9 | 1650 | | | | 2700 | 28 |
| 10 | 1650 | 204 | | 210 | 2400 | 33 |
| 11 | | |) | | | |
| 12 | 1600 | 173 | | 57 | 2650 | 123 |
| • 13 | 1600 | 405 | | <u>.</u> 83 | 2550 | 25 |
| J14 | 1600 | 35 | | 169 | 2300 | յ _ե յ _ե |
| 15 | 1900 | 780 | · | | 2550 | 37 |
| 16 | 1600 | 65 | | | 2750 | 83 |
| 17 | 1600 | 23 | | 60 | 2950 | 53 |
| 18 | 1750 | 222 | | 25 | 2650 | 5 |
| 19 | 1950 | 50 | | 35 | 2650 | 15 |
| 20 | 1750 | 147 | | 78 | 3100 | 18 |
| 21 | 1250 | 112 | | 178 | 3000 | 53 |
| 22 | 1650 | 260 | | | 2650 | 25 |
| 23 | 1450 | 193 | | | 2950 | |
| 24 | 1300 | 260 | | 98 | 2550 | 25 |
| 25 | 1600 | 270 | | 23 | 3000 | 8 |
| 26 | 1600 | 108 | | 13 | 2550 | 8 |
| 27 | | 165 | | • | | |
| 28 | 1500 | 376 | | 139 | 2300 | 8 |
| 29 | 1600 | 7474 | | | 2650 | |
| 30 | 1600 | 165 | | | 2650 | 13 |
| 31 | | · | | | | |
| AVERAGE | 1660 | . 176 | | 115 | 2541 | 42 |
| | | · · · · · · · · · · · · · · · · · · · | | | | |

MINERALS AND CHEMICAL DIVISION

P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH October YEAR 1969

| 70.435 | WEST PLA | NT OUTPALL | 10" 1 | | EAST PLA | VP OUTE ALL |
|-----------------|----------|--|---------|--|----------|---------------------|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Hin | ppm Pc05 (Total) |
| 1 | 1600 | 92 | | 7 | 2950 | 5 |
| 2 | 1450 | 860 | | 89 | 2700 | 27 |
| 3 | 1450 | 80 | | 15 | 2750 | 44 |
| 4 | 1500 | 151 | | <u> </u> | 2700 | 28 |
| 5 | 1600 | 135 | | | 2750 | 30 |
| 6 | 1600 | 405 | | 20 | 2550 | 23 |
| 7 | 1450 | 27 | | 18 | 2550 | 700 |
| 8 | 1750 | 1120 | | 25 | 3500 | 390 |
| . 9 | 1450 | 350 | | 27 | 2550 | 15 . |
| 10 | 1450 | 62 | | 151 | 2200 | |
| 11 | 1750 | 362 | | | 2550 | 23 |
| 12 | 1750 | 15 | i[| | 2700 | 1+14 |
| 13 | 1450 | 280 | | 53 | 2550 | 35 |
| Įlį | 1500 | 280 | | 62 | 2400 | 25 |
| 15 | 1600 | 280 | | 169 | 2500 | 53 |
| 16 | 1450 | 530 | | 3300 | 2700 | 890 |
| 17 | 1500 | 67 | | 62 | 2500 | 3 |
| 3.8 | 1350 | 236 | | | 2500 | 39 |
| .19 | 1450 | 169 | | | 2650 | 127 |
| 20 | 1300 | 330 | | 135 | 2400 | 42 |
| 21 | 1450 | 860 | | 130 | 2300 | 78 |
| 22 | 1450 | 250 | | 350 | 2400 | 86 |
| 23 | 1450 | 1650 | | 110 | 2400 | 30 |
| 2) _† | 1600 | 80 | | 46 | 2300 | 5 |
| 25 | 1450 | | | | 2300 | |
| 26 | 1600 | | | | 2700 | |
| 27 | 1600 | 500 | | 160 | 2300 | 33 . |
| 28 | 1300 | 390 | | 210 | 2300 | 53 |
| 29 | 1300 | 276 | | 700 | 2200 | 165 |
| 30 | 1650 | 376 | | 285 | 2700 | 89 |
| 31 | 1600 | 70 | • | 169 | 2300 | 46 |
| AVERAGE | 1510 | 354 | | 274 | 2554 | 112 |

MINERALS AND CHEMICAL DIVISION P. O. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH September YEAR 1969

| | WEST PLAI | NT OUTFALL | 10" D | | EAST PLAT | EAST PLANT OUTFILL | | |
|-----------|-----------|---|---------|--|-----------|--|--|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | nom P ₂ O ₅ (Total) | | |
| 1 | li | | | | | | | |
| 2 | 1650 | <u>լ</u> ելե | | 5Q | 2700 | 28 | | |
| 3 | 1500 | 35 | | 60 | 2500 | 8 | | |
| <u>}</u> | 1650 | 25 | | 3 | 2650 | 3 | | |
| 5 | 1600 | | | 42 | 2650 | | | |
| 6 | 1450 | | i | | 2750 | | | |
| 7 | 1600 | 1980 | | | 2950 | 13 | | |
| 8 | 1600 | 120 | | 57 | 2700 | 15 | | |
| 9 | 1650 | 65 | | 236 | 2400 | 53 | | |
| 10 | 1450 | 62 | | 112 | 2550 | 28 | | |
| 11 | 1600 | 57 | | 3 | 2550 | 13 | | |
| 12 | 1350 | 127 | 1 | 280 | 3000 | 23 | | |
| 13 | 1600 | 23 | | <i>^.</i> | 2700 | 55 | | |
| 14 | 1600 | 44 | | | 2500 | 123 | | |
| 15 | 1600 | 18 | | 86 - | 2650 | 188 | | |
| 16 | 1350 | 20 | | 95 | 2650 | 60 | | |
| 17 | 1300 | 27 | | 86 | 2500 | 35 | | |
| 18 | 1300 | 48 | | 30 | 2550 | 18 | | |
| 19 | 1350 | 5 | | 28 | 2750 | 13 | | |
| 20 | 1450 | 25 | - | | 2550 | 15 | | |
| 21 | 1650 | 72 | | | 2700 | 27 | | |
| 22 | 1450 | 210 | | 35 | 2750 | 17 | | |
| 23 | 1350 | 108 | | 89 | 2550 | 37 | | |
| Sj+ | 1100 | 183 | | 55 | 2650 | 27 | | |
| 25 | 1450 | 300 | | 42 | 2050 | 25 | | |
| 26 | 1350 | 188 | | 80 | 2950 | 3 | | |
| 27 | 1350 | 83 | | • | 2550 | 15 | | |
| 23 | 1750 | 188 | | | 2700 | | | |
| 29 | 1450 | 83 | | 151 | 2200 | 3 15 | | |
| <i>29</i> | 1600 | 18 | | 53 | 2950 | 27 | | |
| 31 | • | | · | | 1 2000 | <u> 1</u> | | |
| AVERAGE | 1490 | 151 | | 80 | 2631 | 33 | | |

MINERALB AND CHEMICAL DIVISION P. 0. 80X 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH August YEAR 1969

| | WEST PLAN | T OUTFALL | 10" [| | EAST PLA | NT OUTSTLL |
|---------|-----------|---|---------|--|----------|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | npm P ₂ O ₅ (Total) |
| 1 | 1650 | 600 | | 120 | 2750 | 53 |
| 2 | 1450 | | | | 1450 | |
| 3 | 1500 | 98 | | | 3300 | 8 |
| 4 | 1650 | 480 | | 15 | 3000 | 25 |
| 5 | 1750 | 151 | | 112 | 3100 | 30 |
| 6 | 1.600 | 300 | . | 30 | 3000 | 13 |
| .7 | 1750 | 30 | | 20 | 3400 | 15 |
| 8 | 1600 | 28 | | 25 | 3500 | ! 11 |
| 9 | 1170 | 102 | | | 3500 | 20 |
| 10 | 1500 | 89 | | | 3100 | 5 |
| _11 | 2400 | 210 | | 48 | 2950 | 17 |
| 12 | 1650 | 336 | | . 102 | 1850 | 25 |
| 13 | 1500 | 20 | | 55 | 3100 | 23 |
| 1/4 | 1500 | 28 | | 155 | 3700 | 53 |
| 1.5 | 1300 | 15 | | 80 | 3150 | 25 |
| 16 | 1450 | 1300 | | | 3500 | 28 |
| 17 | 1350 | 18 | | <u> </u> | 3150 | 25 |
| 18 | 1350 | 3 | | 244 | 3150 | 39 |
| 1.9 | 1600 | 1080 | | 165 | 2950 | 20 |
| 20 | 1600 | 25 | | 72 | 2750 | 27 |
| 21 | 1850 | 390 | | 18 | 3300 | 15 |
| 52 | 1650 | 27 | | 198 | 31400 | 62 |
| 23 | 1600 | 39 | | | 2700 · | 35 |
| 24 | 1750 | 62 | | | 2550 | 25 |
| 25 | 1650 | 89 | | 147 | 2500 | 46 |
| 26 | 1900 | 155 | | 72 | 3000 | 27 |
| 27 | 1500 | 130 | | 42 | 2500 | 147 |
| 28 | 1350 | 270 | !! | 72 | 2500 | 20 |
| 29 | 1850 | 33 | | 188 | 2500 | 46 |
| • 30 | 1650 | 160 | | | 2700 | 46 |
| | 1600 | 92 | · | | 3400 | 37 |
| AVERAGE | 1600 | 212 | | 94 | 3077 | 32 |

MINERALS AND CHEMICAL DIVISION

P. G. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH_July YEAR 1969

| | WEST PLAN | T OUTFALL | 10" D | | EAST PLAT | EAST PLANT OUTFILL | | |
|------------|-----------|---|---------|--|-----------|--------------------|--|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | Total) | | |
| ì | 1600 | 112 | | 35 | 3700 | 27 | | |
| 2 | 1600 | 67 | | 151 | 3300 | 59 | | |
| 3 | 1650 | 200 | | 150 | 3300 | 30 | | |
| <u>l</u> ; | 1600 | 105 | | 105 | 2650 | 33 | | |
| 5 | 1900 | 60 | | | 3100 | 62 | | |
| 6 | 1450 | 105 | | | 2950 | 53 | | |
| 77 | 1600 | 50 | | 102 | 3300 | 39 | | |
| 88 | 1750 | 89 | | 183 | 3400 | 35 | | |
| 9 | 1750 | 830 | | 75 | 3700 | 35 | | |
| 10 | 1900 | 1350 | !! | 105 | 3500 | 75 | | |
| 11 | 1650 | 160 | | 151 | 3500 | 67 | | |
| 12 | 1850 | 127 | | <u> </u> | 2950 | 70 | | |
| 13 | 1750 | 98 | | | 3100 | 67 | | |
| Jh | 2400 | 80 | | 37 | 3100 | 55 | | |
| 15 | 1650 | 1700 | i | 35 | 2300 | 33 | | |
| 16 | 1900 | 165 | | 37 | 2750 | 27 | | |
| 17 | 1600 | 42 | | 35 | 2750 | 30 | | |
| 18 | 1750 | 650 | | 35 | 3100 | 46 | | |
| 1.9 | 1750 | 13500 | | | 2550 | 35 | | |
| 20 | 1650 | 63 | j | | 2550 | 39 | | |
| 21 | | | | | | | | |
| 22 | 1600 | 350 | | 25 | 2050 | 35 | | |
| 23 | 1600 | 46 | | 27 | 2300 | 27 | | |
| 24 | 1450 | 75 | | 18 | 2550 | 48 | | |
| 25 | 1450 | 530 | | 86 | 2200 | 23 | | |
| 26 | 1450 | 35 | | | 2200 | 13 | | |
| 27 | 1350 | 27 | | | 2550 | 11 | | |
| 28 | 1600 | 23 | | 5 | 2700 | 8 | | |
| 29 | 1600 | 295 | | 11 | 2700 | 7 | | |
| 30 | 1600 | 530 | | 17 | 2650 | 8 | | |
| 31 | 1900 | 330 | | 8 | 3100 | 42 | | |
| AVERAGE | 1680 | 325 | | 59 | 2885 | 38 | | |

MINERALS AND CHEMICAL DIVISION

P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEMATER DATA

MONTH June YEAR 1969

| | WEST PLA | NT OUTFALL | 10" D | | EAST PLAT | EAST PLANT OUTFALL | | |
|-----------|----------|---------------------|---------|--|-----------|--|--|--|
| DAY | Gal/Min | ppm P205 (Total) | Gal/Min | ppm P ₂ 0 ₅ (Total) | Gal/Min | ppm P _S O ₅ (Total) | | |
| .1 | | | | | | | | |
| 2 | 1650 | 13 | | 183 | 1330 | 25 | | |
| 3 | 1500 | 5 | | 60 | 2700 | 13 | | |
| 4 | 1650 | 18 | | 155 | 3100 | 295 | | |
| 5 | 1850 | 20 | :: | 57 | 4100 | 222 | | |
| 6 | 2050 | | | 120 | 2650 | 53 | | |
| 7 | | i | ji · | | | | | |
| . 8 | | 23 | | | | | | |
| 9 | 1750 | 53 | | 18 | 3300 | 15 | | |
| 10 | 1650 | 115 | | 57 | 3300 | 285 | | |
| 11 | 1600 | 95 | | 57 | 4300 | 60 | | |
| 12 | 1900 | 230 | | 18 | 3100 | 13 | | |
| 13 | 1650 | 83 | | <u>^</u> 123 | 3300 | 37 | | |
| 14 | | | | | li | | | |
| 15 | | | | | | | | |
| 16 | 1650 | 143 | | 27 | 3400 | 3 | | |
| 17 | 1750 | 65 | | 27 | 3300 | 13 | | |
| 18 | 1450 | 151 | | 7 | 3700 | 39 | | |
| 19 | 1170 | 105 | | 15 | 2700 | 42 | | |
| 20 | 1500 | 37 | | 78 | <u>.</u> | 3.7 | | |
| 2). | • | 28 | | | | 30 | | |
| 55 : | · | 198 | li | | | 17 | | |
| 23 | 1650 | 183 | | 37_ | 3500 | 27 | | |
| 5, | . ——— | 48 | | 57 | 3900 | 33 | | |
| 25 | 1650 | | | · · · · · · · · · · · · · · · · · · · | 3150 | | | |
| 20 | 1600 | 86 | | 55 | 3800 | 8 | | |
| 27 | 1600 | 37 | | .72 | 3900 | 173 | | |
| 23 | | 139 | | | | 102 | | |
| 20 | | | | 37 | | | | |
| 30 | 1350 | 160 | | 7 | 3550 | 30 | | |
| 31 | | | | | | | | |
| AVERAGE (| 1630 | 88 | | 60 | 3304 | 67 | | |
| ! | | \ | | | | | | |

MINERALS AND CHEMICAL DIVISION

P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH May YEAR 1969

| | WEST PLAN | VT OUTFALL | 10" D | | | T OUTSILL |
|----------------|-----------|---|---------|--|---------|---|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | nom P ₂ 05 (Total) |
| l | ! 1450 | 62 | | 33 | 3300 | 48 |
| 2 | 1300 | 62 | | 105 | 2930 | 30 |
| 3 | 1170 | | | | 2700 | 46 |
| ĵ [†] | | 80 | | | j 2700 | 23 |
| 5 | 1500 | 39 | | 46 | 2500 | 15 |
| 6 | 1900 | 11 | | 147 | 3100 | 42 |
| 7 | 1650 | 15 | | 13 | 2950 | 143 |
| _ 8 | 1650 | 5 | | 39 | 2750 | 315 |
| 9 | 1650 | | i | 230 | 2750 | 18 |
| 3.0 | | | | | 2950 | 28 |
| 11 | | 15 | | | 2700 | 17 |
| 12 | 1600 | 39 | | 33 | 2750 | 20 |
| 13 | 1850 | 150 | | | 2950 | 260 |
| <u> </u> | 1750 | 300 | | 70 | 3500 | 37 |
| 15 | 1450 | 37 | | 20 | 3100 | 28 |
| 16 | 1450 | | | 3 | 3100 | |
| 17 | | | | | 2700 | |
| 18 | | 102 | | | 2700 | 20 |
| 19 | 1950 | 27 | | 39 | 3150 | 50 |
| 20 | 1750 | 35 | | 18 | 2650 | 25 |
| 21 | 1600 | 67 | | 198 | 2950 | 25 |
| 22 | 1650 | 15 | l . | 188 | 2550 | 50 |
| 23 | 1750 | | | 80 | 3100 | |
| 5j÷ | 1900 | | | | 3300 | |
| 25 . | | 44 | | | 2950 | 17 |
| 25 | 1950 | 15 | | 37 | 2950 | 3 |
| 27 | 1850 | 28 | | .8 | 2650 | 5 |
| 23 | 1450 | 550 | | 7 | 2700 | 20 |
| 29 | 1750 | | | 83 | 2700 | <u>, , , , , , , , , , , , , , , , , , , </u> |
| 30 | | | | | | |
| 31 | 1750 | 27 | | | 3300 | 33 |
| AVERAGE | 1660 | 77 | | 67 | 2903 | 53 |

MINERALS AND CHEMICAL DIVISION P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

MONTH April YEAR 1969

| | WEST PLAN | T OUTFALL | 10" 1 | | EAST PLA | T OUT TIEL |
|------------|-----------|---|----------|-----------------------------------|----------|---|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ | Gal/Sin | opm P _C O ₅ (Totall) |
| 1 | 1500 | 147 | | 5 | 2950 | 28 |
| 2 | 1450 | 147 | | 110 | 2750 | 39 |
| 3 | 1500 | 236 | | 405 | 2550 | 86 |
| 2; | 1600 | 130 | | 23 | 2700 | 23 |
| 5 | 1450 | | <u> </u> | | 2700 | 27 |
| 66 | 1450 | 62 | | | 2700 | 17 |
| 7 | 1450 | 115 | ! | 65 | 2700 | 5 |
| <u>.</u> 8 | 1500 | 155 | li | 23 | 2950 | 25 |
| 9 | 1600 • | 28 | | 405 | 2700 | <u>.</u> |
| 10 | 1650 | 188 | | 230 | 3100 | 44 |
| 11 | 1650 | 89 | | 23 | 3100 | 13 |
| 12 | 1650 | | | | 2550 | 35 |
| 13 | 1600 | 42 | | 8. | 2950 | 30 |
| 14 | 1900 | 276 | | 23 | 2950 | 25 |
| 15 | 1500 | 188 | | 112 | 2700 | 39 |
| <u>ló</u> | 1650 | 86 | | | 2750 | 48 |
| 17 | 1500 | 160 | | 252 | 3100 | 33 |
| . 18 | 1900 | 57 | | 48 | 3400 | 15 |
| 19 | 1650 | 25 | | | 2700 | 11 |
| 20 | | | | | 2400 | 23 |
| 21 | 1650 | 139 | <u> </u> | 15 | 3150 | · 8 |
| 22 | 1750 | 120 | | 83 | 3400 | 18 |
| 23 | 1750 | 75 | | 98 | 3000 | 17 |
| 5Jt | 1600 | 105 | | | 2950 | կկ |
| 25 | 1750 | 120 | | 150 | 3000 | 23 |
| 26 | 1250 | · 325 | | | 3000 | 27 |
| 27 | 1450 | 39 | | | 2700 | 62 |
| 23 | 1350 | 276 | 1 | 620 | 3000 | 92 |
| 29 | 1600 | 23 | · | 180 | 1750 | 31 |
| 30 | 1450 | 2300 | | 44 | 3100 | 8 |
| 31 | | | | | | |
| AVERAGE | 1580 | 209 | | 146 | 2578 | 32 |

MINERALS AND CHEMICAL DIVISION

P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEMATER DATA

MONTH March YEAR 1969

| 53.AM | WEST PLAN | NT OUTFALL | 10" D | | HAST PLAT | T OUT I.I. |
|----------|-----------|---------------------|---------|---|-----------|------------|
| DAY | Gal/Min | ppm P205 (Total) | Cal/Min | ppm P ₂ O ₅ (Total) | j Gal/Hin | Total) |
| l | 1170 | 20 | į | | 2400 | 46 |
| 2 | 1500 | 25 | | | 2950 | 46 |
| 3 | 1300 | 270 | | 46 | 2750 | 27 |
| Ì; | 1450 | 5/1/1 | | 67 | 3100 | 27 |
| 5 | 1170 | 165 | | 65 | 2550 | . 35 |
| ó | 1450 | 170 | | 8 | 2950 | 55 |
| 7 | 1300 | 169 | | | 2950 | 35 |
| 8 | 1600 | 23 | | | 3100 | 75 |
| 99 | 1450 | 80 | | 11 | 2650 | 57 |
| 10 | 1300 | 92 | | 46 | 3000 | 11 |
| _11 | 1450 | 27 | | 130 | 3000 | 42 |
| 12 | 1300 | 160 | | 210 | 2650 | 7 |
| 13 | 1450 | 53 | | 112 | 2700 | 23 |
| J₁t | 1450 | 33 | | 25 | 2950 | 15 |
| 15 | 1450 | 28 | | | 2400 | 198 |
| 16 | 1350 | 23 | | | 3400 | 330 |
| 17 | 1450 | 130 | | 108 | 2650 | 230 |
| 13 | 1500 | 165 | | 210 | 3100 | 50 |
| `.9 | 1750 | 102 | | 130 | 3100 | 11 |
| 20 | 1600 | 78 · | | 18 | 2750 | 20 |
| 21 | 1300 | 33 | | 65 | 2700 | 39 |
| - 22 | 1450 | 11 | . | | 2700 | 46 |
| 23 | 1350 | 5 | | | 2300 | 33 |
| ્રો: | 1500 | 130 | | 60 | 2400 | 7 |
| 25 | !' 1450 | 46 | | 18 | 2700 | 18 |
| 26 | 1600 | 89 | | 1230 | 2550 | 420 |
| 27 | 1300 | 102 | | 150 | 2650 | 11 |
| 28 | 1450 | | | | 2400 | |
| 09 | 1600 | | !! | | 2550 | |
| | 1450 | 130 | | | 3100 | 48 |
| | 1170 | 13 | | 135 | 2700 | 39 |
| A /BRACA | 1380 | 90 | : | 142 | 2689 | 69 |

MINERALS AND CHEMICAL DIVISION P. Q. BOX 912

POCATELLO, IDAHO 83201

WASTEMATER DATA

MONTH February YEAR 1969

| | SUP PLAI | NI OUTPALL | : 10" D | | EAST PLA | Ar Other Call |
|-----------------|----------|---------------------|---------|--|-----------|---------------|
| DVA | | ppm 1205 (Total) | Gal/Min | ppm P ₂ 0 ₅ (Total) | Gad./Wile | Total |
| | · | | | 1 | il | 15 |
| Ω. | 1300 | 50 | | | 2400 | 15 |
| 3 | 1450 | 105 | | 570 | 2400 | 75 |
| 14 | 1170 | 120 | | 7 | 3100 | 160 |
| 5 | 1170 | 200 | · | 11 | 2050 | 160 |
| <u></u> ဝ် | 1170 | | i: | 23 | 3100 | |
| 7 | 1300 | 460 | E . | 11 | 3100 | 350 |
| 8 | 1750 | 8 | i | | i: 3300 | 35 |
| 9 | 1300 | 50 | | | 2550 | 530 |
| 10 | 1250 | 50 | . | 236 | 2500 | 170 |
| li ! | 1250 | 48 | i | | 2150 | 130 |
| 12 | 1170 | 160 | | 50 | 2700 | 15 |
| 13 | 1050 | 260 | | 39 | 3300 | 23 |
| ìl _t | 1170 | 127 | | | 3100 | 30 |
| 15 | 1170 | 39 | | | 3300 | 25 |
| 16 | 1300 | 17 | ii | 20 | 3300 | 78 |
| 17 | 1250 | 60 | | 108 | 3300 | 95 |
| 18 | 920 | 80 | | 110 | 2750 | 50 |
| 19 | 980 | 62 | | 268 | 2650 | 42 |
| 20 | | 1 | | | () (i | |
| 21. | 800_ | | | | 2550 | |
| 20 | 920 | | | | 2550 | |
| 21 | 1300 | 23 | | 210 | 2700 | 42 |
| 21. | 1350 | 178 | | 236 | 2700 | 105 |
| 23 | 1100 | 98 | | 155 | 3300 | 42 |
| 20 | | 139 | | 160 | 3100 | 42 . |
| 27 | | <u> </u> | | | | |
| | 1600 | 44 | | 500 | 2400 | 102 |
| <u>23</u> | | | • | 280 | 2550 | 62 |
| 29 | | : , | | · | | - |
| <u>?)</u> | | · | | | | · |
| 31 ! | | | | | | |
| VERAGE | 1220 | 108 | | 158 | 2803 | 98 |
| | | | | | 1 | <i>,</i> - |

MINERALB AND CHEMICAL DIVIBION
P. D. BOX 912

POCATELLO, IDAHO 83201

WASTEWATER DATA

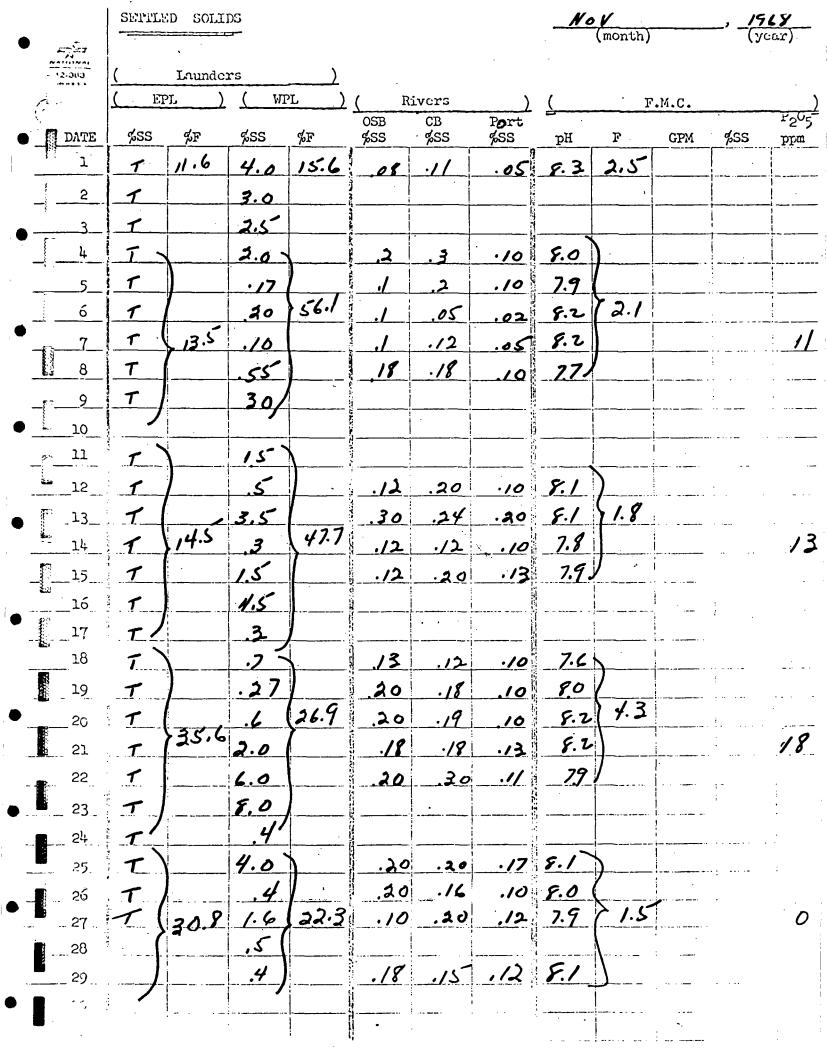
MONTH January YEAR 1969

| | WEST PLAN | NT OUTFALL | 10" I | | EAST PLAN | T OUTFALL |
|---------|-----------|---|---------|---|-----------|--|
| DAY | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) | Gal/Min | ppm P ₂ O ₅ (Total) |
| 1 | | | | | | |
| 2 | 1600 | 200 | | 200 | 4200 | 8 . |
| 3 | 1300 | | | 230 | 2l+00 | |
| 4 | | | | | - | |
| 5 | 1300 | 39 | | | 2700 | 1.1 |
| 6 | 1300 | 1600 | | 148 | 3100 | 25 |
| 7 | 1350 | 180 | | 11 | 3100 | 28 |
| 8 | 1450 | 204 | | 108 | 3100 | 55 |
| 9 | 1450 | 80 | | 13 | 3100 | 27 |
| 10 | 1450 | 147 | | 336 | 3100 | 17 |
| 11 | 1600 | 3150 | | | 2700 | 300 |
| 12 | 1450 | 180 | | <u> </u> | 3100 | 86 |
| 13 | 1450 | 95 | | 5 | 2700 | 55 |
| 14 | 1350 | 350 | | 89 | 2700 | 33 |
| 15 | 1750 | 1600 | | 72 | 2700 | 62 |
| 16 | 1170 | 480 | | 80 | 5,100 | 30 |
| 17 | 2550 | 28 | | 20 | 1450 | 315 |
| . 18 | 1450 | 60 | | <u> </u> | 2700 | 11 |
| 19 | 1450 | 170 | | | 2700 | 20 . |
| 20 | 1750 | 165 | • | 204 | 2550 | 20 |
| 21 | 1450 | 230 | | 65 | 2400 | 1,8 |
| 22 | 1250 | 150 | | 83 | 2400 | 18 |
| 23 | 1250 | 83 | | 7 | 2400 | 15 |
| 5/1 | | · | | 7 | 2200 | 8 |
| 25 | 1350 | 200 | | | 2550 | 37 |
| 26 | 1170 | 112 | | | 2700 | 15 |
| 27 | 1300 | 89 | | •390 | 2200 | 20 |
| 28 | 1450 | 155 | | 270 | 2400 | . 39 |
| 29 | 1450 | 46 | | 15 | 2400 | 60 |
| 30 | 1450 | 39 | . | | 2650 | 27 |
| 31 | 1170 | 72 | | 98 | 2700 | 55 |
| AVERAGE | 1400 | 367 | | 112 | 2672 | 51 |

| | | EFFLU | ENT DIT | Unes | | | | | | (mont | h) | | ear) |
|---|-------------------------|-------------|---|-------------------------------|-------------|-------------------------------|------|----------------------------|-------------------------------|------------|--------------------------------------|--------------|----------------|
| • | ET ET | (| • | EAST | 1 |) | (| | WES | S T | · |) | |
| 1 | 42-363 | pH | Settled Solias Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | рН | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ TPD | SOL | |
| _ | E: 1 | 7.0 | 17 | 39 | 2650 | .6 | 7.5 | .50 | 28 | 1450 | .3 | FOO | |
| • | 2 | 6.7 | 1 | 112 | 2750 | 1.9 | 6.4 | 2.2 | 188 | 1250 | _ | 2125 | |
| | , 3 | 7.1 | T | 33 | 3100 | .6 | 3.9 | .6 | 600 | 1050 | | 750 | |
| | | 73 | T | 60 | 3/00 | | 6./ | i | 460 | 980 | | 600 | ··· |
| • | F-0 | 7.0 | - <u>-</u> - | 89 | | 1.12 | 3 | 10.0 | 420 | | | 950 | |
| | | - | | | 3100 | | 6.0 | 11.5 | | | | | |
| | 9 6 | 68 | 7 | | 3300 | | 6.8 | 4.5 | 1 | 1300 | | 200 | : : |
| • | 7 | 6.5 | T | 183 | 2700 | 3.0 | 6.4 | .3 | 1 | 1300 | i | 325 <u>~</u> | |
| | | 6.9 | | 1 | 3/00 | | 55 | ./ | | 1350 | | * | ! ! |
| | 9 | 6.6 | T | | 3100 | 2.6 | 6.2 | .3_ | | 1450 | 1 | 260 | |
| | 10 | 6.5 | T | | 3300 | | 6.3 | 3.5 | | 1050 | | 472 | <u> </u> |
| • | 11 | 4.4 | T | 57 | 2700 | .9_ | 4.3 | /·/ È | 165 | 1 | | 675 | <u> </u> |
| | 12 | 7.6 | | | 2400 | 1.2 | 3.4 | 1/5 | ! | 1050 | | : | · |
| | 13_ | 7.3 | | i - | 2950 | 1.0 | 6.0 | | 188 | | | 500 | - 2 |
| • | 14_ | 6,7 | T | 86 | 2760 | 1.4 | 6.3 | ٠ <u>٠</u> - ١ | 135 | | 1.2 | | 4 |
| | 15 | 7.7 | T | 2 | 3100 | ./ | 6.6 | | 130 | J | | F25 | # |
| | 1616 | <i>7.</i> 6 | T | 37 | 3100 | .7 | 5.8 | 21.04 | 950 | 1450 | 8.3 | 875 | |
| • | 17_ | 7.6 | T | 28 | 3/00 | .5 | 3.1 | 8.5 | 3500 | 1450 | 30.57 | 400 | <u> </u> |
| | 18 | 7.8 | T | 15 | 2100 | .3 | 7.0 | .6 | 198 | 1300 | 1.6 | 900 | Ď |
| | 19 | 7.6 | T | 80 | 3/00 | ₹.4 | 6.6 | 1.0 | 183 | 1300 | 1.4 | 925 | |
| | 20 | 7.9 | T | 15 | 3100 | .3 | 4.0 | .0 | 350 | 1450 | 3.1 | 1125 | : |
| | 21 | 7.8 | T | 15 | 3100 | .3 | | .4 | 230 | 1450 | 2.0 | | |
| | 22 | 7.7 | + | 42 | 3100 | .8 | 60 | .6 | 420 | 1450 | 3.7 | 500 | : ! |
| • | 23 🚜 | 7.3 | 7 | 25 | 2950 | .5 | 4.3 | .05 | 178 | 1450 | 1.6 | 500 | |
| | 24 | | | | | | | | | | | <u> </u> | |
| ֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֡֓֓֡֓֡֓֡֓֡ | 25 | | : | | | | | | | | · | | <u> </u> |
| | EWA 526 | 7.2 | 7 | 53 | 2700 | .9 | 3.5 | T | 550 | 1450 | 4.8 | 290 | |
| | 27 | 3.5 | T | 268 | 2700 | | 3.5 | 1.0 | 1 | 1450 | i | _ | |
| | 28 | 6.4 | 1 | | 2700 | 1.6 | 6.6 | .5 | 112 | 1450 | 1.0 | 500 | |
| | 29_ | 3.3 | | <u> </u> | 2700 | | 7.4 | .5 | 53 | 1450 | 1 | 675 | |
| | 29 | 7.8 | | | 2700 | ,2 | 6.1 | 1.0 | | 1450 | | 500 | |
| 7 | Reclaim Hzo River 31 | 2.9 | | | 2700 | | 3,5 | | | 147-0 | 1 | Acid for | # 2 vor Flu |
| ' [| | | mpl | | - 4 | 0 | 4 12 | -26- | | 1 | i | | T |
| | . • | | | 3065/1.1. | 18,789 na19 | | | រូវ ខេត្តកំពង់ | 13080/1131 | 138450/233 | ! | | -1 |

| | LDS | | | | De | C | 1768 |
|--|--------------|----------------|-----------|-------------|-------------|--|--------|
| • | | | | | (11 | Conth) | |
| Enunde | nrs) | | | | | | .) |
| | (WPL) | - | ivers |) | <u>(</u> | F.M.C. | |
| • Daniel Si | γss γF | 000 %88 | CB %SS | Fort %SS | pН | F GPM | Car pa |
| T | .50 | 进 | .18 | .10 | F.3 \ | ; ; ; | |
| T | 2.20 | .10 | .30 | .15 | 7.8 | | |
| • , | .60 | .10 | .13 | .10 | 7.9 | 1.6 - | |
| T (| 10.00 | .08 | ./2 | . 09 | 7.9 | | |
| 5 T 28.6 | 11.50 \ 22.8 | .10 | ./2 | .10 | 7.9 | | |
| T | 4.50 | .// | ./0 | .09 | 7.9 | | |
| T | .30 | <u> </u> | i · | • | | _ | • |
| | .10) | | <u> </u> | | H H H | | |
| | .30 | ·// | .16 | .09 | 7.6 | ⊞ | |
| • • · · · · · · · · · · · · · · · · · · | 2.50 | ./0 | .10 | .10 | 7.6 | · · · · · · · · · · · · · · · · · · · | |
| T >38.1 | | ./0 | /2 | .10 | 25 | <u>ع ، ي</u> | |
| | .12 (4/8 | · | ./2 | • | 7.7 | <u> </u> | // |
| · / / | 1.50 | ./2 | .10 | .20 | 8.0 | · · · · · · · · · · · · · · · · | |
| | 150 | | | 2 | ;; | | • |
| 7 7 | 1.50 | ; ; | <u> </u> | ! | · · | | |
| ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ | 21.00 | ·// | .// | | 7.9 | | |
| 7 7 | 8.50 | .10 | .18 | ,20 | 7.7 | | |
| 18 7 | .60 | ./0 | .10 | 10 | 6.8 | 2./ | a |
| 19 7 | 1.00 71.5 | .10 | Ì | .10_ | 7.9 | · · - | 8 |
| $\begin{array}{c c} & & & & & & & & & & & & & & & & & & &$ | | • .//_ | ,/0 | .07 | 7.7 | <u>. </u> | |
| | .4 | | | i | · : | - | |
| 22_ | .6 | | | | | - | |
| 23.* ~ | .05 | .10 | 105 | .05 | 7.8 | | |
| 2)1 | | | · | | i. | - | |
| | I > 64.6 | | | 10 | 8./ | , 7 | |
| (| | .20 | .20 | ,20 | 81 | /• / · · · · · · | |
| 7 | .5 | 1/0 | /0 | .10 | | | |
| | .5 | | | |) | •• | |
| , * T | 1.0 | ./0 | .10 | .10 | 8.0 | - · · · · - | |
| * Park | Oo, seel | :03 | ce bo. | 3 12- | 21-6 | 8 | |
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| | EFFLU. | SMT DIT | Curi. | | | | | | (mont) | h) | <u> </u> | ean) |
|-----------------|----------|-------------------|-------------------------------|----------|--------------------------------------|-------------|-------------------|-------------------------------|---------|-------------------------------|------------------|--|
| • NATIONAL | (| , | EAST | . | .) | (| • | WES | S T | · |) | |
| . 42-383 ; | <u> </u> | Settled Solids | P ₂ 0 ₅ | | P-0- | | Settled Solids | | | P ₂ 0 ₅ | SO _{l4} | |
| i . | Нф | Vol.% | ppm | GPM | P ₂ O ₅ TPD | рН | Vol.% | P ₂ O ₅ | GPM | TPD | <u>וומדמי</u> | |
| ●)A E: 1 | 8.1 | 1 | _// | 2700 | .2 | 7.3 | 4,0 | 130 | 1450 | 1.1 | 3250 | <u>)</u> |
| 2 | 7.9 | T | 8 | 3500 | _,2 | 6.4 | 3.0 | 405 | 1450 | 3.5 | 4000 | 1/4 |
| 3 | 2.3 | <u></u> | 23 | 3/00 | .4 | 6.6 | 2.5 | 222 | 1300 | 1.7 | 5000 | - |
| 44_ | 7.7 | 17 | 33 | 3700 | .7 | 7.0 | 2.0 | 350 | 1250 | 2.6 | 5000 | fa |
| 5 | 7.9 | T | 25 | 3500 | .5 | 7.7 | .2 | 53 | 1250 | .4 | 8500 | -3 |
| 6_ | 7.7 | T | 30 | 3500 | .6 | 6.9 | ب2_ | 95- | 1170 | .7 | 7500 | - 4. |
| | 7.6 | T | 39 | 3500 | .8 | 4.5 | ,/ | 230 | 1170 | 1.6 | 1125 | J ~ |
| • 8 | 8.0 | 7 | 18 | 2500 | .4 | 5:5- | .6 | 036 | 1170 | 1.6 | 750 | |
| 9 | 7.9 | T | # | 3500 | .4 | 7.4 | .3 | 27 | 1450 | ,2 | 1250 | 8 % |
| 10 | | | 35 | | | | | 127 | | | | N |
| | 7.4 | 1 | . 7 | 2100 | .7 | 6.8 | 1,0 | 7 | 1250 | 1.0 | F75 | 2 |
| 12 | 7.0 | 1 | | 3100 | 2.0 | 7.6 | .5 | 20 | 1450 | .6 | 500 | 4 |
| 13 | 7.7 | 1 | 11 | 3100 | .2 | 6.6 | 3.5 | 1120 | 1300 | 8.7 | 550 | |
| _14 | 7.8 | T | 15 | 3100 | 3 | 6.5 | .30 | 143 | 1350 | 1.2 | 425 | |
| 15 | 7.9 | 1 | 25- | 3100 | .5 | 6.4 | 1.5 | 204 | 1450 | 1.8 | 775 | |
| 16 | 8.1 | 1 | 11 | 3/00 | .2 | 6.7 | 4.5 | 178 | 1450 | 1.6 | 750 | |
| 17 | 8.0 | 7_ | 11. | 3500 | ,٤ | 64 | .3 | -26 | 1300 | .3 | F25- | <u> </u> |
| 18 | 7.0 | 7 | · | 3/00 | | 6./ | .7 | | 1300 | : : | 700 | : : |
| 19 | 7.9 | 7 | 8 | 2100 | .2 | 9.0 | ,3 | 39 | 1170 | .3 | 425 | <u> </u> |
| 20 | t | | #8 | 3100 | ٠,2 | 8.5 | .6 | 35 | 1250 | ٤. | 375 | <u> </u> |
| • <u> </u> | 6.8 | 7 | 127 | 3/00 | 2.4 | 6.4 | 2:0 | 169 | 1170 | 1.2 | 500 | <u> </u> |
| 22 | 3.3 | 11 | 33 C | 3/00 | 6.3 | 2.5 | 6.0 | 215 | 1300 | 1.7 | 1425 | <u></u> |
| 23 | 7.5 | M 1 | i | 1 | | 4.5 | ! | | 1300 | | 600 | ! ! |
| 24 | 7.5 | | L. | 4 | | <i>7.9</i> | I . | 1 | 1 | • | | |
| 25 | 5.7 | #T | 78 | 2700 | 1.1 | 2.0 | 4.0 | 147 | 1350 | 1.2 | 575 | |
| 26 | 7.4 | 五十 | 20 | 2700 | <u>.2</u> | 3.7 | ,40 | 83 | 16.00 | .8 | 725 | |
| 27 | | ; ,: | | - - | <u> </u> | <u> </u> | | | | | • • • • • | <u> </u> |
| • <u> </u> | 7.4 | T | 15 | 2700 | <u>.</u> 2 | 6.7 | | 1 - | 2300 | 1.4 | 750 | |
| 29 | | ļ | | | | 6.8 | | · | 1300 | <u> </u> | 700 | |
| 30 | | | | ļ | | 7.7 | .4 | <u> </u> | 1300 | | 600 | <u> </u> |
| 31 | | | พปลา/ | [81,109] | * | 1 | | 14525/ | 136785/ | * | | |
| <u> १८८८/इस</u> | · · | | 1042/ | /3131 | | | | 181 | 1312 | | | |



| - · | | | Settled | · | | | | Settled | | | <u>.</u> |
|---------------|---------------------------------------|-------|-----------------|-------------------------------|-------------|--------------------------------------|------------|--|----------------------------|---------------------------|--|
| <u>.</u> | Date | | Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ TPD | | Solids Vol.% | P2 ⁰ 5 _ppin | P ₂ (GPMTi | 0 ₅ 20. |
| • | 1 | 7.1 | Gr | 6V | 3100 | 1.1 | 6.4 | 8.0 | 244 | | : : 1 |
| | 2 | 2.4 | | 39 | 3100 | 2 | 3.9 | 4.0 | 530 | _ i | <u>, 3</u> |
| <u></u> | 33 | 7.8 | | | 3100 | | 6.3 | 5.0 | | 1170 | |
| • | 44 | 2.7 | | 33 | 2950 | .6 | 6.4 | 2.0 | 188 | 1170 1 | <u>. </u> |
| | 5 | 7.V | | 65 | 3300 | 7.3 | 6.4 | 3.0 | 178 | 1170 1 | <u>,).</u> |
| · | 6 | 7.3 | | 48 | 2750 | . 8 | 6.7 | 2.0 | 147 | 1450 1 | ٠ کړ . |
| • | 7 | 7.6 | | 28 | 1170 | ٠.٧ | 3.8 | 2.0 | 530 | 1450 4 | 4.b |
| 1 | 8 | 1.3 | | 37 | 3/00 | | 6.3 | 6.6 | 300 | 1100 2 | .0 |
| <u></u> | 9 | 7.7 | | | 2700 | | 6.9 | 2,0 | | 1050 | |
| | 10 | 7.6 | <u> </u> | 39 | 2400 | .6 | 3.7 | 2.0 | 500 | 1450 4 | <u>ı. Ç</u> |
| | 11 | 2.6 | 41 | 25 | 2950 | .1 | 4.1 | ************************************** | 325 | 1300 2 | <u>: 1</u> |
| <u>.</u> | 12 | 1.0 | | 32 | 2400 | ., | 4.3 | . 3 | 260 | 1300 7 | 2,6 |
| • | 13 | 7.6 | <u> </u> | 48 | 3/00 | . 9 | 5.9 | :2 | 270 | 1310 2 | <u></u> |
| • | 14 | 7.8 | | 33 | 3100 | .6 | 6.0 | 4.5 | 370 | 1350 3 | 3. 6 |
| - | 15 | 7.6 | <u> </u> | 33 | 3100 | <u></u> | 3.レ | . 3 | 370 | 1350 3 | 30 |
| <u> </u> | 16 | 7.6 | | 23 | 3100 | .4 | 7.1 | | 18 | 1350 | <u>.)</u> |
| • | 17 | 1.6 | <u> </u> | 46 | 3100 | - | 5.9 | . レ | 350 | 1350 5 | <u> i</u> |
| -(<u> </u> | 18 | 7.6 | <u> </u> | | 2950 | | 3.1 | . ک | | 9241 | |
| | 19 | 8.0 | | | 2950 | | 4.2 | 2.0 | | 1450 | |
| • | 50 | 2.7 | | 17 | 2750 | .3 | 6.6 | .1 | 230 | 1300 | <u>/. i</u> |
| | 21 | 7.9 | | 20 | 2950 | . 4 | 7:1 | 2.2 | 112 | 1250 | <u>·</u> |
| - | 22 | 8.0 | ļ <u>.</u> | | 2700 | .3 | 7.7 | 7.5 | 165 | 1250 1 | <u>.</u> 1 |
| • | _23 | 8.0 | | 18 | 3300 | .4 | 6.7 | 4.0 | 183 | 1300 1 | <u>'. (</u> |
| | 24 | 8.0 | | 11 | 3100 | | 6.7 | 4.5 | 210 | 152D \ | , . , , , , , , , , , , , , , , , , , , |
| | 25 | 8.1 | | 15 | 3100 | 3 | 6.7 | 3.5 | 244 | 1450 2 | <u>Z.</u> , |
| | 26 | 8.0 | | /3 | 7100 | 1 | GCAB | ・レ | 57 | 1450 | المند |
| | 27 | 8.0 | | 18 | 2700 | | 8.0 | | 68 | 1450 | - • ! |
| | 28 | 1.1 | V | 7_ | 2950 | | 8.4 | 27.0 | 70 | 1300 7 | 5.1 |
| | 29 | 8.1 | 50 | 1 25 | 3500 | Ł . | 7.5 | 20.0 | 260 | 1170 1 | |
| | 30 | 7.9 | | 11 | 3100 | ,\bullet | 8.9 1 L | 5.0 | 67 | 980 | ٠.' |
| | · · · · · · · · · · · · · · · · · · · | . ~ . | 1. | ۲, ا |) > | . 1 | , , , | // | 1.5 | 1 (0): | : |

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| t | | ٠. | | • • • • | We s | t |
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|---------------------------------------|----------------|--------------|------|-------------------|-------------------------------|--|---------------------------------|---------------|-------------------|------|-------------|----------|
| | | | | Settled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ . | | Settled Solids | P205 | J. | P205 |
| · · · · · · · · · · · · · · · · · · · | Date | · | рН | Vol.% | ppm | GPM | TPD_ | pH | Vol.5 | _ppm | GPM_ | TPL |
| | 11 | | 7.1 | T | 62 | 3100 | 1,2 | 6.4 | 8.0 | 240 | 1050 | 1,5 |
| : | 2 | | 7.4 | \mathcal{F} | 39 | 3100 | .7 | 39 | 4.0 | 530 | 13 SU | 4,= |
| | 3 | | 7.8 | <i>,</i> - | | 3/00 | | .6.3 | .50 | | 1470 | |
| • <u> </u> | ž _t | | 7.7 | | 33 | 3950 | 16. | 6.4 | 2.0 | 188 | 1170 | 13 |
| : :. , | 5 | | 7.7 | | 65 | 32.5m | /.3 | 6.4 | 30 | 178 | 1170 | 1,2 |
| · | 66 | | 73 | | 48 | 275 | . ,8 | 6.7 | 2.0 | 147 | 1450 | 1,2 |
|) <u> </u> | 7 | | 7.4 | | 28 | 1170 | 1.2 | 3.8 | 2.0 | 530 | 1450 | 4. |
| - | 8 | | 7.3 | 1- | 37 | 3/00 | .07 | 6.3 | 6.6 | 300 | 1100 | 2,0 |
| (| 9 | | 7.1 | 1 | | 2700 | | 6.9 | 2.0 | | 1050 | ļ |
| | 10 | | 7,6 | | 39. | 240) | .6 | 3.7 | 3,0 | 500 | 1450 | 4.4 |
| - <u> </u> | 11 | | 7.6 | 7 | 25 | 2950 | .5 | 4,1 | .2 | 325- | 1300 | 2.5 |
| ` <u>}</u> | 12 | | 7,0 | 7 | 37 | 2400 | .5 | 43 | , 3 | 260 | /300 | 315 |
| | 13 | | 7.6 | T., | 48 | 3/50 | .9 | 59 | ,2 | 270 | 1350 | 3,: |
| | 14 | | 7.6 | T | - | 3/4 | .6 | 6.0 | 4.5 | 370 | 1350 | 3.0 |
| | 15 | | 7.6 | T | 33 | 3000 | .6. | ۍ. ار | | 370 | 1350 | 3, |
| | 16 | | 7.6 | 7 | 23 | 3 | 4 | | | 18 | 1250 | ,2 |
| | 17 | | | <i>-</i> | 42 | 3 | .8 | 59 | ,2 | 350 | 18572 | 2.8 |
| | 18 | | 26 | T. | | 2950 | | 3.5 | ر,٠ | | 1450 | |
| | 19 | | 8.0 | Γ | | 2950 | <u> </u> | 4.7 | 2.0 | | 1450 | <u> </u> |
|) | 20 | | 7.7 | | 17 | 27.50 | ,3 | 6.Z | ./ | 230 | 1200 | 1.8 |
| | 21 | | 7.9 | - i | 20 | 2030 | ,4 | 7.1 | 2.2 | 112 | 1250 | .9 |
| | 22 | | 8,0 | T: | 17 | 2700 | ,3 | 7.7 | 7.5 | 165 | 1050 | 11: |
| | 23 | | 80 | T | 18 | 3300 | .4 | 6.7 | 4,0 | 183 | 1300 | 1.5 |
| _ | 24 | | 8.0. | T |]/ | 3100 | ,2 | 6.7 | 4,5 | 210 | 1250 | 1.5 |
| · ! | 25 | <u> </u> | 8.1 | 1 | 15- | 3/00 | .3 | 6.5 | 3.5 | 246 | 1450 | 2,, |
| | 26 | | 8.0 | 7 | /3 | 3/00 | ,3 | 6.7. | .2 | 57 | 1450 | .5 |
| | 27 | | 8.0 | T | 18 | 2700 | 1.3. | (GRAB) Y.O | 1.6 | 68 | 1450 | 1,6 |
| | 28 | | 8.0 | <u> </u> | 7 | 1950 | 1./ | 8.4 | 27.0 | 70 | 1300 | 1.6 |
| | 29 | | 8.1 | 1 | 25 | 37.00 | .5 | 7.5 | 20.0 | 260 | 1170 | 1.8 |
| | 30 | <u> </u> | 7.9 | ナ | // | 3/00 | T . | 89 | 5.0 | 67 | 980 | 14 |
| | 22 | | 01 | 1— | /ス | 12,00 | じつ | 01 | 111 | 160. | 1,000 | .1 < |

| E, | a | S | t |
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|----------------|----------|--------------|------|-----------------|-------------------------------|---------|---------------------------------|---------------|-------------------|-------------------------------|----------------|-------------------------------|
| | | - | | ettled olids | P ₂ 0 ₅ | | P ₂ 0 ₅ . | | Settled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ |
| | Date | | | vol.% | ppm | GPM | TPD | _pH | Vol. % | _ppm | _GPM | TPD |
| | 1 | | | | | ····· | | | | | · | |
| P | *3 | | 1.3 | 61 | 39 | 3110 | | 6.9 | .11 | 170 | 1350 | 1.4 |
| <u> </u> | *4 | | 1. V | 4 | 3.9 | 3100 | . 7_ | 7.2 | .00 | 98 | 1300 | <i>. j</i> |
| end End | ₩ | | | | | | | | | | | |
| pon Ter | 5 | | 2.1 | .01 | 44 | 2750 | | 6.7 | 61 | 120 | 1450 | 1.1 |
| over | 6 | | 8.0 | 51 | 20 | 2400 | ٤. | 6.7 | ., | 127 | 1600 | 1.1 |
| • . <u> </u> | 7 | | 4.6 | | 35 | 2950 | 6 | 7.2 | ,, | 44 | 1450 | |
| | 8 | | 4.0 | | 89 | 2550 | 1.4 | 7.0 | .01 | 80 | 1600 | |
| <u></u> | 9 | | 7.0 | | 95 | 3/00 | 1.8 | 6.5 | .02 | - 27 | 1450 | <u>-</u> } |
| • — | 10 | | 7.6 | | | 3100 | | 6.6 | .,~ | 188 | 1450 | . 1. t |
| - } | 11 | | 2.3 | <u> </u> | 36 | סמקב | . 6 | 7.5 | 61 | 50 | 1450 | . 5 |
| | 12 | | 7.1 | 4 | 57 | 2500 | . 9 | 6.9 | ان. | 123 | 1500 | 1.1 |
| | 13 | • | 7.3 | | 18 | 2950 | . 3 | 6.5 | .02 | 130 | 1500 | 1. |
| | 111 | | 7.6 | | 17 | 2950 | 3 | 6.6 | .01 | 173 | 1500 | 1.1 |
| | 15 | | 7.3 | | 46 | 2950 | . 3 | 7.4 | .ov | 50 370Fi | 1500 | 3.3 |
| | 16 | | 7.8 | | 20 | 3000 | 4 | 6.0 | . 03. | 550 | 1500 | 5.4 |
| • | 17 | | 3. ? | | 330 | 2700 | 5.4 | 6.0 | .04 | 250 | 1500 | 1.: |
| | 18 | | 3.1 | | 330 | 3/00 | 6.Z | 6.5 | .02 | 170 | 1600 | 1. |
| | 19 | | 3.7 | | 110 | 3/00 | 2.1 | 5.5 | OV | 340 | 1600 | 3. |
| • <u></u> | 20 | | 3.6 | | 108 | 3500 | 2.3 | | - | <u> </u> | | <u> </u> |
| | 21 | · | 3.9 | · . | 60 | 2950 | 1.1 | 7.4 | 61 | | 1600 | 0. |
| - | 22 | | 6.6 | <u> </u> | 42 | 2700 | 2_ | 7.8 | " | 8 | 1450 | |
| | 23. | | 7.5 | 61 | 3 | 2200 | .04 | 7.9 Ammo | -Phos 1 | 20 - Slurr | /300 y Pump | eakir |
| - | 21+ | | 1.7 | | /3 | 2300 | .,٧ | <i>ુ</i> . કુ | 45 | 260 | 1450 | |
| | 25 | <u> </u> | 2.5 | | 7 | COES | . 1 | 6.4 | .02 | 250 | 1350 | 2.1 |
| | 26 | | 7.6 | | 30 | 2002 | | <u>5.v</u> | .02 | 330 | 1450 | ٤.٢ |
| - <u>-</u> | 27 | · | 2.5 | 4 | 18 | 2950 | 3_ | 5.5 | .02 | 420 | 1600 | 4. |
| | 28 | | 6.5 | 0/_ | 108 | 3300 | 2./_ | | | no wate | <u></u> | <u> </u> |
| | 29 | | 1.V | 4. | 57 | 2950 | 1.0 | 7.8 | 4 | 17 | 1300 | |
| - | 30 | | 1.1 | 91 | 1803/ | とうらひ | . 4 | 8.0 | .01 | उउ | 1050 | |
| • | 1 ! | 1 | i | | 1, 1, 1/2021 | 79 /00/ | (| F | i. | | ľ | 1 |

West Settled Settled P205 P205 P205 P205 Solids Solids Vol.% TPD Vol.% Date GPM_ рH GPM TPD ppm pr ppm_ 1 3/00 1.3 ・フ 6.9 1:4 33 7 39 102 1350 170 .00 97 8 4 39 7.2 1300 £ アマ T 2/00 4 6.7 Ť 7.1 4-.o1 ,7 120 5 1750 2750 8.0 6.7 T 1: = ,3 20 1600 T 127 2400 6 7 4.6 7.2 T 42 35 2650 ,6 1-57 4 7 1,4 \Rightarrow 4,0 1 80 7.0 1600 8 89 2550 ,0/ 95 ,2 T 6:9 31<u>00</u> 7.0 1.8 27 1450 9 02 1.5 T 188 145 62 76 7 3/0 10 12 3: 04 270) 50 25 T 7 73 16 11 ,9 1.1 71 57 123 12 T 250 6,9 1500 01 6.5 /, こ 18 3 1500 7. 3 1. 2950 120 ,0i 13 1.6 17. 29.50 .3 173 1500 D $I_{l_{1}}$ T 6.6 .01 7.6 7 46 2950 .8 7.0 1500 50 15 7, 3 07 370 Fitte 3,3 5,0 T ,4. 1500 16 1.8 3000 20 60 <u>550</u> 2.3 T /5°Oð 7.8 17 5-,4 えいつ 33 o 2.700 6.0 04 1.6 3.: 320 1600 T. 18 3/00. .6:2 65 170 :03 2.6 /4 C = 3100 19 ľ ٦./ 390 110 :07 3.6 3500 2.3 108 20 /i/ 7.4 21 T 0.1 3.9 60 2650 42 8 .7 7.8 1450 07 22 2700 دات از 154 <u> 2</u>.9 20 7.5 T /200 23 1450 <u>/</u>3 24 1800 ₹, 860 7,5 1 7.5 25 23011/ 1350 7.0 6.5 02 250 30 5 5.2: 26 \overline{I} 1450 25 03 5.5 **グ2**9 7.5 ,3 18 T 29--27 <u>·0</u>2 1600 23<u>00</u> 21 108 28 :01 7.8 <u> 271</u>25 7,2 T. 57 1300 0 29 1.0 25 33 1050 378.50/11. 1803/... 4687/ 7940/

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| | Settle | d P |

| 42-383 | · | • | | E | a s t | | | | W | est | | : |
|---------------|------|-----------|-----|------------------|-------------------------------|------|---------------------------------|------|--------|-------------------------------|----------|-------------------------------|
| | | • | | ettled Solids | P ₂ 0 ₅ | • | P ₂ 0 ₅ . | | | P ₂ 0 ₅ | | P ₂ 0 ₅ |
| | Date | | Ή | Vol.% | mqq | _GPM | TPD | pH | Vol.%_ | _ppm | _GPM | TPD |
| | 1 | | 7.8 | Sr | /3 | 3000 | ٠.٧ | _5.6 | .01 | 248 | 1250 | |
| | 2 | | 8.0 | 4 | 5 | 2700 | | 5.6 | .01 | 350 | 1300 | 2.7 |
| | _3 | | | . ' | | | <u> </u> | • | | | • . | |
| • | 1, | | 7.8 | Gr | 15 | 2700 | , 3 | 3.3 | 14 | 500 | 1170 | 3. J |
| | 5 | | 7.9 | • | 11 | 3000 | .03 | 4.1 | (V | 260 | 1100 | _/.; |
| | 6 | | 7.8 | | 20 | 2550 | ٠,٧ | 5.7 | .03 | 325 | 1050 | 2. / |
| • • • • • • • | 7 | | 1.2 | | 29 | 3000 | | 4.5 | ٥٧ | 330 | 1170 | |
| | 8 | | 7.1 | <i>"</i> | 57 | 3000 | 1.03 | 5. 9 | .08 | 236 | 1050 | /.] |
| (B.A. | 9 | | 1.6 | • | 8 | 3000 | 、レ | 7.3. | .04 | 80 | 1050 | |
| | 10 | | | | | | · | ٠. | , | | | |
| | 11 | | | | | | | | | | : | |
| | 12 | | 6.7 | Vr | 92 | 3100 | 1.7 | 7.1 | . p 3 | 115 | 920 | (; |
| | 13 | • | 6.9 | n. ; | 62 | 2700 | 1.0 | 7.4 | ・ロレ | 123 | 920 | • |
| | 1,4 | | 7.3 | h | 35 | 2550 | ,,' | 8.7 | .34 | 108 | 1300 | |
| F7 - | 15 | - | 7.3 | •• | 28 | 2950 | 1 | 9.0 | | 230 | 1450 | 1 |
| | 16 | | 7.0 | | 67 | 3/00 | 1. 3 | 6.9 | . الا | 350 | 1300 | 2.7 |
| | 17 | • | | | | | | | | | | |
| | 18 | | | | | | | | | | | ! |
| | 19 | | 1.3 | - 0 - | 20 | 2700 | . 3 | 2.7 | Gr | 250 | 1750 | Z. 1 |
| | 20 | A., II L. | 7.5 | dr | 28 | 2780 | .5 | 36 | Vr | 230 | 1500 | 2. |
| | 21 | | 7.4 | | 53 | 2500 | . 8 | 7.3 | .03 | 180 | 1500 | 1. |
| | 22 | | 1.6 | .,, | 48 | 1900 | . 6 | 7.4 | 3 | 350 | 1450 | 1 . |
| | 23. | | 7.6 | ••• | 46 | 2950 | . 8 | 7.1 | .01 | 350 | 1450 | |
| | 24 | | | | | -/ | | | | | | |
| | 25 | - | 7.5 | Tr | 30 | 2500 | . / | 6.8 | .0V | 180 | 1350 | 1. |
| | 26 | | 1.3 | - " | 48 | 2750 | . 8 | 8.5 | .02 | 25 | i · | |
| | 27 | | 7.3 | " | 15 | 2500 | ,v | 7.8 | .03 | 42 | 1350 | <u></u> |
| | 28 | | 6.8 | .03 | 6V | 2750 | 1.0 | 7.5 | .02 | 57 | 740 | |
| | 29 | | 4.7 | .01 | 155 | 2350 | 2.4 | 6.8 | . 0/ | 83 | 1500 | |
| • | 30 | | 6.9 | Gr | 44 | • | .7 | 6.8 | . 23 | 108 | i. | /: |
| | | | 1 ^ | <i>"</i> | 1. | -/ | , , | 1 4 | ΛI | 77 | ו אינוני | : |

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| · • | | | | Settled | ъ Л | | א ה | | Scitled | PA | | |
|---------------|----------------|-----|-----------------|-----------------|-------------------------------|---|--------------------------|-------|-------------------|-------------------------------|----------|-------------------------------|
| | Date : | | pH | Solids Vol.% | P ₂ O ₅ | GPM | P2 ⁰ 5 TPD | pH | Solids _Vol.ち_ | P ₂ O ₅ | GPM_ | P ₂ O ₅ |
| • | 1 | | 7.8 | T | 12 | 3000 | <u>i</u> | 5.6 | .0/ | 248 | 1250 | 1.9 |
| <u></u> | 2 | 2 | 7. 1 | | 7 | 2700 | 0/ | 5.6 | .01 | 350 | 1300 | 2.1 |
| | 3 | | | | 7 | | | | · | 180 | | |
| • | Ŋ | | 7.8. | - | 15 | 2700 | ,3 | 3.3 | T | 500 | 1170 | 3.5 |
| | | | 19 | 7 | 11 | 3000 | .03 | 4, / | T | 260 | 110 | 1.7 |
| | 6 | | 7.8 | 7 | 20 | °5 2. €.€) | .2 | 5.7 | ,03 | 325 | 1050 | 2.1 |
| | 7 | | 7.3 | T | 27 | 300 | .5 | 4,5 | ,07 | 330 | 1170 | 2,3 |
| | 8 | | 7.1 | 1 | 57 | 3000 | 1.03 | 5.9 | 08 | 236 | 1050 | 1.5 |
| | 9 | ·] | 7.6 | 1 | 8 | 3000 | .2 | 7.3 | ,04 | 80 | 1050 | .5 |
| | 10 | | | | | | | | | | | |
| • · · · . | 11 | | · | | | | | | | | · - | |
| 02° | 12 | | <u> </u> | -, | 92 | 2/20 | 1.7 | 7.1 | 103 | 115 | 920 | .6 |
| | 13 | | 6.9 | T. | 62 | 2707 | 1,0 | 74 | .02 | 123 | 920 | ,7 |
| • | 14 | | 7.3 | 5 | 31- | 2550 | -5. | 8.7 | 134 | 108 | 1300 | 8. |
| | 15 | | 7:3 | T | 28. | 2950 | 1.5 | 9,0 | | 230 | 1450 | 2.0 |
| | <u>1</u> 6 ' | | 7.0 | T | 62 | 3/00 | · // ::- | 6.9 | 1/2. | 2.5 | 13000 | 2 |
| • | 17 | | | | | | | | | | | |
| | 18 | | | | | | | | | - | | |
| | 19 | | 7. i | -0- | 20 | 2707 | .3 | 2.7 | T | 250 | 1750 | ٠,د ا |
| | 20 | | 7.5 | T | 28 | ر ما الماري | ,5 | 3,6 | <i>I</i> | 230 | 1500 | |
| | 5.7 | | 74 | | 2 | 25.3 | ,8 | 7.3 | 103 | 180 | 1500 | 1,0 |
| | 22 | | 7.6 | <i>J</i> . | 48 | 1950 | ,6 | 7,4 | ,3 | 350 | 1450 | 3 |
| | . 23. | | 7.6 | 7 | 46 | 2950 | 1.8 | 7.1 | .01: | 350 | 1450 | 3.1 |
| · · | 2 ¹ | | | | | | | | | | <u> </u> | <u> </u> |
| • • • | 25 | | 7.5 | T | 30 | 2500 | 5 | 6.8. | ,02: | 180. | 1350 | 1,5 |
| | 26 | | 7,3 | . 7 | 48 | 2750 | .8. | 8,500 | ,00 | 25 | 1600 | 3 |
| | 27 | | 7,3 | T | 15 | 2500 | ,2 | 7.8 | 193 | 42 | 1350 | 1.4 |
| | 28 | • ! | 6.8 | 1,03 | 62 | 2750 | 1.0 | 7.5 | 50. | 57 | 760 | 03 |
| | 29 | | 4.7 | ,01 | 125- | 2550 | 2.4 | 6.8 | .01 | 83 | 1500 | 1,8 |
| • <u>;</u> | 30 | | 6.9 | 17 | 44 | 2700 | 07 | 6.8 | .03 | | 1600 | 1, c |
| | 37 | , | 6.0 | 17 | 16 | 3127 | 1,2 | 1.9 | .01 | 70. | 1450 | 1.6 |

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| | | · | • | 5 | Settled Solids | P ₂ 0 ₅ | • | P ₂ 0 ₅ . | | Scttled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ |
|------------|---------------------------------------|-----------------|-------------------|-------|-------------------|-------------------------------|---------|---------------------------------|----------|-------------------|-------------------------------|-------------|-------------------------------|
| | <u> </u> | Date | | | Vol.% | ppm_ | _GPM | TPD | pH | Vol.5 | _ppin | _GPM | TPD. |
| _ | | 1 | | 4.2 | 1r | 83 | 3/00 | 1.5 | 1.0 | <u>0£.</u> | 86 | /300 | |
| - | · · · · · · · · · · · · · · · · · · · | 2 | | 1.3 | · | 3 | 2200 | <u> </u> | 6.4 | 1.70 | 169 | 1600 | |
| _ | - | 3 | | 7.3 | | | 2700 | <u>/</u> | 3.7 | 0V | 340 | 1170 | 2.4 |
| •_ | | 1, | | 1.3 | .01 | _/3 | 2650 | · ン | 7.7 | 15r | | 1300 | <u> </u> |
| | | 5 | | | | - | | | 7.6 | <u>"</u> | 39 | 1450 | ا ق |
| - | | 6 | | | | | | | 6.4 | <u>"-</u> | 170 | 1450 | 1.1 |
| • - | <u> </u> | 7 | · · · · · · · · · | 1.4 | .01 | 17 | 2950 | .3 | 7.レ | .02 | 62 | 1600 | .6 |
| _ | <u> </u> | 8 | | 7.6 | Jr | 7 | 2650 | 1 | 6.6 | .04 | 172 | 1300 | 1.5 |
| : - | <u>(</u> *.3 | 9 | | 2.4 | .01 | 33 | 2950 | <u>. 6</u> | 4.9 | Ur | 268 | 1500 | 2.5 |
| | | 10 | | 2.9 | 47 | 8 | 3000 | .1 | 6.6 | .04 | 98 | 1500 | |
| _ | · · · · · · · · · · · · · · · · · · · | 11 | | 6.7 | Or | 123 | 2700 | 2.0 | 2.6 | _11 | 3150 | 1350 | 25.1 |
| _ | | 12 | | | | | | | 6.5 | . 11 | 135 | 1460 | \ |
| | <u> </u> | 13 | | ÷ | ·i_ | • | | | 7.1 | ,10 | 95 | 1300 | |
| • 🕦 | | 2,4 | | 8.0 | JV | 2 | 2700 | .1 | 7.レ | .12 | 60 | 1450 | |
| : - | -r: | 15 | | 2.9 | Gr | 11 | 2650 | ٠,٧ | 6.5 | .20 | 143 | 1450 | <u></u> |
| | <u> </u> | 16 | | 7.2 | Vr | 51. | 2700 | .8 | 6.3 | .05 | 134 | 1450 | 7.7 |
| • _ |]r: | 17 | | 6.6 | .02 | クレ | 2250 | 1,2 | i _ | .03 | 135 | 1250 | · · |
| _ | مق | 18 | | 6.7 | .ov | -67 | | 1.3 | 7. 0 | .08 | 102 | 1350 | Į. |
| ı <u> </u> | | 19 | | 7. 1 | Tr | 1 | 3/50 | | 7.9 | . 04 | 33 | 1600 | } |
| | | 20 | | • | | | | | 7.3 | .06 | | | |
| | | 21 | | 7.4 | 4 | 17 | 3150 | . 3 | 6.9 | 08 | 160 | 1450 | 1. |
| - | | 22 | | 7.3 | 71 | • 7 | 2700 | | 5.1 | .06 | 1. | 1300 | 1 . |
| | | 23. | | 7.0 | 77 | 46 | 2950 | l' _ | 6.1 | .06 | 1 | 1300 | · . |
| • - | | 24 | | 3.5. | · . | 3760 | 3400 | | 6.1 | .04 | 2150 | 1170 | i |
| | | 25 | | 7.5 | V. | 13 | 2700 | | Z. 0 | .07 | 276 | 1170 | l . |
| | | 26 | | 2.0 | | 44 | 2700 | · · | 2.7 | ,04 | 200 | 1170 | 1 |
| • - | | 27 | | 6.8 | · | 65 | 2700 | , , | 6.6 | , vP | 20 | 1170 | į . |
| _ | (| 28 | · · · · · · | 2.7 | | 18 | 2700 | / | <u> </u> | .16 | 60 | 1100 | |
| | | 29 | | 7. 3 | | | | i . | ŧ | 1 | 305 | | 1 1 |
| • | | | | 1. | | 20 | 2200 | |] | .01 | 1 | 1150 | į |
| | | 30 | · . | 7.4 | | 47 | 2700 | <u>、</u> と | 5.1 | .0/ | 711) | | : |
| | | 1 3 1, 1 | | • / / | ! Ψ ′ | ; 44 X | 1 71.6. | | 0 | , 11/ | 1 7.77 | : , , , , , | |

| ************************************** | Date | | | Settled Solids Vol.4 | P ₂ O ₅ | GFM | P ₂ O ₅ | | Settled Solids Vol.% | P ₂ O ₅ | GPM_ | P ₂ O ₅ |
|---|-------|---------------------------------------|-------------|----------------------------|-------------------------------|-------|-------------------------------|---------------|----------------------------|---------------------------------------|-------------|-------------------------------|
| • [] | 1 | | 1/2 | Tr | <u> </u> | -7119 | 15 | 7,0 | 70 | 76 | 1307 | 1.7 |
| | . 2 | | 73 | !; · | / - | -70% | < .1 | 100 / · | 1.20 | 169 | 1672 | 1.6 |
| : | 3 | | , , | : | | - 7: | 1 | 5.7 | رج) ، | 31/0 | 73.4 | 2, |
| • 5% | Į, | | | , : | / > | 26.0 | 2 | 2. 7 | 1/6 | 7 | 13:10 | K.1 |
| | 5 | | | | | | | 7.6 | | 39 | /(/ | () |
| | 6 | | | | | | | 1 | | 170 | 100 | 1.5 |
| • | 7 | | | ,417 | 17 | 290) | 3 | 7.2 | 12 | 62 | $f(\gamma)$ | 16 |
| | 8 | | 2.6 | | 7 | 2033 | | 6.6 |) \$/ | 172 | 1700 | 1,5 |
| (4.3 | 9 | | -11 | .41 | <u>ا ۋۇ</u> . | 2930 | .6 | <u>17.5) </u> | 1. | بريرسر | 1.3/3 | 2.4 |
| | 10 | | 7.7 | | 8. | | | <u> </u> | | 98 | | <u> </u> |
| • . | 11. | : | 10 / | ; <u>.</u> | 123 | 27. | O | <u> </u> | 1// | 3+50 | 1.35 | 252 |
| | 12 | | | | . — | Wou | 111-5 | | * | 135 | 11150 | 1, 2 |
| (- | 13 | • | | · | | - | | | 1.0 | 35 | 1315 | 1.7 |
| | 14 | | | · .· | 7 | 2.382 | _/_ | 7.2 | 12 | 60 | y'y .\\\\\ | |
| | 15 | | 7. : | | 11 | | 12. | | | 143 | 2723 | 1 |
| | 16 | | | | 51. | | | · · | | 13.1 | | 1 |
| • | 17 | | h . | | ښد ر | · | 12 | | <u>.</u> | /3- | 1200 | 1/_ |
| - | 18 | | 6,7 | 14.75 | _ | 1 | 1.3 | <u> 2. a</u> | | - 2 |] - | 3. |
| | 19 | | 7.5 | 7 | -7 | - | 1,/ | 7.9 | :04 | 33 | 1600 | 1,3 |
| | 20 | : | | | · . | | | 7.3 | .06 | | <u> </u> | <u> </u> |
| | 21 | | 7, 4 | T | 111 | 3/50 | <u>ێڿڔ</u> | 6,9 | 08 | 100 | 1450 | |
| —— | 22 | | 7.3 | T. | | 2700 | ,/ | 5,1 | ,06 | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | 1300 | - [|
| | 23 | · · · · · · · · · · · · · · · · · · · | 7.0 | 7 | 46 | 2950 | .8 | 6,1 | .06. | 215 | 130 | 1.7 |
| | 2l; | | 3.5. | .03 | 3760 | 3400 | 76.7 | 6:1 | 100 | 2/50 | 1170 | 15.1 |
| | 25 . | | 7,5 | ·T | 15 | 2700 | .,3 | 2.0 | .07 | 276. | 1170 | 1,9 |
| | 26 | · | 7.0 | | 44 | 2700 | i | 2.7 | 1.04 | 200 | 1170 | 1, 4 |
| - . | 27 | | 6.8 | T | | 2700 | - | 6.6 | 128 | 20 | 1170 | 1,1 |
| - | 28 | | 7. <i>7</i> | 7 | 18 | 2700 | -3 | <u>3,3</u> | .16 | 60 | 1100 | -; |
| · • · · · · · · · · · · · · · · · · · · | _29 | | 2.3 | 7 | 20 | 2700 | , | 3.5 | .01 | 305 | 1450 | |
| · | 30 | | 7.4 | I | 11 | 2700 | 7 | 5.1 | .01 | 236 | | |
| - . · | হয় - | ! | 7.1 | - | 49 | 2600 | 1.8 | 60 | 1.17. | 1210 | 1170 | 11.5 |

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| i | | 5 | Settled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ | | | P ₂ 0 ₅ | P ₂ 0 ₅ |
|--|------------|------|-------------------|-------------------------------|------|-------------------------------|------|---------------|-------------------------------|-------------------------------|
| | Date | Ho | Vol.% | _ppm | _GPM | TPD | pH_ | <u>vol.</u> % | _ppm | GPMTPD |
| | 1 | | | ; | | | | | | |
| | 2 | 7.4 | Tr | 23 | 2700 | . 4 | 6.7 | 135 | 130 | 1600 1, |
| | 3 | 7.7 | • | 3 | 2700 | ۷.1 | 6.8 | 20. | 178 | 1170 1. |
| • | 4 | 7.0 | .07 | 70 | 2500 | 1.0 | 6.2 | .50 | 376 | 1/70 2, |
| <u> </u> | 5 | 1. 9 | Vr | 8 | 2400 | / | 3,1 | .11 | 188 | 1450 10 |
| | 6 | 7.6 | | 20 | 2700 | .3 | 3.8 | .08 | 221 | 1450 11 |
| • • • | 7 | 7.9 | | 11 | 2950 | . 3 | 5.5 | .04 | 295 | 1600 2,6 |
| | 8 | 1.8 | | 23 | 3/00 | . 4 | 5.5 | 15 | 295 | 1600 2, |
| | 9 | 1.4 | | د3 - | 2950 | .4 | 6.5 | 1.3 | 143 | 1500 11. |
| | 10 | 4.8 | | 15 | 2650 | .2 | 8.8 | 2.8 | /3 | 1600 |
| • · | 11 | 7.8 | | 20 | 2200 | .3 | 9,0 | 8.0 | 23 | 1600 |
| | 12 | 1.8 | | 28 | 2300 | . 4 | 6.5 | 1.3 | 236 | 1500 2, |
| | 13 | 7.6 | | 22 | 2300 | . 4 | 4.4 | .02 | 301 | 1500 Z. |
| • 1 | 1 4 | 7.7 | | 20 | 2550 | . 3 | 4.6 | . 01 | 193 | 1600 1.1 |
| | 15 | 7.5 | | 35 | 2550 | | 7.3 | .02 | 33 | 1600 . |
| ſ | 16 | 7.9 | | 15. | 2650 | 、レ | 7.4 | . 05 | 105 | 1450 |
| ● E ⁿ | 17 | 7.9 | | 20 | 2650 | .3 | 7.4 | .30 | 67 | 1450 . |
| نظر | 18 | 7.9 | | 27 | 2650 | .4 | ر ا | .20 | 151 | 1450 1. |
| | 19 | 7.5 | | 7 | 3000 | | 7.レ | .10 | 151 | 1450 1. |
| ě | 20 | 7.7 | V | 15 | 2400 | レ | 7V | JR | 23 | 1450 .: |
| , | 21 | 8.0 | PR | 20 | 2700 | . } | 5.7 | ,50 | 330 | 1600 3. |
| | 22 | 7.9 | | 23 | 2700 | 4 | 6.9 | . 75 | 151 | 1600 1. |
| i de la companya de l | 23. | 7.8 | | 16 | 2300 |), | 6.9 | .06 | 78 | 1450 |
| • | 24 | 7.6. | · | 17 | 2950 | . 3 | 4.4 | .30 | 530 | 1450 4. |
| | 25 | 7.7 | | 22 | 2950 | | 7.3 | So | 89 | 1450 . |
| | 26 | 7.3 | V | 21 | 2950 | 1 | 7.0 | .// | 13 | 1450 |
| • | 27 | 7.3 | .02 | 50 | 2950 | • | 6.4. | .// | 80 | 1450 |
| | 28 | 4. V | 01 | 75 | 3500 | 1.6 | 7.8 | 50 | 42 | |
| | 29 | 4.0 | 01 | 115 | 3300 | 2.3 | _ | | - | - |
| • | 30 | 39 | (Ir | 102 | 2950 | 1 | 6.6 | .04 | 27 | 1300 |
| - | રા | | ÷ | 684/3n_5 | • | | | <i>-</i> | 14507/161 | 41390/ |

| ÷ | 1 | • | | | | | | | ٠. | · · · · | June | c |
|---|--------------------|---------------|-------|-------------------|-------------------------------|--|--------|---|---------------------------------------|-------------------|---------------------------------------|-------------------------------|
| THE THE | | | | | | | | | • | <i>,</i> | | |
| 42-383 | | | · | · | ast | | | | · | est | | |
| | · | | | Settled Solids | P ₂ 0 ₅ | | P205 . | | Settled Solids | P2 ⁰ 5 | | P ₂ 0 ₅ |
| 1 | Date | | рН | Vol.5 | ppm | GPM | TPD_ | H | Vol.% | _ppmi | GPM_ | TPD |
| | 1 | | | | | | | | · | | | |
| ; - | 2 | | 21 | 7 / | | | . 4 | 6.2 | | , | 1/1/1/ | 1,2 |
| <u> </u> | 3 | | 22 | 11 6 | | 2789 | <,/ | <u>'E</u> | | | ***1,.7 | 12 |
| • | 14 | | 7.0 | | | 1. 2.4.3 | /.0 | , . | | | 172 | |
| | 5 | | 7.9 | 7 | | - :/-: | , /. | <u> </u> | . j 1 | | 14/2 | 4 |
| | 6 | | To la | | 2.7 | - 1, 1 | . , 3 | | , (, | | 27/3 | 1 |
| • | 7 | | 7.9 | , | | (زېد. | , 3 | | | | | 2, |
| | 8 | | 78 | | <u>زیست</u> | 310) | | | 15 | | . : | 2,6 |
| <u>(</u>) | 9 | | 24 | | | 7. s () | uf. | | 1.3 | | | 1.3 |
| | 10 | | 7.8 | | - | | , | <u> </u> | , j. | | | |
| • · · · · · · · · · · · · · · · · · · · | 11 . | | | \ | 0 | | ,,, | | | 23 | | 12 |
| | 12 | | 75 | Tre | خ : ٠ | 2500 | 4 | | | 23% | | 12/ |
| <u></u> | 13 | | 26 | 11 | | 3300 | 4 | J.V | 1-1- | 3 | 1 500 | 2. |
| | 14 | | 1 | 11 | | 2370 | .3 | 46 | 0/ | 1,3 | 1600 | 10 |
| | 15 | : | 7,5 | ά | 35 | 2770 | | 2.3 | .02 | | 1600 | تيا |
| | 16 | | 7.9 | i į: | 1/3 | 2650 | ,2 | 7.4 | 1,05. | 105 | 1450 | 1.2 |
| • | 17 | | 2.9 | h | 20. | 1632 | .3 | <u> 7.4</u> · | 30 | 67 | 1410 | .6 |
| | 18 | • | 7.9 | 'ì | 27 | 2540. | 4 | 6.5 | . , 20 | 131 | 11150 | 1.3 |
| | 19 | | 9.5 | | 2 | 3.44 | | | 1, 1,1 | 131 | 11129 | 1/3 |
| • | 20 | | | | 15. | 1. 1. 9 | | | 17 | - 3 | 140 | |
| | 21 | | 8.0 | 1 | .:) | 2297 | 3 | 5.7 | 187 | | 7115 | 3: |
| | 22 | • | 79 | | - |) 1 ay | (/ | 6 | | | | 17 |
| | 23 | · | 38 | | | <u> </u> | , 2 | 10.3 | | | 11/1/2 | 1 |
| | . 5 _j t | | 56. | | | | | | | | , , , , , , , , , , , , , , , , , , , | <u> </u> |
| | 25 | , | 77 | • / | - 7 | | . ,5 | 17.31 | ٠. زن. | | !1 | |
| | 26 | | 5/3 | | | | 4 | <u> 9. 9 </u> | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | - ~ | 11 | <u></u> |
| • • | 27 | | > 3 | .0レ | 50 | | , 9 | 6.4. | 11 |) | , , | 1.7 |
| | 28 | | 1/2 | .01 | 75 | 350) | 1.6 | 7.8 | (3) | (1) | 11/50 | 1. 1 |
| | 29 | · · · · · · · | 40 | 01 | 115 | : کارون کارون ک | 5:3 | * | | | | - |
| • ; | 30 | | 39 | Tr | 102 | 2450 | 1.8 | 6.6 | , 04 | 1,00 | 1300 | ð |
| | эт. Д. | | | | 7 | | İ | ! | 17 | 1/1 | 11160 | 1. |
| | | | | | | | | | - | | | |

42-191

East

| | | ÷ | S | Settled | | | | | Settled_ | | | | |
|-------------|----------------|---|------|-----------------|-------------------------------|----------|-------------------------------|----------|----------------|-------------------------------|---------|-------------------------------|--|
| , , | Date · | | ٤ | Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | | Solids | P ₂ O ₅ | _GPi⁄i∙ | P ₂ 0 ₅ | |
| • | 1 | | 7. 7 | VOI. 5 | ppm. | 2200 | <u>1.F.D</u> / | 5,2 | 40 <u>1.04</u> | _ppm350 | 1600 | _ | |
| <u>`</u> | 2 | . | 7.8 | JR. | 10 | 2150 | | 7,0 | .08 | 80 | 1850 | , | |
| | 3 | | | ٧٨. | , | <u> </u> | | . 3.7 | .10 | <u> </u> | 1600 | 2. | |
| | l _i | | | a a | | | | 6.8 | .40 | 110 | 1600 | | |
| | 5 | | 7.2 | √R. | .15 | 2150 | ,2 | 6,1 | ,20 | 183 | | | |
| | 6 | | 7.8 | TR. | | 7.200 | | 6.4 | .30 | 123 | | | |
| | 7 | j | 7.9 | Vn. | 7 | 2200 | . / | 6.7 | 7,60 | 376 | | | |
| | 8 | | 7.8 | TP. | 7 | 2050 | | 4.1 | .02 | 376 | | | |
| (1) | 9 | | 8.0 | VE. | В | 2050 | . / | 3.7 | .03 | 460 | | İ | |
| | 10 | | 7.7 | VE. | /3 | 2550 | , 7 | 5,2 | .06 | 280 | 1500 | 1 | |
| | 11 | | 8.1 | TE. | 8 | 2550 | | 6.4 | .07 | 115 | 1750 | 1 | |
| 7 | 12 | | 7.8 | Ve. | 3/ | 2650 | ,6 | 6.7 | , 10 | 83 | 1600 | | |
| | 13 | | 7.8 | Vr. | 35 | 2400 | . , | 3:4 | iov | 930 | 1450 | 8. | |
| | 14 | | 7.6 | | 15 | 2400 | , b | 4.2 | .01 | 720 | 1500 | 6, | |
| _t 3 | 15 | | 7.5 | | 23 | 2200 | , 3 | 5.1 | 3.0 | 650 | 1600 | 6. | |
| | 16 | | 7.9 | | 3. | 2150 | | 4.0 | ,01 | 350 | 1500 | 3, | |
| • • | 17 | | 500 | <u> </u> | 50 | 3100 | . 9 | 6.6 | .02 | 110 | 1450 | 1. | |
| | 18 | | 3.8 | | 139 | 2950 | 2,5 | | | | | | |
| | 19 | | 5.8 | | 37 | 2400 | | 7.8 | . ,07 | 46 | 1600 | | |
| 8 3. | 20 | | 7,6 | | 8. | 2300 | | 4,3 | .01 | 480 | 1750 | عك | |
| | 21 | | 7.9 | * | 25 | 2500 | .4 | 6:2 | 2/ | 670 | 1450 | <u>.</u> | |
| | 22 | | 7.2 | VR | 17 | 2500 | .2 | 4.0 | .14 | 950 | 1450 | 8. | |
| | 23. | | 8.0 | | 9 | 2500 | | 3.7 | .):(| 130 | 1450 | 4. | |
| | 24 | | 8.0 | 4 | 3 | 3300 | <u> </u> | 7.2 | .02 | 80 | 1600 | 2 . | |
| | 25 | | | | - | | | | | | | <u> </u> | |
| | 26 | | 1.4 | TR | 15 | 2400 | ٦, ک | 7,2 | 115 | 95 | 1450 | | |
| - <u> </u> | 27 | | 8.1 | // | 13 | 2400 | $-\nu$ | <u> </u> | ,60 | 0 کک | 1170 | 13. | |
| | 28 | | 8.1 | | | 2550 | | 6.2 | .40 | 252 | 1600 | <u>Z</u> . | |
| | 29 | | · | • | | | | | | <u> </u> | | | |
| | 30 | | 7.9 | Vr | 15 | 2950 | 3 | 1 | . 10 | | 1 | 1 | |
| <u> </u> | 27 | | つり | 1, | 31 | 7 | , | ₹ / | ! ./ | 10. | ill. | 1 | |

East West Settled 1 Settled 2 1113 Solids Solids Vol.% GPM TPD Vol.% _ppm_ GPM_ TPD Date _ppm pii 34 350 1 <u>, 9</u> <u>j_</u>: 10 ું છે 2 3 l, 4/5 5 6 7 8 9 10 11 12 y. 93.7 13 ٠, 14 15 l 16 330 50 17 f(z)17 18 37 1/2 19 1.3 20 73.5 21 22 23 24 25 26 2. 27 2.7 ≥ 5.2 28 29

West East Settled Solids P205 Settled Solids P205 P205 .

| | | | Settled | P ₂ O ₅ | | P ₂ 0 ₅ | | Settled | P ₂ 0 ₅ | | P ₂ 0 ₅ |
|---|------|------|-----------------|-------------------------------|-------|-------------------------------|------------|-----------------|-------------------------------|-------|-------------------------------|
| | Date | рΉ | Solids Vol.% | ppm, | _GPM | -2°5 · TPD | Hq | Solids Vol.% | _ppm, | GPM | -2-5 _TPD_ |
| • | 1 | 8.0~ | Tr. | 3 | 2700 | ٠./ | 6.5 | .21 | 143 | 1900 | 1.6 |
| · · · · · · · · · · · · · · · · · · · | 2 | 8.0 | | 15 | 2300 | 2 | 7.0 | .15 | _188 | 1750 | 20 |
| <u> </u> | 3 | 7.9- | · . | <u> /J</u> | 2300 | | 6.6 | 15 | 139 | 1750 | 1.1 |
| • | lı · | 8.0 | | _/3_ | 2700 | <u>٠</u> | 4.3 | .02 | 376 | 1600 | 3.6 |
| | 5 | 7.2 | | 18 | 2550 | .3 | 3.2 | 25 | 830 | 1600 | 8. |
| | 6 | 7.9 | | 20 | 2550 | . 3 | 6.5 | 45 | 220 | 1600 | 2.66 |
| • | 7 | 7.5 | | 7 | 2700 | . / | 6.4 | ./ʃ | 147 | 1750 | 1.1 |
| | 8 | 7.8 | | | 2400 | . 2 | 6.8 | .35 | 120 | 1750 | /•= |
| (*** | 9 | 8.1 | | 4_ | 1900 | 4.1 | 5.4 | .25 | 390 | 1600 | 3.7 |
| | 10 | 7.6 | | 28 | 2050 | . 3 | 6.3 | 1.6 | 252 | 1750 | 9,6 |
| | 11 | 7.9 | · · · | 15 | 1450 | . / | <u>5.3</u> | .55 | 130 | 1750 | ي ك |
| | 12 | 8.3 | | | 2050 | . / | 6.6 | ,40 | 200 | 1.600 | 1.6 |
| | 13 | | · . | • | | | 7.1 | .20 | 150 | 1600 | 1.5 |
| | 14 | 8.0 | | | 1.900 | <.1 | 7.4 | .80 | 60 | 1750 | .6 |
| | 15 | 8.0 | <u> </u> | 14 | 2050 | · . Z | 9.7 | 3.5 | 360 | 1250 | 3.5 |
| <u>.</u> | 16 | 8.1 | | 1 | 1900 | <./ | 6.2 | 15. | 112 | 1250 | 1. |
| • _ * _ | 17 | 6.1 | | 55 | 2400 | .9 | 1.2 | .30 | 72 | 1900 | |
| منظم ـــــــــــــــــــــــــــــــــــ | 18 | 4.0 | | -210 | 1600 | 20 | 6.2 | .03 | 21 | 1600 | <u> </u> |
| | 19 | 7.9 | | /3 | 2550 | .2 | 3.9 | .02 | 460 | 1450 | 4.0 |
| | 20 | 2.1 | | 35 | 2550 | کـــــا | 4.1 | 01 | 280 | 1600 | 2. |
| | 21 | 7.3 | | 17 | 1750 | .2 | 4.0 | er | 390 | 1750 | 4.1 |
| | 22 | 7.9 | | 17 | 2500 | . 3 | 4.7 | .08 | 376 | 1500 | 3.5 |
| | 23 | 7.8 | | 11 | 2/50 | . 1 | 4.3 | .02 | 750 | 2:50 | 9. |
| | 24 | 7.8 | | 17 | 2150 | .2 | 4.5 | .02 | 405 | 1500 | 3. |
| | 25 | 7.5 | | 25 | 2300 | .4 | 6.0 | •// | 270 | 1500 | 2.1 |
| | 26 | | | | · | | 6.4 | 27. | 280 | 1600 | 2 |
| • <u> </u> | 27 | | · . | · | | | 6.1 | .17 | 300 | 1600 | 2, |
| | 28 | 7.9 | | | 2300 | 2 | 5.5 | ./0 | 440 | 1600 | 4: |
| - , | 29 | 7.2 | | 3 | 2050 | 4.1 | 5.9 | OZ | 178 | 1750 | 1. |
| • <u> </u> | 30 | 7.7 | <u> </u> | · // | 7300 | . 2 | 5,9 | .02 | | | |
| • | 31. | | 1 - | ز | 1-1 | n. > | 15 | 21 | 200 | 17.20 | 13 6 |

East

| | | | | | | | | | · · · · · · · · · · · · · · · · · · · | · | | |
|---------------------------------------|--------------|----------|-----|------------------|-------------------------------|---------|-------------------------------|-------------|---------------------------------------|-------------------------------|------|---------------|
| | | | | ettled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ | | Settled Solids | P ₂ 0 ₅ | | P205 |
| <u> </u> | Date | | | Vol.% | ppm | GPM | TPD | рН | Vol.% | _ppm | GPM_ | TPD. |
| • R | 1 | | 7.3 | | 13 | 2700 | · . 2 | 5.2 | - | 520 | 1450 | 5.0 |
| - | 2 | ļ | 7.8 | | 23 | 2550 | ,4 | 3.2 | | 170 | 1450 | _ 1. 5 |
| | 3 | | 7.6 | .01 | 37 | 2300 | 5 | 7.1 | .02 | 75 | 1500 | 7 |
| • | 4 | | 8.1 | Tr. | 7 | 2300 | .1 | 3.5 | .13 | 570 | 1500 | <u>5.1</u> |
| b | 5 | | 7.2 | Tr. | 27 | 2150 | 3 | _7.5_ | 31 | 118 | 1500 | _1.1 |
| | 6 | | 7.4 | | 30 | 2650 | •5 | 4.3 | .06 | 500 | 1450 | 4.3 |
| • | 77 | | 6.8 | | 50 | 2400 | 7_ | 6.8 | .05 | 230 | 1600 | 2.2 |
| _ | 8 | | 4.1 | | 135 | 2400 | 1.9 | 5.8 | .01 | 180 | 1450 | 1.6 |
| | 9 | | 7.9 | | 7 | 2550 | .1 | 3.6 | .45 | 336 | 1450 | 2.9 |
| v- | 1.0 | | 8.0 | | 3 | 2550 | < .1 | 3.3_ | .02 | 600 | 1450 | 5.2 |
| | 11 | ļ . | 8.0 | | 8 | 2500_ | 11_ | 6.0:_ | 35 | 275 | 1600 | 2.É |
| _ | 12 | | 8.0 | | <u>11</u> | 2500 | .2 | 3.0 | .02 | 860 | 1100 | 5.7 |
| | <u> 13</u> | | 7.8 | | 18 | 2500 | 2 | <u>4.8</u> | .10 | 500 | 1170 | 3.5 |
| | 1,4 | | 7.9 | | 13_ | 2400 | .2 | 3.3 | .01 | 560 | 1170 | 3.5 |
| _ | 15 | _ | 8.2 | | | 2550 | 2 | _ | - | | - | - |
| | 16 | <u> </u> | 3.8 | | 108 | 2550 | 1.6 | | <u>-</u> . | | _ | |
| | 17 | <u> </u> | 7.6 | | 13 | 2650 | .2 | 6.7 | .07 | 460 | 1350 | 3.5 |
| -C | 18 | ļ | 6.4 | | 50 | 3000 | 9 | 3.7 | .01 | 155 | 1450 | 1.1 |
| | 19 | | 4.2 | <u> </u> | 102 | 2650 | 1.6 | 3.2 | .01 | 700 | 1450 | 6. |
| P | 20 | | 7.7 | - | 18 | 2200 | .2 | 7.5 | .11 | . 27 | 1500 | |
| | 51 | | 7.8 | | 13 | 2700 | 2_ | 6.7 | | 173 | 1450 | 1.5 |
| | 22 | <u> </u> | 7.5 | | 28 | 2550 | 4 | 6.2 | .20 | 188 | 1650 | 1.9 |
| | 23 | ! | 7.9 | | 46 | 5,100 | 7_ | 7.3 | .70 | 180 | 1900 | 2.0 |
| - | 2 <u>l</u> + | | 7.9 | | 17 | 2700 | 3_ | 2.3 | .11 | 140 | 1750 | 1.: |
| . <u>.</u> | 25 | <u> </u> | 7.7 | | 27 | 2500 | 4 | 5.8 | .20 | 252 | 1600 | 2. |
| · · · · · · · · · · · · · · · · · · · | 26 | | 7.9 | | 17 | 2500 | .3 | 3.2 | .01 | 336 | 1450 | 2.9 |
| . | 27 | | 8.1 | | 5 | 2500 | .1 | 7.1 | .20 | 39 | 1450 | <u> </u> |
| | 28 | | 8.2 | | 15 | 2400 | .2 | 7.8 | .01 | 65 | 1450 | |
| . — | 29 | | 8.2 | | 8 | 2550 | 1.1 | 6.5 | .36 | 330 | 1600 | 3. |
| <u> </u> | 30 | | 8.1 | | 8 | 2550 | .1 | 6.9 | .11 | . 80 | 1450 | |
| - | ไรา | İ | 0 7 | 47 | כר |) slino | 2 | 6.9 | . 30 | 204 | 1850 | 2. |

| | | • | | | | | • | | XX | meh | |
|---|----------------|---|-----------------|-------------------------------|-------------|--------------------------------------|---------------------------------------|----------------------------|-------------------------------|----------------------|---------------------------------------|
| 取扱可量エスター・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・ | | . : | | | | | | | • | | |
| 42-383 | | | E | ast | • | | | | est | | |
| | | | Settled | pΛ | | P. O . | · · · · | Settled | P_O_ | | P ₀ O ₌ |
| | Date · | рН | Solids Vol.% | P ₂ O ₅ | GPM | P ₂ 0 ₅ TPD | Ho | Settled Solids Vol.% | P ₂ O ₅ | GPM_ | P ₂ O ₅ _TPD |
| | 1 | 7.3 | | 13 | 2700 | ; 2 | 52 | | L. | 1 | (-0 |
| · · · | . 2 | 1,2 | | <i>23</i> | : 3.50 | /، د | | | 125 | | 1.5 |
| | 3 | | | 37 | | | 7.1 | 19.30 | 7, | (4) | . 7 |
| • ,; | l _i | | | 7 | | / | | | 570 | 4.)) | 5/ |
| | 5 | 7 2 | | 27 | | 3 | | | 112 | | //./ |
| | 6 | 4 | | 30 | | | | | (U) | /(- | 4,3 |
| • | 7 | 6.7 | | 7 3 | | 7 | | | , , , , , , | • | 2. L |
| 6 | 8 | | | 135 | | 1,9 | 5 | | / | _ · _ · · | 1.6 |
| <u></u> | 9 | 1 1 : | | 75-1 | | , / | | | | | 2.2 |
| | 10 | | | ? | | 5.1 | | | | | 5 |
| •-(| ii | | | | | 1 | | | . - | | 2.4 |
| <u>.e</u> | 12 | | | | · · - | 2 | | · · · · · · · | 40 | | |
| | 13 | | | 10 | | ik | | | () | / | 5 |
| | 24 | | | 15 | | 2 | ` | • | <i>[-1</i>] | | |
| r - | 15 | | | 1: | · · · · · · | 2. | | | | | |
| | 16 | , | | 11)6 | | 1.6 | | | | | |
| • p | 17 | | | 13. | | 1- | 1/ | | : | | |
| مم | 18 | | - | | | . 9 | 1 | .) | | | 1.6 |
| | 19 | | +i | | | 1.6 | | 0 | 7 | | 6.1 |
| | 20 | 7 " | | | 20 | 2 | / | .// | 2.39 | | 1.2 |
| | 21 | | | 1.13 | | 1.1 | , , , , , , , , , , , , , , , , , , , | | 17/3 | | 1/,5 |
| | 22 | | | <u>:</u> • ;; | | | | | | | 1/1 |
| | 23. | | | 46 | | | | | 7-1 | | 12. |
| | 2 <u>l</u> t | 7.6 | 业 | 17 | | , | b | | 140 | | 1.3 |
| | 25 | 1. | | 29 | | . / | | |)))) | 11 /1 | <u> - /</u> |
| | 26 | 7.7 | | 17 | - 3 / | <u> </u> | 3.2- | /]- | | 1 15 | 2.9 |
| - <u>[</u> | 27 | 81 | | 1 | | | 2. | 1215 | | | 1,3 |
| | 28 | (L | | 1 | | , 2 | 27 | | | 7: | 6 |
| 5 | 29 | 82 | | | 12. | 1.1 | 2 | برخ تحد | | <u> </u> | 3.2 |
| | 30 | 81 | | | 5 | 1 | 1 | | / | 777 | 1 |
| | 21 | 12.4 | 1 - 1 | 1 128 | 2500 | 1.4 | 5,5 | 1./5 | 13.76 | 1979 | 12.4 |

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| | · | • | | | | | | | · | | | |
|---|--------------|----------|------|-------------------|-------------------------------|--------|-------------------------------|--------------|-------------------|-------------------------------|-------------|-------------------------------|
| | | | | Settled Solids | P ₂ 0 ₅ | _ | P ₂ 0 ₅ | | Settled Solids | P ₂ O ₅ | | P ₂ 0 ₅ |
| | Date | · | рН | Vol.% | ppm | GPM | TPD | _pk | Vol. % | ppm | GPM | TPD |
| | 1 | | 3.4 | Tr. | 160 | 1900 | · 1.8 | 6.3 | •75 | 350 | 1600 | 3.4 |
| - | 2 | | 7.4 | Tr. | 65 | 2550 | 1.0 | 7.0 | .50 | 127 | 1750 | 1.3 |
| | 3 | | 7.0 | Tr. | 55_ | 2050 | 7 | 7.0 | -53 | _155 | 1600 | 1.5 |
| | 1, | | 7.1 | Tr. | 55 | 2650 | •9 | 7.8 | .11 | 110 | 1600 | 1.1 |
| | 5 | | 7.1 | -04 | 50_ | 2300 | 7 | 6.6 | 50 | 302 | 1600 | 2.9 |
| | 66 | | 7.3 | Tr. | 42 | 2300 | .6 | 6.6 | .75 | 325 | 1600 | 3.1 |
| • | | | 7.5 | Tr. | 33 | 2200 | .4 | 6.0 | .80 | 405 | 1750 | 4.2 |
| | 8 | <u> </u> | 7.5 | Tr. | 30 | 2400 | .4 | 3.7 | .10 | 500 | 1750 | 5.2 |
| <u>(</u> | 9 | | 3.8 | | 115 | 2700 | 1.9 | 7.3 | 1.0 | 139 | 1750 | 1.5 |
| •- | 10 | | 3.2 | | 150 | 2550 | 2.3 | 7.2 | .16 | 130 | 1450 | 1.1 |
| | 11 | | 6.8 | | 11 | 2150 | 1 | 7.8 | .16 | 38 | 1600 | 4 |
| · • • • • • • • • • • • • • • • • • • • | 12 | | 4.0- | | 89 | 2650 | 1.4 | 7.4 | .16 | 104 | 1500 | .9 |
| <u> </u> | 13 | <u> </u> | 7-5 | | 15 | 2400 | 2 | 6.9 | 68 ¹ | 222 | 1600 | _2.1 |
| | 3.4 | | 7.8 | | 28 | 2200 | | _6.1_ | 42 | 362 | 1350 | 2.9 |
| _{ | 15 | | 7.5 | | 25 | 2200 | -3 | 5.6 | .63 | 650 | 1450 | _5.7 |
| | 16 | | 7.9 | | 30 | 2700 | •5 | 5.8 | •75 | 151 | 1300 | 1.2 |
| • | 17 | | 7.7 | | 11 | 2550 | .2 | 6.4 | .20 | :67 | 1750 | .7 |
| | 18 | | 7.8 | | - 10 | 1950 | .1 | 6.9 | .40 | 155 | 1450 | 1.4 |
| | 19 | | 8.0 | | 20 | 2150 | 33 | _5.5_ | .03 | 362 | 1750 | 3.8 |
| • | 20 | | 7.9 | | 30 | 2050 | .4 | 2.8 | .07 | 1050 | 1500 | 9.4 |
| | 21 | | 8.1 | | 28_ | _2200_ | .4_ | 3.5 | .09 | 1440 | 1500 | 3.9 |
| | 22 | | 8.2 | | 15 | 2150 | .2 | 6.6 | .24 | 350 | 1850 | 3.9 |
| | 23 | | 7.7 | | 35 | 2700 | .6 | | | 570 | 1600 | 5.4 |
| · | 2 <u>/</u> ; | | 7.8 | | 35 | 2550 | 5 | | <u> </u> | 155 | 1600 | 1.5 |
| | 25 | | 7.6 | | 30 | 2300 | 4 | 6.1 | .30 | 460 | 1450 | 4.C |
| | 26 | | 6.6 | | 46 | 2400 | .7_ | 4.0 | .02 | 460 | 1500 | 4.] |
| - <u> </u> | 27 | | 7.5 | | 27 | 2400 | .4 | 3.4 | .01 | 620 | 1500 | 5.€ |
| - | 28 | | 7.4 | | 37. | 2200 | .5_ | 6.0 | .08 | 130 | 1500 | 1.2 |
| | 29 | | 7.6 | \ \ | 27 | 2650 | .4 | 4.0 | .05 | 470 | 1050 | 3.0 |
| P | 30 | | | | | | | - | | | 1/1000 | <u> </u> |
| - | 27. | 1 | | | 1304/45 | K8150/ | ļ | | | 9359/200 | 145250/ | .! |

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East

| • 42-353 | | | | Scttled | | | | | Settled | | | |
|--------------|------|----------|---------------------------------------|-----------------|-------------------------------|-------------|-------------------------------|----------|-----------------|-------------------------------|--------------|-------------------------------|
| | Date | | pH_ | Solids Vol.% | P ₂ O ₅ | _GFM | P ₂ O ₅ | Hq | Solids Vol.% | P ₂ O ₅ | GPM | P ₂ 0 ₅ |
| | 1 | 7/ | 211 | 70 | 160 | 15. | 1 | | | 31 13 | | |
| | 2 | | | <u> </u> | (0.5 | | 1.0 | | | | | <u></u> |
| | 3 | | 5.0 | 10 | L . | 29. | | | | | · . | |
| • | 24 | | | Y | 3 . | | | | | | | |
| | | | 27 | 04 | | | .7 | 6.6 | | | | 22 |
| | 6 | | 7.3 | 70 | 116 | | 6 | 7 | | | : | = / |
| • | 7 | | 1.5 | | | | , (/ | <u>(</u> | | 2 . ** | 1 | 4,2 |
| | 8 | | -/- | | 3 | | / | | , , | | | ا نے برت |
| (13) | 9 | | | | 11 | | 1.7 | | 1. | , j | | 15 |
| | 10 | | | ļ | 157 | | | | 1. /. | <u> </u> | | 1.1 |
| — 6.3 . | 11 | <u> </u> | | ļ | | | | | | | | 1,4 |
| | 12 | - | ; | | | <u>.</u> | 1,0 | | | | | <u> </u> |
| <u></u> | 13 | | | | | | | | | <u>.</u> | | |
| | 14 | | | | | | 1 | 6. | | | | 1-1 |
| [| 15 | | , | | | | , 3. | <u>`</u> | | | | 15_ |
| <u></u> | 16 | | <u> </u> | | <u>; ()</u> | | | | | 1 / | - | 1/,2 |
| • | 17 | <u> </u> | | | | | | ., ., | - | | | 1.7 |
| | 18 | | | · . | 10. | | , / | | | · | <u> </u> | 1.1 |
| | 19 | | . : | | | | - | | <u> </u> | 162 | ļ | 3.7 |
| • | 20 | | ļ | 1: | | (j.) . | , 4 | | | - | ļ | 174 |
| | 21 | | · · · · · · · · · · · · · · · · · · · | | 22 | | ./ | · . | <u> </u> | (7:7:) | | 1-1- |
| | 22 | | | | 12 | | - , - | · | | <u> </u> | | 39 |
| | 23 | - | | | - | 7 | | | <u>:</u> | | <u>.</u> | 15.4 |
| | 54 | | | | 32 | | , | | | /: | <u> </u> | 1/13- |
| · U . | .25 | <u> </u> | | | 30 | 1 | / | | <u> </u> | (1) | | 14 |
| | 26 | | | | <u> </u> | <u> </u> | | | <u> </u> | / | <u> </u> | 14/ |
| _ = | 27 | | | ļ | 27 | 1- | 11/ | | | 1027 | <u> </u> | |
| | 28 | | <u> </u> | <u> </u> | 37 | | 1.5_ | <u></u> | <u> </u> | 131 | | 1/1= |
| | 29 | ļ | <u> </u> | <u> </u> | 127 | | L/- | (/ | | 1.470 | | 132 |
| • | 30 | | 7.0 | 71 | 45 | \$2.00 | 1,6 | 5.7. | 1,55 | | 1/5/50 | <u> </u> |
| | 31. | ! | ; | | 1 | } | 1 . | ţ | ; | ; | ļ : | į |

| 42-383 | | | E | ast | · | | | ī | lest | | , ll.; |
|---------------|------|------|----------------------------|----------|-------------|-------------------------------|-------------|----------------------------|-------|----------|-------------------------------|
| | Date | | Settled Solids Vol.% | P205 | GPM | P ₂ O ₅ | | Settled Solids Vol.% | PD 3 | S GPM | P ₂ O ₅ |
| | 1 | 7,20 | T | | 250C | | 6.70 | 4.0 | | 1750 | 122 |
| | 2 | | | | | | | | | | |
| : <u>:</u> | 3 | 7.50 | T | | 2200 | | .6.50 | 5.5 | | 1450 | 162 |
| f | 14 | 2.0 | 3.5 | <u> </u> | 2200 | | 6.1 | 11.0 | | 1600 | 167 |
| | 5 | 3.3 | <u> </u> | V | 2150 | | 5.8 | දු. 0 | | 350 | /875 |
| (| 6 | 7. 4 | 7 | 22.1 | ,70 EQ | | 6.6 | 8.0 | | 7450 | ROSC |
| | 7 | 7.2 | 7 | , | .2050 | | 5 .5 | 3.0 | 64.9 | 1450 | 210 |
| | 8 | | | | | | | | | | |
| | 9 | | | | | | | | | | |
| | 10 | 3.5 | | | 2050 | | 6.5 | e,c - | | 1650 | 1550 |
| <u> </u> | 11 | 2.8 | . 35 | | 2050 | | 7.2 | 4.0 | ` | 1350 | 2500 |
| ŧ | 12 | 7.6 | 7 | 7/69.0 | 2200 | | 5.6 | 3.0 | | ωS | 22,50 |
| فنا | 13 | 7.8 | | | 2550 | | 2.9 | 1.0 | 161.4 | 1600 | 1:-5: |
| | 14 | 6.8 | - | | 2356. | | 6.6 | 8.0 | | //sc. | |
| U | 15 | _ | | | | · 5. | 2.8 | 1.5 | | 2050 | 1400 |
| | 16 | | | | · · | | 2.5 | ٧. | | 1900 | 150 |
| | 17 | 7.1 | 7 | | 2550 | | 6.6 | 5.0 | | 165 C | 105 |
| | 18 | 7.7 | T. | | 3650 | | 5,4 | 7 . 0 | | 16 So | /240 |
| | 19 | 7.8 | 7 | | 265 C | | 5,3 | 4.5 | 1 | 1750 | 40.00 |
| | 20 | 8.C | | 8.831 | 2650 | | 645 | 3.5 | | 1600 | 195 |
| 5 7: | 21 | 7.8 | T | | 2550 | | 3.1 | 3.0 | 72.8 | 1500 | 120 |
| | 22 | 6.5 | | 1 | 3100 | | 6.1 | 10.5 | | 1750 | 2/25 |
| | 23. | 7,0 | | 17 | 33°C | | 6.3 | 11.5 | / | 700 | 240 |
| | 24 | 6.9 | | | 3300 | | 2.0 | 20 | | - 50 | } 27 5 |
| | 25 | 7.35 | | \ | 2650 | | 5, c | 10.01 | | 1430 | /8 ? |
| | 26 | 7, 4 | | | 2700 | | 6:9 | 10.0 | 2, | 7177 | Sega |
| | 27 | 7.9 | - | 17.7 | 2750 | | 27.357.379 | 570 | 165 | /458 | 735 |
| | 28 | 7,9 | T | | 2650 | ** | 6.5 | 10:05 | | 1038 | 262 |
| | 29 | . | | | | | | | 7 | | |
| | 30 | | | | ; | | | | | | |
| | 31 | | | | | | | | | | |
| - | | | Ţ | ţ | | 1 | | · | : | | |

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| 42-393 | | | Ŀ | e s t | | | | \ | lest | | |
|--------------|-------|------------|-------------------|-------------------------------|-------|-------------------------------|----------|----------------|-------------------------------|-------|-------------------------------|
| | D. L. | | Settled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ | ٠ | Settled Solids | P ₂ 0 ₅ | an. | P ₂ 0 ₅ |
| | Date | Hq | Vol.\$ | _ppm_ | GPM_ | TPD_ | рН | Vol.% | ppm | GPM | TPD_ |
| | 1 | 8.2 | Tr. | 70 | 2300 | 1.0 | 4.5 | .09 | 500 | 1600 | 4.8 |
| | 2 | 7.6 | Tr. | 15 | 2300 | .2 | 3.9 | 11 | 480 | 1450_ | 4.2 |
| _: | 3 | 7.8 | Tr. | Ò | 2700 | 0 | 3.7 | .36 | 1020 | 1600 | 9.8 |
| | 4 | 8.2 | Tr. | | 3100 | | 3.9 | .06 | 700 | 1750 | 7.3 |
| | 5 | 7.7 | Tr. | 23 | 2300 | .3 | 5.4 | .32 | 890 | 1500 | 8.0 |
| | 6 | 8.0 | Tr. | 13 | 2150_ | .2_ | _6.6_ | 1.30 | 600 | 1750 | 7.4 |
| • . | 7 | 8.0 | Tr. | 77 | 2150 | 1 | 4.8 | .40 | 1510 | 1450 | 13.1 |
| _ | 8 | 7.6 | Tr. | 17 | 2150 | .2 | 3.1 | | 1390 | 1450 | 12.1 |
| | 9 | ļ <u>.</u> | | | ļ | | <u></u> | | | | ļ |
| • | 10 | 7.6 | Tr. | 80 | 2700 | 1.3 | 3.2 | .20 | 1650 | 1750 | 17.3 |
| , | 11 | | <u> </u> | | | | <u> </u> | · | | · | · . |
| | 12 | 7.6 | Tr. | 17 | 2500 | -3 | 3.5 | .10 | 570 | 1450 | 5.0 |
| 1 80 | 13 | 7.6 | Tr. | 18 | 2500 | .3 | 2.7 | .32 | 2150 | 1600 | 20.4 |
| | 14 | 7.8 | Tr. | 11 | 2200 | .1 | 3.0 | .20 | 1350 | 1650 | 13.3 |
| _[- | 15 | 7.0 | Tr. | 70 | 2550 | 1.1 | 4.7 | .10 | 420 | 1750 | 4.4 |
| | 16 | 7.0 | Tr. | 67. | 2550 | 1.0 | 7.1 | 40 | 178 | 1450 | 1.6 |
| • | 17 | 7.0 | Tr. | 50 | 2700 | 8 | 5.9 | .25 | 300 | 1900 | 3.4 |
| | 18 | 7.5 | Tr. | - 50 | 2700 | .8 | 6.9 | .60 | 130 | 1900 | 1.5 |
| | 19 | 7.8 | Tr. | 25 | 2500 | 4 | 5.9_ | 25 | 183 | 1600 | 1.8 |
| • | 20 | 7.2 | Tr. | 50 | 2500 | .8 | 6.6 | .38 | 260 | 1600 | 2.5 |
| | 21 | 7.0 | Tr. | 60 | 2500 | .9 | 6:3 | .92 | 300 | 1350 | 2.4 |
| - | 22 | 7.4 | Tr: | 27 | 2150 | .4 | 6.0 | 1.0 | 460 | 1450 | 4.0 |
| | 23. | 4.4 | Tr. | 94 | 2150 | 1.2 | 6.3 | 2.0 | 620 | 1350 | 5.0 |
| | 24 | 7.2 | Tr. | 30 | 2950 | .5 | 5.6 | •35 | 600 | 1750 | 6.3 |
| | 25 | | | | | | | | | | |
| · · | 26 | 7.6 | .03 | 40 | 2150 | .5 | 2.5 | .15 | 2100 | 1450 | 18.3 |
| | 27 | 7.3 | Tr. | 50 | 1950 | .6 | 6.8 | .25 | 500 | 1300 | 3.9 |
| | 28 | 7.4 | Tr. | 70 | 1950_ | .8 | 2.6 | .02 | 250 | 1300 | 2.0 |
| · E | 29 | 7.6 | Tr. | 17 | 2400 | .2 | 4.0 | .05 | 600 | 1600 | .5.8 |
| • | 30 | 7.7 | Tr. | 18 | 5/100 | .3 | 4.4 | .30 | 370 | 1450 | 3.2 |
| | 31 | | | | | | | t ! | | | · |

| | | • | 1111 | ו א פיטי | . ע | renc | <u>ي</u> | | | | シ シシ | |
|--------|---------------------------------------|------|----------------|-------------------|---------------------------------------|----------|---------------------------------|--------------|-------------------|-------------------------------|--|-------------------------------|
| • | LEMPE | | <u> </u> | \sim / | (2) | | | (48) | [1] | (III) | | |
| 1 | 42-351 | · | (11) | | 37) (ast | | | | | i e sit | (1500) | <u>)</u> |
| | | | | Settled Solids | P ₂ 0 ₅ | | P ₂ 0 ₅ . | | Settled Solids | P ₂ 0 ₅ | | P ₂ O ₅ |
| • | | Date | Ha | | _ppm_ | GPM_ | TPD_ | pH /N o | Vol.8 | _ppm | GPM | _TPD_ |
| | | 1 | 8.2 | 17/ | 70 | 320 | 10 | 1.24 | .08 | 500 | 1600 | 4,6 |
| - | | 2 | 7.6 | 17/ | 15 | 23 | ,2 | 31/37 | .]! | 4/20 | 11/57 | 4.2 |
| • | | 3 | 78 | 17. | 0 | 2013 | 0. | 2-/ | 36 | 020 | - (- (- (- (- (- (- (- (- (- (- (- (- (- | 9.8 |
| • | | 4 | - 6- | 7/ | 0 | 17.0 | D | 5.9 | .06 | 700 | | 7.3 |
| | | 5 | - | Tr | 23 | . [| ج. | .06 | .32 | 890 | 21.7 | 8,0 |
| | <u> </u> | 6 | 8,0 | 71 | 13 | 1,370 | 2 | lake 🛴 | 130 | 600 | 1720 | 7.4 |
| • | • | 7 | () | 7, | 7_ | 12150 | ./ | 1.8/14 | ,40 | 15/0 | 1400 | 13/ |
| | | 8 | 7.6 | 7/ | 17 | -150 | , 2 | 3.1 | | 1390 | 1450 | 12.1 |
| - | | 9 | | | 1 | | | | | | | |
| • | | 10 | . (. | 7/ | 80 | 2000 | 13. | | .Z. | 1350 | 17 1 | 17 3 |
| | _ _ . | 11 | - | | | | | | - | | | 7-7-0 |
| - | | 12 | 7.7. | 10 | 177 | | . 3 | | ./: | 570 | 112 | 15.0 |
| - | _ | 13 | 7/ | 7/ | 1/ | 250) | 3 | 27 | .32 | 250 | , . | 1 |
| | <u> </u> | 14 | | -/, | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | 2) 11 | | 3.0 | .20 | V 330 | 160 | 133 |
| - | · · · · · · · · · · · · · · · · · · · | 15 | 7.0 | 17/ | 70 | 23. | 1/ | 11 y | | (/2.0 | 17(3) | 4.4 |
| = | | 16 | 120 | TV | 10 | 33,0 | 1.0 | 2.1 | · //) · | 1 1 ~ 1 | 11/50 | 1.6 |
| • | £-; | 17 | 7.0 | 7/ | 12. | 2700 | 1.0 | 1.1 | , 77 | 300 | 1730 | |
| - ! | | 18 | 1.5 | 17/ | 577 | 2700 | .8 | 1. 0 | | 130 | 19.1 | |
| - | | 19 | | 1 | | // | / | 2 / | | | | 1/3 |
| _ | | | 1.1 | TV | 3-7 | - | ι , ι / | |) | 1/3 | 1/3/2 | 1/2 |
| •_ | | 20 | 1/.2 | 1. | Kn | -5 | 9 | 10 | . F.S. | | /; ; | |
| - | | | 20 | 110 | 60 | 2,7// | +77 | <u>[a. 3</u> | 172 | 1000 | 13.0 | |
| _ | | 22 | |) Y | 27 | 513) | <u> </u> | 0 |),: | 1/,1 | 1723 | 17 |
| •- | | 23. | 4.4 | 50 | 4 .7 | 1.11 | 1/2 | 6 | 1 () | 1000 | 1500 | 3 |
| - | | 24 | 72 | TV | 30 | 1.75 2 1 | <u>ا ک</u> | 5.6 | | (QQL) | 1732 | |
| - | | 25 | | 1 | 10 | | | | | | <u> </u> | |
| _ | | 26 | 7.6 | - | 40 | | 5 | | 10 | 3100 | 1/6 | 12 |
| _ | . | 27 | 7.3 | 177 | 50 | 1930 | | 6 | | 200 | 1300 | 3.7 |
| | | 28 | 71 | 171 | 170 | 11(15) | ΄, χ | 3.1. | 02 | 220 | 1300 | 2, |
| _ | 5 | 29 | 7.6 | 17 | 17 | 8 (D) | ,2/ | 4.0 | <u> </u> | 600 | 1601 | 5.8 |
| • | - | _30 | 2.7 | 170 | 18 | 1-1 | ,3 | 4.4 | 30 | 3>0 | 11/3 | 12 |
| | • | 31 | | ļ | | | İ | | | | | |

| | 1 | EFFL | UENT | DI | гсне | S . | 1.16. | • | MONU | | |
|----------------|------|----------|---|----------|-------|-------------------------------|-------------|------------------------------|----------|--------|-------------|
| • | | | | | | = N | 1007 | o | Nov | 1-1967 | |
| 49.383 | | | E | ast | | . (| 130 | W | lest | | |
| / - | : | | | | L. | | | | • | E | yel! |
| | Date | } Hor | Settled Solids , & Vol. % | , P205' | _GPM | P ₂ O ₅ | Нд | Settled Solids ' Vol.% | P2011 | GPM | P205 TPD |
| | 1 | 8.20 | T | 17.2 | 2300 | | 4.50 | . 80 | | 1600 | 770 |
| ! | 2 | 7.60 | T | | 2300 | | 3.90 | | 1 89.1 | /450 | 970 |
| , | 3 | 7.80 | | | 2700 | | 3.70 | 3.60 | | 1600 | 2000 |
| | 4 | 8,20 | 7 | | 3100 | | 3.90 | . ó0 | | 175c | 950 |
| | 5 | 7.70 | 7 |) | 2300 | | 5,40 | 3.20 | 7 | /500 | 1500 |
| | 6 | 8.50 | 7 \ | | 2150 | | 6.60 | .3.00 | <u></u> | 1750 | 2425 |
| • | 7 | 8.00 | Т | | 2150 | | 4.80 | 4.00 | · | 1450 | 6000 |
| | 8 | 7.60 | 7 | | 2150 | | 3.10 | 4.20 | | 1450 | 1251 |
| | 9 | | | 78.7 | | | | | , 13.7 | | |
| • | 10 | 7.60 | <u> </u> | · | 2700 | | 3.20 | 2.00 | | 1750 | 3000 |
| · —: | 11 | 7.80 | | | 2400 | | 3.80 | 1.00 | | 1750 | 75 c |
| | 12 | 7.60 | T / | | 2500 | | 3.50 | 1.00 | , | 1450 | 225 |
| • | 13 | 7.60 | + | | 2500 | · | 2.70 | 3.20 | | 1600 | 1600 |
| | 14 | 7.80 | T | | 2200 | 7. 2. | 3.00 | 2.00 | | 1650 | 3500 |
| _[| 15 | 7.00 | T | | 455) | | 4.70 | 1.00 | | 1. | 125 |
| | 16 | 7.00 | T . | -17,6 | 2550 | · | 7.10 | 4,00 | 50.2 | /450 | 1125 |
| | 17 | 7,00 | - 1 | | 7760 | | 5.90 | 2,50 | | 1900 | 1000 |
| 6 0 | 18 | 7.50 | 7/ | | 3,100 | | 6.90 | 6.00 | | 1900 | 1000 |
| | 19 | 7.80 | τ | | 2500 | | 5.90 | 2.50 | | 160c | 875 |
| • | 20 | 1.20 | + | | 2500 | | 6.60 | 3.80 | | 1600 | 875 |
| | 21 | 7.00 | T | 27.4 | 2500 | | 2.30 | 05.€ | / | | 70.75 |
| <u> </u> | 22 | 7.40 | 一 | · | 2150 | | 6,00 | 10.0 | <u> </u> | 1450 | 12.72 |
| • | 23. | 4.40 | | | 8150 | | 3.30 | 20.0 | -64.8 | /350 | 1:0 |
| | 24 | 7.20 | T | | 2950 | | 5.60 | 3.50 | | 1750 | 117; |
| <u> </u> | 25 | | | | | ļ | | | | | - |
| <u> </u> | 26 | 7.60 | .30 | | 2150 | <u> </u> | 2.50 | 1.5 | | 1450 | 155 |
| | 27 | 7.30 | T. | <u>/</u> | 1950 | · | 6.80 | 2,50 | <u> </u> | 130c | 5 50 |
| | 28 | 7.40 | T | -13,6 | 1950 | <u> </u> | 2.60 | ,15 | 72.7 | 1300 | 250 |
| <u></u> | 29 | 7.60 | $\left \begin{array}{c} \mathcal{T} \end{array} \right $ | | 2400 | | 4,00 | .50 | <u> </u> | 1600 | 1254 |
| • | 30 | 7.70 | + | | 2.400 | <u> </u> | 4.40 | 3.00 | ļ | 1450 | 1125 |
| - | 31 | | | į | 1 | j | 1 | İ | | | i |

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| • | Date | • | | Settled Solids Vol.% | P ₂ O ₅ | GPM_ | P ₂ O ₅ | H_ | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ |
|----------------|------|---------------------------------------|----------|----------------------------|-------------------------------|----------|---------------------------------------|----------|----------------------------|-------------------------------|-------|-------------------------------|
| • | 1 | | 8.1 | Tr. | 13 | 2400 | 2 | | <u> </u> | | . | |
| _: | 2 | | 7.9 | Tr. | 15 | 2050 | .2 | | | | | |
| | 3 | | 7.5 | .1 | 16 | 2550 | .2 | | | | | |
| • | 14 | | 7.8 | Tr. | 7 | 2550 | .1 | | , | | | |
| <u> </u> | 5 | | 7.7 | .1 | 7 | 2400 | .1 | | | | - | |
| : | 6 | | | | | | | | | | | |
| • | 7 | | (pı | mp out | of order | .) | | | | | | |
| 1 | 8 | | <u> </u> | | | · | | | | | | |
| | 9 | | · · | | | | | <u>·</u> | | | | |
| | 10 | | | | | | | · | | | | ! |
| - , | 11 | | | | | | | ļ | | | | <u>.</u> |
| | 12 | | | | | | | 7.5 | .45 | 370 | 1750 | 3.9 |
| | 13 | • . | | | • | | | · | | | · · | <u> </u> |
| • <u>*</u> | 14 | | | | | | | 7.9 | .6 | 650 | 1900 | 7.4 |
| | 15 | | | | | · | 7 | 6.1 | .35 | 735 | 1750 | 7-7 |
| | 16 | | | | | | | 6.3 | 1.3 | 1270 | 1600 | 12.2 |
| • | 17 | | _ | | | | <u></u> | 5.4 | .02 | 570 | 1350 | 4.€ |
| | 18 | | | | | | | 7.4 | 1.4 | 600 | 1350 | 4.5 |
| | 19 | | | - | | | | 6.8 | .5 | 340 | 1750 | 3.€ |
| • | 20 | | | | | · · | <u> </u> | 6.8 | 45 | 420 | 1900_ | 4.8 |
| | 21 | | | | | · | | <u>:</u> | | <u> </u> | | |
| - | 22 | | | | | | ļ | 6.6 | .85 | 800 | 1500 | 7.2 |
| • | 23. | <u> </u> | | · | -: . | | | 5.8 | .9: | 1470 | 1600 | 14.1 |
| _ | 24 | | - | | | <u> </u> | | 3.8 | -06 | 830 | 1350_ | 6.5 |
| | 25 | | | | | <u> </u> | <u> </u> | 4.5 | Tr. | 420 | 1100 | 2.8 |
| | 26 | - | | | | | | 3.7 | .5 | 18000 | 1450 | 15.6 |
| | 27 | · · · · · · · · · · · · · · · · · · · | | | | <u>i</u> | <u> </u> | | | | | |
| | 28 | | - | | - | | | <u> </u> | | ļ. | | <u> </u> |
| | 29 | | | | ! | ! | · · · · · · · · · · · · · · · · · · · | 3.2 | .5 | 1830 | 1450 | ! |
| | 30 | | | | | ļ·. | <u> </u> | 5.8 | .6 | 550 | 1450 | i |
| | 31 | . | 7.7 | Tr. | 15 | 2300 | .2 | 3.9 | .5 | 1650 | 1050 | 10.1 |

West (500) East Settled Settled P₂0₅ P205 P₂O₅ _TPD_ P₂O₅ TPD_ Solids Vol.% Solids Date Vol.% GPM_ рĦ ppm GPM 1 -400 **少**迈 1300 2050 2 120 2510 3 1600 4 5 (% £ (/A) 2.1 6 11(01) 7 on. 8 9 10 11 Par & Burn 11 370 12 13 6:10 14 15 16 17 1350 18 19 340 3. 6 20 420 21 2 10 $Y_{i_1}(\gamma_i)$ 22 1970 23. 24 420 25 26 2 000 27 28 1230 1260 29 <u>537</u> 30 11,50 31

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| 42-383 | | | E | ast | | " 1" | | Ţ. | lest (مرابع | . · · | |
|-------------|------|--------------|-------------------|-------------------------------|------------|----------|------|-------------------|----------------|--------------|-------------------------------|
| | | | Settled Solids | P ₂ 0 ₅ | • | P.O. TED | | Settled Solids | P205 | | P ₂ 0 ₅ |
| • | Date | Hq | Vol.% | ppm | <u>GPM</u> | TPD | Hq | Vol.% | ppm | <u>GPM</u> | TPD |
| | 1 | 8,1 | 1 | | 2400 | · | | | | | Did! |
| <u>'</u> | 2 | 7.5 | T | | 2050 |) | 6.2 | 10.0 |) | /300 | (|
| | 3 | 7.5 | / | | 255-0 | · | 6.5 | 5.0 | | 1750 | |
| <u> </u> | 4 | 7,8. | 1 | | 25.0 | >,4 | 4.0 | 1.0 | (/. 2 | 1600 | |
| | 5 | 7.7 | / | | 2400 | | 7.7 | 4,5 | | 15 3 | |
| · | 6 | ļ, | | | | <u> </u> | 7,2 | 1,5 | | 1750 | |
| • . | 7 | , | | : | | | | | | | |
| | 8 | | | | <u> </u> | | | | · | | · · · |
| | 9 | 7.8 | -0- | | 2050 | \ | 3.0 | 4 |) | 72300 | |
| • | 10 | 1.9 | - 0 - | | 2050 | | 7.17 | () | / 12./ | 17570 | 1 |
| _: | 11 | 1.3 | 1 | | 2550 | 10.2 | 2.8 | 2 | | 1750 | |
| <u> </u> | 12 | 1.9 | T | | 3200 | \ \ | 7.5 | 4,5 |) | 1750 | Cont. |
| | 13 | 7.57 | 7 | | 1600 | | | | | · | ļ <i>'</i> |
| k | 14 | | | | <i>/</i> . | 1 | 7.9 | 6,0 | <u> </u> | 1900 | 1/ |
| | 15 | | | | | | 6.1 | 35 | / | 1750 | |
| <u> </u> | 16 | 7.8 | T | | 2050 | greet | 6,3 | 13.0 | | 1600 | V. |
| • | 17 | 8.0 | T | | 2200 | | 5.4 | .2 | 62.5 | 1352 | ľ |
| | 18 | 4.0 | <u></u> | | 2050 | | 7.4 | 14.0 | i | 135 | 1 |
| | 19 | 7.5 | 丁 | | 1900 | 18.1 | 6.8 | 5,0 | | 1750 | |
| • | 20 | 7.8 | T | | 2300 | | 6.8 | 4.5 | | 190C | |
| | 21 | ļ | | | | | 6,60 | 6.0 | · | 1750 | · ~ |
| | 22 | ļ | | | | | 6.64 | 8.5 | | 1500 | |
| | 23. | 7.9 | T | | 2300 | | 5,85 | 9.0 | | 1600 | <u></u> |
| · · · | . 24 | 8.0 | T | | 3300 | ļ | 3.83 | 65 | /- | 1350 | - |
| | 25 | 7.84 | T | | 2300 | <u> </u> | 4.50 | .05 | 90.1 | 1100 | 1 |
| | 26 | 0.8 | + | | 2400 | 6.9 | 3.70 | 5.0 | ļ | 1450 | deg. |
| • 6 | 27 | 7,75 | T | | 1900 | | | | | | ples |
| | 28 | <u> </u> | <u> </u> | · | | ļ | 3.85 | 1.10 | ļ 4———— | 1900 | |
| - | 29 | | | | /\ | | 3.15 | 5.2 | | <i>14</i> 50 | 650 |
| • | 30 | 7.50 | T | | 1950 | | 5.80 | 6.2 | i | 1450 | 80c |
| - | 31 | or.r | T | | 2300 | (Comp) | 3.90 | 5.20 | | 1600 | 105 |

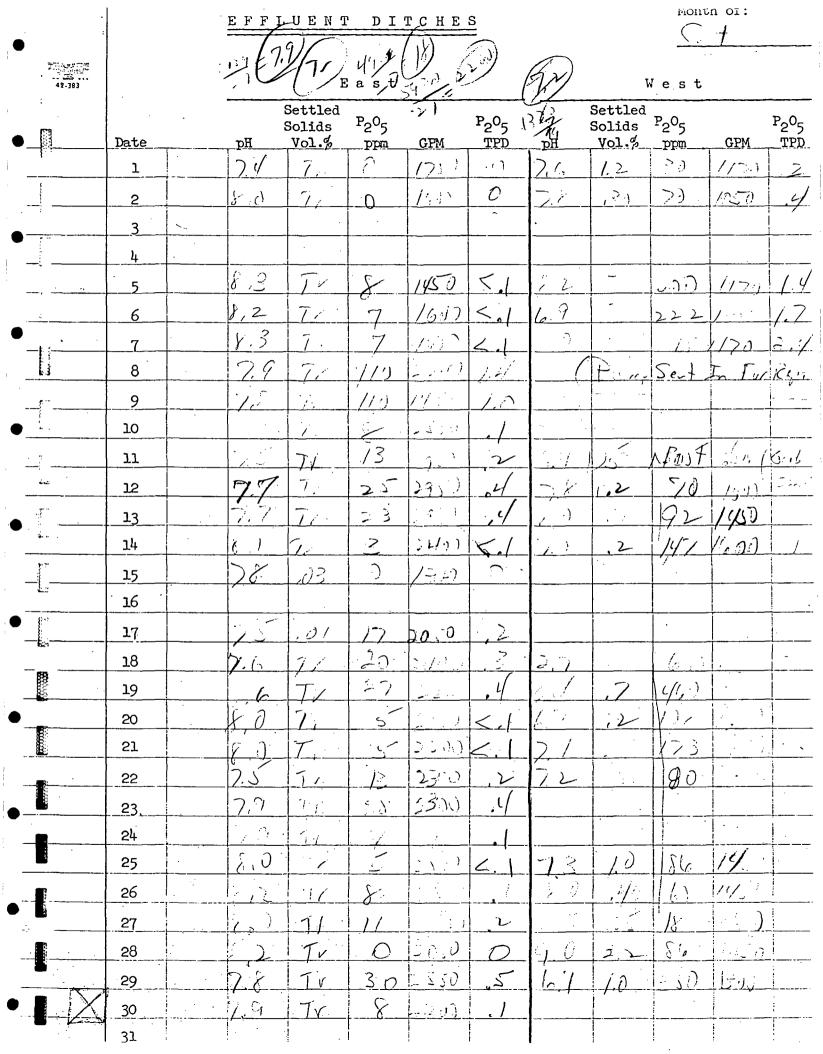
September, 1967

MOHUN OI:

42.383

East

| 42-383 | ļ | | | E | ast | | | | , | Vest | | |
|----------------|------|---------------------------------------|------|----------------------------|-------------------------------|------|-------------------------------|----------|----------------------------|-------------------------------|--------------|---|
| | Date | | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | рН | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ |
| | 1 | | 7.4 | Tr. | 0 | 1750 | .0 | 7.6 | 1.2 | 30 | 1170 | .2 |
| , | 2 | | 8.0 | Tr. | 0 | 1600 | 0 | 7.8 | .30 | 70 | 1050 | .4 |
| | 3 | | 0.0 | | | 1000 | | | 155 | <u>!</u> | | |
| • | 4 | | | | | | | | | | | |
| <u> </u> | 5 | · | 8.3 | Tr. | 8 | 1450 | 〈. 1 | 8.2 | | 200 | 1170 | 1.4 |
| | 6 | | 8.2 | Tr. | 7 | 1600 | \(\lambda \) | 6.9 | | 222 | 1300 | 1.7 |
| • | 7 | | 8.3 | Tr. | 7 | 1450 | \(. 1 | 8.0 | | 345 | 1170 | 2.4 |
| | 8 | | 7.9 | Tr. | 110 | 2200 | 1.4 | (| Pump se | nt in fo | repai | r) |
| | 9 | | 7.8 | Tr. | 110 | 1450 | 1.0 | | | | | |
| • | 10 | | 8.1 | Tr. | 8 | 2550 | .1 | · | | | | |
| _: | 11 | · | 7.5 | Tr. | 13 | 2950 | .2 | · | | | | |
| | 12 | | 7.7 | Tr. | 25 | 2950 | .4 | | | | | <u> </u> |
| | 13 | · . | 7.7 | Tr | 23 | 2950 | - 14 | · | | | <u> </u> | ļ |
| | 14 | | 8.1_ | Tr. | 3 | 2400 | X.1_ | | - | | - | |
| | 15 | | 7.8 | .03 | 0. | 1300 | 0 | <u> </u> | | | | <u> </u> |
| | 16 | | | | | | | · ——— | | | | <u> </u> |
| | 17 | | 7.5 | .01 | 17 | 2050 | .2 | | ļ. <u></u> | | | |
| | 18 | | 7.6 | Tr. | - 20 | 2400 | -3 | ` | | - | <u> </u> | <u> </u> |
| | 19 | | 7.6 | Tr. | 27 | 2200 | .4 | | | ļ | <u> </u> | |
| • | 20 | | 8.0 | Tr. | 5 . | 2550 | ۲.1 | | | | ļ | |
| | 21 | | _8.0 | Tr. | 55 | 2200 | ۲.1 | | | | | <u> · </u> |
| - | 22 | | 7.5 | Tr. | 13 | 2300 | .2 | | | | | |
| • | 23 | · | 7.9 | Tr. | 28 | 2300 | .4 | | | | | |
| - | 24 | | 7.9 | Tr. | 7 | 2400 | .1 | | | | + | |
| <u> </u> | 25 | | 8.0 | | 5 | 2550 | ۲.1 | | | | | ļ. ——— |
| - | 26 | · | | | | ļ | | | <u> </u> | | · . | <u> </u> |
| ▼ 1 5 | 27 | · · · · · · · · · · · · · · · · · · · | | <u></u> | | | |] | | | <u> </u> | |
| _ | 28 | | | · | ļ | | <u> </u> | | ļ | <u> </u> | | |
| | 29 | | | | | | | | | | | <u> </u> |
| • | 30 | | | | ļ | ļ | | | ļ | ļ . | | |
| - . | 31 | | | | | | - | ľ | ľ | | | |



TACTION OF

Sixt 1967

| | | | : | | • | | | | | | | |
|------------------|-------------|----------|-----|----------------------------|-------------------------------|------------------------------|---------------------------------------|---------------|----------------------------|--------------|---------------------|-------------|
| 42-383 | | | | E | ast | | V | | | <i>l</i> est | | |
| • | <u>Date</u> | F | | Settled Solids Vol.% | P ₂ O ₅ | - ونيا اردا GPM | P.J.J. | | Settled Solids Vol.% | P205 | ۶-)? ازجا GPM | P 07 |
| | 1 | , 8 | 7.4 | 1 | | スコ | .8 | 7.6 | 12.0 | | 1170 | 2.6 |
| | 2 | | 80 | 7 | | 1600 | | 7.8 | 3.0 | · | 10570 | |
| | 3 | | | | | | | | | | | |
| | 4 | | | | | | | | | | · | |
| | 5 | | 8.3 | 1 | | 1450 | | 9.0 | | | 14:0 | \ |
| | 6 | | 8.2 | | | 1600 | | <u>6.9</u> | <u> </u> | | 1200 | <u> </u> |
| • . | 7 | | 83 | 1 | | 1450 | | 8.0 | | | 1170 | |
| | 8 } | 1.4 | 7,9 | T' | | 2200 | | | <u> </u> | | | 72.9 |
| | 9 | | 7.8 | ·- - | | 14:00 | | £ | E11' | 11-15 | S 1 11 | |
| • | 10 | | 8.1 | - | | A500 | | | | · · | 1450 | |
| | 11 | - | 75 | T | | 2627 | | 6 | 5.0 | | 1600 | Plan |
| <u> </u> | 12 / | | 7.7 | 1 | | 2950 | | 7.8 | 2.0 | | 1600 | ~ |
| | 13 | | 1.7 | 1 | | 25.87 | | 8.0 | 1.0 | | 1450 | 7.2. |
| - | 14 | 7.6 | 8./ | | | 2400 | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | <u> 200</u> | 2,0 | | 1600 | |
| | 15 | | 1.6 | .3 | | 1300 | | | | | | ; ; |
| | 16 | | | | | | | | | | / | · · |
| • • | 17 | | 7,5 | ,/ | | 2050 | | | | | | |
| - <u> </u> | 18 | | 7.6 | 1 | | 2 | | 2.7 | . T | | 750 | <u>ئ</u> |
| | 19 | | 7 | 1 | | 2200 | | | 7,0 | | 150 | /_ |
| • | 20 / | | 8.0 | T | | 2550 | | 6.7 | 2,0 | | 1600 | 13.9 |
| | 21 | > ,7 | 8.0 | T. | | 2220 | | 7.1. | 4.0 | <u> </u> | 1450 | |
| | 22 | | 7.5 | 1 | - | 2300 | · | 7.2 | 57.2 | | 11751 | |
| | 23/ | <u>-</u> | 7.9 | 5 | | 2300 | | | | | / | <u> </u> |
| | 24 | | 7.9 | T | | 2400 | | · · | | | | |
| | 25 | | 8.0 | 1 | | 2550 | | /~ <u>-</u> . | 10. | | 150 | |
| _ | 26 | | 8,2 | 1 | | 32.70 | | 8.0 | 4.0 | | 1450 | γ. - 3.7 |
| • & · | 27 | | 8.0 | T | | 2400 | | 8.5 | 2.5 | | 1450. | 135. |
| | 28 | 711.2 | 8,2 | 1 | | 2050 | | 9,0 | 22.0 | | 1450 | |
| | 29 | · | 7.8 | T. | | 25-5-0 | | 6.7 | 10.0 | | 1300 | |
| • | 30 | | 2.9 | T | | 2200 | | <u>-</u> | | | | |
| - | 31 | | | • | | | ļ | | ſ | | | ! |
| | | | | | | | | | | | | |

August, 1967

East

| • | Date | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | рН | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ |
|---|------|------------|----------------------------|-------------------------------|-------|-------------------------------|------------|----------------------------|-------------------------------|-------------|-------------------------------|
| | 1 | 8.0 | Tr. | 18 | 1750 | .2 | 7.5 | .03 | 23 | 1170 | .2_ |
| | 2 | 7.7 | 0 | 5 | 1450 | < .1 | 5.9 | .70 | 188 | 1450 | 1.6 |
| | 3 | | | | | | | | | | |
| | 4 | | | | | | | | <u> </u> | | |
| | 5 | | | | | | | | | | |
| | 6 | | | | , | | | | | | |
| • · · · · · · · · · · · · · · · · · · · | 7 | 7.8 | Tr. | -11 | 2400 | .2 | 6.7 | .70 | 83 | 1170 | .6_ |
| دره در در در در در در در در در در در در در | 8 | 7.5 | Tr. | 23 | 2400 | .3 | 8.3 | .06 | 37 | 1450_ | .3_ |
| | 9 | 7.7 | Tr. | 11 | 2400 | .2 | 8.3 | .15 | 18 | 1450 | .2 |
| • | 10 | 6.7 | .02 | 57 | 1170 | .4 | 8.0 | .60 | 193 | 1300 | 1.5 |
| | 11 | 3.7 | Tr. | 50 | 1170 | .4 | 7.9 | .65 | 200 | 1300 | 1.6 |
| . <u>- La</u> | 12 | 7.3 | Tr. | 50 | 1170 | .4 | ļ | | | <u>.</u> | <u> </u> |
| | 13 | 7.3 | Tr. | 18 | 17750 | .2 | | | <u> </u> | <u> </u> | <u> </u> |
| i . | 14 | 7.4 | .02 | 21 | 2400 | 3 | 7.2 | •35 | 198 | 1170 | 1.4 |
| | 15 | 7.7 | Tr. | 15 | 2700 | .2 | 6.0 | .65 | 295 | 1170 | 2.1 |
| <u> </u> | 16 | 7.8 | Tr. | - 8 | 2550 | 1.1 | 6.2 | .80 | 210 | 1170 | 1.5 |
| | 17 | 7.5 | 0 | 20 . | 2700 | .3 | 6.8 | .45 | 127 | 1450 | 1.1 |
| <u> </u> | 18 | 7.5 | Tr. | 50 | 1450 | .4 | 6.8 | .30 | 280 | 1050 | 1.8 |
| | 19 | 7.3 | Tr. | 30 | 1500 | 3. | 7.5 | .10 | 70 | 920 | 1.1. |
| • | 20 | 7.5 | Tr. | 18 | 2400 | .3 | 7.7 | .35 | 30 | 1170 | ,2 2-} |
| | 21 | 6.8 | .10 | 281 | 2500 | 4.2 | 6.2 | .03 | 78 | 920_ | .4_ |
| | 22 | 7.9 | Tr. | 13 | 2700 | .2 | 3.3 | .40 | 980 . | 1170 | 6.9 |
| • | 23 | 7.1 | Tr. | 20 | 2400 | •3 | 6.1 | .80 | 89 | 1300 | .7 |
| - - | 24 | 7.8 | Tr. | 15 | 2550_ | 2 | <u>6.3</u> | 1.0 | 244 | 1300 | 1.9 |
| | 25 | 7.6 | Tr. | 108 | 1750 | 1.13 | 2.9 | .25 | 30 | 920 | .2 |
| | 26 | 7.7 | Tr. | 0 | 1300_ | 0 | 7.2 | .30 | 50 | 1170 | -4- |
| — <u>— — — — — — — — — — — — — — — — — — </u> | 27 | 6.0 | .05 | 55 | 2700_ | .9 | 7.8 | 35 | 44 | 1450 | -4 |
| | 28 | 7.4 | .01 | 15 | 2400 | .2 | 8.7 | .40 | 71 | 1170 | 1.1 |
| | 29 | 7.8 | | 8 | 2700 | 1.1 | 7.1 | | 98 | 1450 | .8 |
| • | 30 | <u> </u> . | | | . | <u> </u> | · | | | | 1-1 |
| - | 31 | | | | | | | t | | [i 1 | |

| | İ | EF | FL | UENT | DI | гсне | S | | | Mont | n, 01: | |
|----------|------|-----------------------------|---|-------------------|-------------|--------|---------------------------------|----------------|-----------------|-------------------------------|------------------|-------------------|
| • | | · <u>=</u> γ ήγ | / <u> </u> | | 421 | 7 711 | = //.} | $D^{\alpha N}$ | . • | 21.1 | //y _ | |
| 42.383 | | | $\left\langle \cdot \right\rangle \cdot \left\langle \cdot \right\rangle$ | \mathcal{L}^{N} | a 26/t | 3/1 | / | | 112 | رلبرگر I e_s t | 3/// | 2) |
| | | 7 | 7 | Settled | | - | Z | | Settlen | 1.191 | (1255) | |
| | Date | (* / <u>.</u> H q | | Solids Vol.% | P205 Ppm | GPM C | P ₂ 0 ₅ (| (, , \) pH | Solids Vol.% | P ₂ 0 ₅ | GPM_ | P ₂ 05 |
| | 1 | 8. | | 70 | / | 120 | . 2 | 7 | .03 | 23 | 1125 | . 2 |
| | 2 | 5. | \rightarrow | \circ | 3 | 1454 | <./ | 5.9 | . 7.0 | 12. | 142 | 1.6 |
| • | 3 | | | | | | | | | | | |
| | 4 | | | | | | | | | | | |
| <u> </u> | 5 | | , | | | | | | | | | |
| <u> </u> | 6 | | | | | | | · | | | | |
| i | 7 | 7 | 2 | 77 | 11 | . Zyn? | .2_ | 67 | | 8 5 | 1:15 | .6 |
| 1 | 8 | • | | Tr | 23 | -443 | . 3 | | .06 | 37 | 1140 | 3 |
| | 9 | 2, | 7 | 70 | 11 | 2400 | .2 | 23. | ./5 | K | 1452 | , |
| • | 10 | 6. | -/ | | 21 | 1178 | 4 | 20 | .60_ | 113 | 1>1 | 1.5 |
| | 11 | | 1 | 11 | 50 | 11-10 | | 1.7 | ٠/ ن | -)0 | 1308 | 1.6 |
| <u>ٺ</u> | 12 | | 3 | 71 | <u>.</u>) | 1170 | ./ | | | - 1 | - | <u></u> |
| | 13 | | 13 | 1 | 15 | 1780 | 12 | | | | | ļ |
| | 14 | 7 | ,4 | .02 | 51 | 46) | ``` | | 35 | 13% | 170 | /_ |
| , a s | 15 | -/ | | Īć | 15 | 2 | 2 | 6,0 | 1065 | 295 | 114. | 2.7 |
| | 16 | | 7_ | - Î. (| 8 | - 4 | | 42 | 53. | 210 | <i></i> | 1.5 |
| | 17 | | <u> </u> | ٥ | 3-17 | 2710 | , 5 | 68 | ,115 | 122 | 11/ | 1.1. |
| | 18 | - | | | -5) | / | 1 | 4.8 | .30 | | | 1.8 |
| | 19 | -/ | . 3 | 70 | 30 | | , 3 | .7.5 | .10 | 20 | 127 | 1, (/ |
| • | 20 | | | īc | 18 | 20 | 3 | 1/ | | 30 | | . 2- |
| | 21 | 6 | <u> </u> | 16 | 281 | | 11/2 | · 2 | 1 | 75 | 1 | 1./ |
| _ | 22 | | 2 | 71 | 13 | - / | ,2 | · .; | .40 | 910 | 11.11 | 6,9 |
| | 23 | | ./_ | 7, | (۽ د | 2 (1) | 3 | <u> </u> | J.A. | 7 | 1000 | 7 |
| - | 24 | 2 | 2 5 . | 7 | 15 | | , 2 | <u></u> | / | 24/1/- | 20 | 1.9 |
| | 25 | - / | | D | 10 | 1549 | 1.1. | <u> </u> | | 35 | 1726 | 2 |
| | 26 | | | · | 1-6- | 1 | (| | | 1 1 | · V) | . 4/ |
| - B | 27 | | | .05 | 55 | 2700 |). | | | <u> </u> | 145) | 4 |
| 2 | 28 | | 4 | |) , | | <u> </u> | | <u> </u> | 11 | <u></u> | <u> </u> |
| | _29 | | : | .02 | 8 | \> | | | 1.25 | 92 | 1.00 | 8 |
| • | 30 | | 1 | 70 | 0 | 3950 | 0 | 60 | 1./_ | 42, | 1600 | 1/ |
| | 31 ! | | | - | 1 7 | | 1 ./ | 1 : · / | <u> </u> | 33 | 10.99 | 1.3 |

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| 42-353 | | | | <u> </u> | ast | | | · | I | <i>l</i> est | | |
|---|--------|----------------------|------|----------------------------|-------------------------------|--------|-------------------|-----|----------------------------|--------------|-------------|-------------------------------|
| • | Date | ppm F | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P2 ^O 5 | | Settled Solids Vol.% | ppm_ | GPM | P ₂ O ₅ |
| | ı | 1/ | | 0 |] | | | | 3.5 | | GPM 1/3/ | |
| | 2_ | | 8.0 | T | | | | 7.5 | 3 | | | |
| | 3 | | _ | | | | | | _ | | 0.1 | |
| | 4 | | 7.7 | 0 | | | | 5,9 | 7.0 | 6 | V 1 1 | |
| | 5 | 10.0 | | | | 2400 | | 7 | | | 1250 | |
| | 6 | | - | | | | | | | | | |
| • | 7 | N T | 7.8 | T | | | | 6.7 | ?.5 | | | |
| | 8 | | 7.5 | T | | | | 8.3 | 1.6 | 7 | 1 | |
| | 9 | / | 7.7 | Í | | 2700 | | 8,3 | 1.5 | >207 | | 205 |
| • | 10 | 7.41.9 | 6.7 | 1,2 | | | | 8.0 | 6.0 | | | |
| \$ · | 11_ | <u>.</u> | 3.7 | 1 | | | | 7.9 | 6,5 | | | |
| | 12 | | 7.3 | T | | | | | | | | |
| • | 13 . \ | | 7.3 | T. | · | 1750 | | | | - | | ,26. |
| | 14 | <u>\</u> | 7.4 | .2 | | 2400 | 1 | 7.2 | 3.5 | | | 11- |
| | 15 | <i>!</i> | 7.7 | | | 2700 | | 6.0 | 16,5 | //. | | 1/7 |
| | 16 | | 2,8 | 7 | | 2000 | | 62 | 8.0 | 1 | 1 | 1. 2. |
| • | 17 | 27.7 | 75 | 0 | | 2750 | . ' | 6.4 | -15 | 76 | | 145 |
| | 18 | | 7.5 | T | | /4 373 | | 6.8 | 3.0 | (| | 105 |
| | 19 | ! ! | 7.3 | 7 | | 1500 | | 7.5 | 1.0 | | | 92 |
| •_ | 20 - | | 7,5 | T | | 2400 | | 7.7 | 3.5 | | | 1170 |
| | 21 ` | \ | 6,6 | / | | 100 | | 6.2 | , 3. | | | 920 |
| _ _ | 22 | <u> </u> | 7.9 | T | | 2700 | | 3,3 | 4.0 | | ļ | 1170 |
| | 23 | -17.3 | 7./ | | | 2400 | | 6:1 | 8,0 | | " i | 130 |
| - | 24 | ļ' | 7.8 | T | ļ ļ | 251510 | | 6.3 | 10,0 | 1 3/ | •• | 130 |
| | 25 | | 7.6 | T | | 1750 | | 2.9 | 2.5 | | | 920 |
| | 26 |) i . ! | 7.7 | 7 | | 1305 | | 7.2 | 3.0 | 1 | <u> </u> | //7 |
| - · · | 27 | | 6.0 | ,5 | | 2757 | | 7.8 | 3,5 | 1 | <u> </u> | 100 |
| | 28 | | 1,4 | ./ | <u> </u> | 2400 | | 8.7 | 4 | | <u> </u> | 1170 |
| • · · · · · · · · · · · · · · · · · · · | 29 (| | 7.8 | 12 | | 2700 | | 7./ | 2.5 | / | <u> </u> | 145- |
| — | 30 | | 7.8 | 7 | | 2750 | | 6.0 | 11.0 | <u> </u> | <u> </u> | 160 |
| _ | 31. | i) Y | 17.8 | ナ | | 2200 | | 7.4 | 10 | 1 | | 160 |

49-333

July, 1967

East

| | Date | | Settled Solids Vol.% | P ₂ O ₅ | - GPM | P ₂ O ₅ | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ |
|----------------|------|--|----------------------------|-------------------------------|----------|--|-----------|----------------------------|-------------------------------|-----------|-------------------------------|
| , - | 1 | <u> </u> | 1 | ppin | GFM | <u> </u> | <u>pn</u> | <u> </u> | _ ppm | GFM | |
| | 2 | ļ | | | | · | | | | | |
| | 3 | 8.3 | 0 | 5 | 1.800 | ۷. 1 | 9.0 | .80 | 60 | 920 | 3_ |
| | 4 | | | | | | | | | | |
| | 5 | 8.7 | 0 | 7 | 1050 | ۲ .1 | 8.9 | 0 | 18 | 920 | .1 |
| | 6 | 6.3 | .80 | 300 | 1050 | 1.9_ | _5.3 | .50 | 460 | 900 | 2.5 |
| | 7 | 7.5 | .02 | 80 | 1450 | .7 | 8.3 | .50 | 800 | 800 | .4 |
| <u>U</u> | 8 | 7.9 | Tr. | 13 | 920 | <u>ل ، ا</u> | 9.3 | 1.3 | 3 | 700 | <u>۲.1</u> |
| -[| 9 | 7.2 | Tr. | 230 | 1170 | 1.6 | 8.6 | .30 | 62 | 800 | .3_ |
| • | 10 | 8.0 | Tr. | 5 | 1300 | 4.1 | 7.2 | -95 | 151 | 1170 | 1.1 |
| , - | 11 | 8.2 | 0 | 7 | 930 | 4.1 | 6.8 | .15 | 105 | 1170 | .7 |
| <u> </u> | 12 | 8.2 | Tr. | 5 | 1170 | < .1 | 7.5 | Tr. | 28 | 930 | .2 |
| - | 13 | <u> </u> | <u> </u> | • | | | 8.3 | .30 | 10 | 1170 | <u> </u> |
| F., | 14 | 7.3 | 0 | 50 | | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | 3.0 | .15 | 1600 | | |
| <u> </u> | 15 | | `. | | | | | | | | <u> </u> |
| <u></u> | 16 | 8.0 | 0 - | 9. | 1600 | 4.1 | 6.5 | Tr. | 92 | 700 | <u>.</u> 4. |
| | 17 | 7.6 | Tr. | 25 | 1600 | .2 | 6.4 | .02 | 72 | 930 | 4_ |
| | 18 | 7.3 | Tr. | 37 | 1900 | .4 | 7.3 | Tr. | 48 | 930 | •3 |
| | 19 | 6.6 | 0 | 28 | 1450 | 2_ | | | | | |
| • | 20 | 8.5 | Tr. | 30 | 1750 | 3 | 8.3 | .01 | 113 | 1050 | .7 |
| Super | 21 | 8.1_ | Tr. | 80_ | 1170 | .6 | 7.9 | .08 | 80 | 930 | <u>.</u> 4 |
| - | 22 | 8.2 | .01 | 30 | 1450 | .3 | 7.9 | .02 | 70 | 930 | .4 |
| | 23. | 7.0 | .01_ | 67 | 1170 | .5 | 8.1 | .15 | 55 | 1050 | .3 |
| - | 24 | 8.0 | 0 | 7 | 1170 | (.1 | 7.9 | .04 | 83 | 1050 | .4 |
| . | 25 | 8.0 | 0 | 88 | 1170 | \(\) .1 | 7.5 | .30 | 147 | 1300 | 1.1 |
| | 26 | 8.0 | .01 | | 1450 | (.1 | 7.8 | .02 | 86 | 1170 | .6 |
| - | 27 | 7.9 | 0 | 8 | 1450 | <u> </u> | 7.6 | .02 | 37 | 1300 | .3 |
| | 28 | 6.9 | 0 | . 50 | 1450 | .4 | 6.6 | .02 | 440 | 1300 | 3.4 |
| . | 29 | | | | | | | | <u> </u> | \ <u></u> | <u> </u> |
| • | 30 | 7.8 | 0 | 8 | 1450 | ر .1 | 6.5 | .20 | 720 | 1170 | 5.C |
| | 31 | 8.2 | 0 | 8 | 1450 | (.1 | 6.8 | •35 | 183 | 1450 | 1.έ |

Month of: July - 67

| 42-383 | | | | E | ast | | | | V | Vest | | |
|---------------------------------------|------|--------------|------|----------------------------|----------------|----------|---------------------------------------|-------|----------------------------|--------------------|----------|-------------------------------|
| • | Date | 1/25 7 | | Settled Solids Vol.% | P2O5 | GPM | P ₂ O ₅ TPD | b/25- | Settled Solids Vol.% | P2 51/25 ppm). | - GPM | P ₂ O ₅ |
| | 1 | 17 | | | | | | | | | 111.3 | |
| · ; | 2 | 16.8 | | | | | | | | J | | |
| | 3 | | | | | | | | antie | | | |
| | 4 | | 8.3 | -0- | | | | 9.0 | anti- |) | | |
| | 5 | 7 | 8.7 | | | | | 99 | 0 | | | |
| : | 6 | | 6.3 | 8.0 | | | | 5.3 | 57. | 53.9 | | |
| • | 7 | 10.x | 7.5 | .2 | | | | 8,3 | 57 | | | |
| | 8 | 1 | 7.9 | T. | | <u> </u> | | 93 | 13.0 | | | <u> </u> |
| | 9 _ | 1 | 7.2 | | | | | 8,6 | 5.5 | / | | |
| • | 10 | | 8.0 | - | | | | 7.2 | Gy . | | | <u> </u> |
| | 11 | | 8.2 | - 0 | | | | 6.8 | 1.5 |] | | |
| <u>.</u> | 12 | 1.0 | Y,2 | T | | | | 7.5 | <u> </u> | 4.6 | | |
| •/ | 13 | HO Son's | _ | | | | | 8.3 | 7 | <u> </u> | | |
| | 14 | \ <u>.</u> . | 7.3 | 0 | C | | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | 30 | 1.5 | | | |
| | 15 | | | _ | 5. | | | | <u> </u> | | | |
| | 16 | 1 | 8.0 | 0 | | | | 6.5 | 1/ | | | <u>.</u> |
| • | 17 | | 7.6 | 7 | · | | | 6.4 | 12 | | | |
| | 18 | | 7.3 | T. | | | | 7.3 | T | | | |
| | 19 | 19,6 | 6.6 | -0- | | | | | | 1 | .4 | |
| • <u>Fr:</u> | 20 | | 8.5 | | | | | 8.3 | ./ | 7.5 / | <u> </u> | |
| | 21 | | 8.1 | 1 | | | | 7.9 | 1.8 | | | |
| | 22 | | 8.2 | ,/ | | | | 7.7 | 1.2 | | | 7/23 |
| • | 23, | | 7.0 | 0/ | | | | 8.1 | 1.5 | | 9 | 1 |
| | 24 | | 8.0 | 9 | | <u> </u> | | 2.7 | .4 | <u> </u> | / | |
| | 25 | | 8.0 | - O >. | | | | 7.5 | 3,0 | | | 1 |
| | 26 | | 8.0 | ./ | ļ | | | 1.8 | ,2 | 1 | | |
| • • • • • • • • • • • • • • • • • • • | 27 | 3,3 | 7.9 | | ļ. | | | 7,6 | 2.2 | | | |
| | 28 | | 1 , | 0 | - | <u> </u> | | 6.6 | , ~_ | 2/ | 0 | <u> </u> |
| | 29 | | | | | 1 | <u> </u> | | | | | <u> </u> |
| • | 30 | | | | | ļ | <u> </u> | , | | <u> </u> | | |
| _ | 31 | | 1.70 | 1 . 9 | | | | 1/2 | -, . | | ļ.: | |

| | | | EFFL | UENT | DI | TCHE | S | | | MONU | n 01: | |
|---|-----------|-------------|--|-------------------------|--|-----------|-------------|---------------------------------------|--|--------------|--------------|--|
| • | | | | | | 3:25 | 7 06 | 1/11.3 | 6.2 | <u></u> | 11/ | |
| | | | 143.) | (2.01 | 12 at | 3 | | <i>ゾ</i> // | | 1 | 13// | 12, |
| 49-383 | | | | | 41 | - | | | Sattled | rest | - | |
| | Data | (| (Zill) | Solids ${}^{\setminus}$ | P205 (| 1300) | P205 | | Solids | P2/9 | (103) | P ₂ O ₅ |
| — | Date 1 | | _DH_ | Vol.% | ppm / | GPM | TPD | рН | Vol.% | ppm | GPM | / TPD |
| <u>· </u> | | | | | | | | | | | | · |
| i | 3 | | | | 5 | /4:d .3 | <./ | | | 6: | 732 | .3 |
| | | | | | | // | | · · · · · · · · · · · · · · · · · · · | | 9 | / | |
| | 4 | | <i>i</i> | | <u></u> | 70 .1 | <.1 | |) | 12. | R. | 7 |
| | 5 | | 7 | | 310 | · · · · · | 1.9 | | | 4/0 | 997 | |
| • | 6 | | - | , | 80. | 1050 | 1.7 | <u> </u> | | | | 2, = |
| | 8 | | 1. 1 | 7 | | 1457 | | 3 | | 3 3 | | |
| | | | | - | 1.3 | 920 | | -1 | | | 1937 | <u> </u> |
| | 9 | | 1 .1 | r | 231 | 1178 | 1.6 | | ارستو , | 1-2 | 1178 | |
| , · | 11 | | | | <u>ニ</u> | 7 30 | <./ | / : | | 121 | | Z-/_ |
| <u></u> | | | 2 | - | (| 1/20 | <u> </u> | Carlo | . / <u>.</u> / | | | 7 |
| | 12 | | 81L | | | 1112 | <. | | 1 . | | 1739 | 1,2 |
| • - | 13 | | <u> </u> | <i>i</i> . | 6 7 /3 | 1. | | | | /) | 1//34 | $\leq l$ |
| | | | 7.3 | ' (| 50 | | 8 | 3.7 | 1 ./ 3 | / | / | <u> </u> |
| | 15 16 | ' | (é.d) | | . , | 111 112 | . , , | | - | | -, / | . 1/. |
| • * | | | 1 | <u> </u> | /- | 1:10 | 2.1 | 6) | 71 | **1 | 701 | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ |
| | 17 | | 7 | 7, | 1) - | 11012 | . 2 | 1 1 | <u>, · ;</u> | 111 | 930/ | 3 |
| | 18 | | 7 3 | | | 1423 | 2 | | | 4/ | 7 3(3) | 1/ |
| | 19 | | 6.6 | <u> </u> | - 9 | 1701 | 1,3 | | | // " | | 1.7 |
| | 20 | | (/ | | 3) | 1 | | | | /13 | 10174 | 1 . 1/ |
| <u> </u> | | | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | Tr | = 1 | 11/8 | .3 | 79 | <u> </u> | | 730 | -1 |
| | 22 | | 82 | -44 | | 11/0 | | 1 | 2 | | 1050 | 3 |
| • | 23 | | 7.0 | ,11 | 6: | |) | 19 | ,64 | 3 t | | 1 2 |
| | 24 | | <u> </u> | (| 7 | 11/10 | <u> </u> | -/-/- | , | | , V | 4. |
| | - 25 | | <u> </u> | | | 1170 | <.1 | | . 20 | 14 | | i |
| • | 26 | | <u> ` </u> | , | 6 | 1450 | <u> </u> | | ,) 2 | ., | | 6 |
| - | 27 | | , | ļ | 8 | (1) | | <u> </u> | . 12 | 0.70 | 1300. | i ' ' |
| | 28 | | (. ' | 0 | 5:0 | 1450 | <u> </u> | | | (1:/2) | 1307. | <u> </u> |
| | 29 | | 7 8 | i | | | | 1.5 | 1 // > - | 1 | 1 / 1 / | |
| | 30 | | 7.8 | 0 | 8 | 1420 | | 6:5 | 0.30 | 727 | 1173 | ن د |
| | 31 | l | P. L | i. () | | 14151 | 1 (.) | 6 8 | 7(| i (Ca | (1430) | 1.6 |

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| | | | C-443-3 | | | | 0-117-3 | | | | |
|---|------|-----|----------------------------|-------------------------------|-------------|-------------------------------|-------------|----------------------------|--------------------------------------|-------------|--------------------------------------|
| • | Date | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | H | Settled Solids Vol.% | P ₂ O ₅ ppm | GPM | P ₂ O ₅ TPD |
| ; | 1 | 2.2 | Tr. | 2520 | 2400 | 36.3 | 5.4 | .60 | 330_ | 1450 | 2.9 |
| <u> </u> | 2 | 3.4 | Tr. | 315 | 1750 | 3.3 | 7.9 | .03 | 300 | 1750 | 3.2 |
| | 3 | 7.1 | .10 | 80 | 1750 | .8 | | | | | |
| | 4 | 4.7 | .01 | 204 | 2700 | 3.3 | 2.8 | .35 | 1600 | 1450 | grab sampl |
| | 5 | 7.4 | Tr. | 46 | 2200 | .6 | 6.4 | .10 | 173 | 1450 | 1.5 |
| 3 | 6 | 7.2 | Tr. | 37 | 2700 | 150 | 5.9 | 35 | 268 | 1450 | 2.3 |
| • | 7 | 7.4 | Tr. | 28 | 2400 | .4 | 7.9 | .50 | 72 | 2050 | .9_ |
| | 8 | 7.7 | Tr. | 11 | 2700 | .2 | 6.7 | .05 | 123 | 1170 | .9_ |
| | 9 | 7.0 | .01 | 60 | 1600 | .6_ | 4.5 | .04 | 390 | 1450 | 3.4 |
| • | 10 | 7.6 | Tr. | 11 | 1300 | <u>.ı</u> | <u>6.</u> 9 | .01 | 325 | 1170 | 2.3 |
| <u>:</u> | 11 | 7.8 | Tr | 0 | 2700 | 0 | 6.1 | .07 | 370 | 1750 | 3.9 |
| *** | 12 | 8.0 | Tr. | 15 | 2700 | 0.2 | 5.8 | .10 | 376 | 1600 | 3.6 |
| • 1 | 13 | 7.8 | Tr. | 3 | 2700 | (0.1 | 6.2 | .15 | 123 | 1600 | 1.2 |
| `` , , . | 14 | 7.5 | .16_ | 20 | 2400_ | ×-3 | 4.5 | .10 | 336 | 1450_ | 2.9 |
| | 15 | 7.6 | Tr. | 17. | 2700 | 3 | _5.0 | 10 | 285 | 1170_ | 2.0 |
| <u>β</u> | 16 | | | | <u> </u> | | ļ | | | | <u> </u> |
| • · · · · · · · · · · · · · · · · · · · | 17 | 7.7 | .02 | 50 | 1750 | •5 | 6.6 | .03 | 230 | 1170 | 1.6 |
| | 18 | 7.4 | .01 | 39 | 2700 | .6 | 6.8 | .20 | 250 | 1450 | 2.2 |
| | 19 | 7.9 | .01 | 11 | 2400 | .2 | 2.7 | .07 | 480 | 1300 | 3.7 |
| • | 20 | 7.9 | Tr. | 5 | 2200 | < .1 | 3.6 | .10 | 420 | 1300 | 3.3 |
| | 21 | 7.9 | Tr. | 5 | 2400 | ₹.1 | 3.5 | .20 | 860 | 1450 | 2.5 |
| | 22 | 8.1 | Tr. | 8 | 2550 | | 6.3 | 45 | 570 | 1450 | 5.0 |
| • | 23. | 8.2 | Tr. | 50 | 1300 | .4 | 7.4 | .01 | 200 | 1050 | 1.3 |
| | 24 | 8.1 | Tr. | 80 | 1300 | .6 | 6.7 | .01 | 330 | 1300 | 2.6 |
| | 25 | 8.0 | Tr. | 7 | 1900 | .1 | 4.0 | .20 | 860 | 1300 | 6.7 |
| | 26 | 8.2 | Tr. | 8 | 2050 | .1 | 6.1 | .15 | 252 | 1050 | 1.6 |
| - | 27 | 7.5 | | 3 | 1300 | 4. 1 | 6.2 | | 230 | 1050 | 1.4 |
| | 28 | | | | ļ | | | | <u> </u> | | |
| | 29 | 7.4 | Tr. | 11 | 2200 | .1 | 6.2 | Tr. | 480 | 1300 | 3.7 |
| • | 30 | ļ | · | | | | | ļ | ļ | <u></u> | |
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| • | | | Settled | Р О | • | 7 F | | Settled | D O | | · 子· |
| • [| Date | ? Hor | Solids Vol.% | P ₂ O ₅ | GPM 4 | P ₂ O ₂ | На | Solids Vol.% | P ₂ O ₅ | GPM 5/2 | P ₂ 0 ₅ |
| | 1 | | 701.3 | | Ì | \ | | | | ļ |) ' |
| · · · | | 1,4 | | <i>//</i> | 2400 | 7176.2 | · ′ | 6.3 | 8 | 1450 | 77.1 |
| | 2 | 3.4 | 1 | | 7: | - | 7, 9 | . 3 | 9 | 1750 | - |
| • | 3 | 7./_ | ن ع | _9 | | | · | | | —— <u>)</u> | |
| - | <u></u> | 4.7 | | 12 | 27:31 | | 2,8 | 5.3 | 8 | 1455 | |
| <u> </u> | 5 | 124 | | 134 | | | <u> </u> | 1,0 | , , | | \ |
| <u> </u> | 6 | 7.2 | سمبد | <u> </u> | | | 5,0 | | ~ | 7 5 5 | |
| · • • • • • • • • • • • • • • • • • • • | 7 | - | T | | | | -, .; | 6.0 | | <u> </u> | <i>:</i> |
| | 8 | 7,7 | | 12 | 27 | 7/6.0 | 4.7 | <u> </u> | .7_ | 1170 | ············· |
| | 9 | 7,0 | ./ | 75 | 112 | : : | 4,5 | - 4 | 2 | 100 | 196 |
| • | 10 | 7,6 | I | 72 | 1 3:5 | | 6.9 | | | 4 | |
| | וו | 7,8 | 1 | 12 | 2722 | / | 6.1. | .7 | 9 | 175 - | ン |
| . | 12 | 8,0 | T | 12 | 2700 | | 5.8 | 1,0 | 83 | 16.00 | |
| •/ | 13 | 7.8 | T. | 12 | 2760 | / | 6.2 | 1.5 | 83 | 1600 | : |
| \\\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\. | 14 | 7,5 | 1.6 | 11 | 2400 | , N | 4.5 | 1.0 | 8 | 145 0 | |
| | 15 | 7.6 | 1 | 12 | 2700 | ^ //:3· | 5.0 | 1.0. | 7 | 1170 | 77: |
| | 16 | * | | _ | - | | * | | | _ | : |
| | 17 | 7,7 | . 2 | 9 | 1750- | | 6,6 | . 3 | 7_ | 1170 | |
| | 18 | 7.4 | 1 | 13 1 | 2700 | | 6.8 | 2.0 | 8 | 1450 | |
| | 19 | 7.9 | . 1 | 11 | 2400 | | 2,7 | , 7 | 池 | 1300 | |
| ● —F?——— | 20 | 7, 9 | T | 10立 | 1225° | | 3,6 | 1.0 | 7 | ,500 | |
| | 21 | 7,9 | I | 11 | 2400 | | 3,5 | 1.0 | 8 | 1450 | |
| | 22 | 8.1 | 1 | 115 | 2550 | 7.0.1 | 6,3 | 4,5 | 8 | 1450 | 15 65 |
| • • | 23 | 8.2 | 1 | 7:1 | 130 6 | | 7.4 | ./. | | 1050 | <u> </u> |
| | 24 | 8.1 | 1 | - フェ | 1300 | <i>/</i> | 6.7 | ./_ | 75 | 1300 | |
| S | 25 | 8,0 | 1 | 95 | 1950 | | 4,0 | 0,0 | 73 | 1300 | |
| | 26 | 8.2 | 1 | 10- | ز ، وئے | | 6,1 | 1,5 | 6至 | 1050 | |
| | 27 | 7.5 | .1 | 94 | 130 - | | : : | . 3 | 1-1- | | <u> </u> |
| | 28 | | | , | | <u> </u> | | ļ | | <u> </u> | <u> </u> |
| | 29 | 7.4 | 7 | 103 | 2200 | | 62 | ーナ | 72 | 1300 | /// |
| • | 30 | <u> </u> | | | | <u> </u> | , | | | <u> </u> | <u> </u> |
| _ | 170. | 841101 | _ | | 1/ | | GRAG. | SAMPLE | | ا ا | <u>Z</u> |

| | | | EFFI | UENT | DI | тсне | S | | | Mont | n oï: | |
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| • | | | 10 | | | | 11.), = | 1415,3 | 3.62 | | uri | |
| FINE SEE | | İ | 1/1/ | $\sum_{\mathbf{E}} \langle \mathbf{v} \rangle_{\mathbf{E}}^{2}$ | ast | 25,770 | () () () () () () () () () () | | | 1 22 s t | 3/1/1 | 71.5 |
| 42-393 | | j | | Settled | 177 | (1) (| 1.4 | | Settled | X | | 2.9 |
| | Date | . (| | Solids Vol.% | P ₂ 0 ₅ | GPM (| P ₂ O ₅ TPD | (S, &) | Solids Vol.% | P205 (| GPM | P ₂ 0 ₅ |
| | 1 | ! | 22 | 101.7 | 2520 | 2.UW | 39.3 | pn / | | ppm > | | 2.9 |
| | 2 | | 301 | 7 | 3/5 | 1: 1 | 2 0 | -, 9 | ./ / | 30) | /) | 3, 2. |
| | 3 | | 7.1 | 10 | 80 | 172 | ,8 | <i>-</i> // | | | | , |
| | 4 | | 1/2 | 0/ | 2011 | <i>X</i> | 3.3 | | | 7 tyn) | | grab |
| . | 5 | | 57 | 7, | 1 | | . / | / / | 12 | | 1 | 1.5 |
| | 6 | | | 1. | 27 | 1 | .6 | | , 2, 7 | 300 | · V. | - · |
| • | 7 | | - :/ | | | /- | c | | | 72 | -100 | .9 |
| | 8 | | | 17. | 11 | (1) | .> | 6.1 | | 123 | 11-1 | 9 |
| | 9 | | | | 60 | 1,/ | 4 | <u> </u> | | (C) | , 4 | 3.0 |
| • | 10 | | 7. (2) | | | ./ | | <u> </u> | 12 | | 17/1 | 2.3 |
| | 11 | | 2 | 17 | | | () | . / | .07 | | 1/1 | 3.9 |
| <u> </u> | 12 | | 2 A | | 15 | | 2 | | .) | 3-1/2 | | 3 3 |
| T | 13 | | 78 | 17. | | . () | <0.1` | 1.2 | 115 | ر در | 1:12 | 1. > |
| * * * * | 14 | | 5 | ./10 | 5) | 2-12/ | A 5.5 | 1/. | .10 | 7.96 | 1:/4 | 100 1 |
| <u>.</u> | 15 | | 7 | 1 | 11 | - | | | | | | 12.1 |
| £.: | 16 | | | | | | | - ··· | | | | |
| • | 17 | | | | 5) | / | ٠, ٥ | | | | i. | 1/2 |
| | 18 | ļ | 711 | . 77 | | 250 | | 6.0 | .50 | 2 1 | 1/21 | |
| | 19 | | | 0/ | 1/ | No. | _2_ | | | (/) | i v | 3.5 |
| • | 20 | | 7.7 | 7. | <u></u> | 7 2/2 | <./ | 1.1. | 11: | (/3) | / | 13: |
| | 21 | , | 2.9 | | \ | 1/0 | <u> </u> | 3-2-3- | .20 | (· ·) | 1/ | 7.5 |
| _ | 22 | ! | <i>i f</i> | ļ · | | | / | | | 1 | / V \ | 5.0 |
| | 23. | [| . 2 | <u> </u> | | 1 0 | | | | | 11/ | 1/3 |
| - | 24 | <u> </u> | : | | | | 1 | <u> </u> | | | | 2.6 |
| | 25 | 1 | 1 | | | <u> </u> | | 1. | | 1 | J. 16 V | 164 |
| | 26 | ! | 1/2/2 | <u> </u> | 8- | | | | | 3 52- | | 1.6 |
| <u> </u> | 27 | <u></u> | | | 3_ | | <_L | . · · · · | | 330 | | 114 |
| | 28 | 2 | | | | <u> </u> | <u> </u> | | <u> </u> | ļ | | |
| <u> </u> | 29 | <u> </u> | 1.4 | 1// | 1/_ | 1-260 | | | 17. | 420 | 1386 | 3.7 |
| • | 30 | | i · | | ļ | | | . | · | · | ļ | 2.9 |
| | 31 | ! | į | | <u> </u> | <u> </u> | | | ! | <u>!</u> | <u> </u> | |

May, 1967

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| : • [] | Date | | Settled Solids Vol.% | P ₂ O ₅ | GPM | P ₂ O ₅ | | Settled Solids Vol.% | P2 ⁰ 5 | GPM | P ₂ O ₅ |
| | ı | J | | | | 0.9 | | Ì | | | |
| | | 7.1 | Tr. | 720 | 2050 | 0.4 | 2.6 | .6 | 1600 | 1600 | 15. |
| | 2 | 7.3 | Tr. | 25 ø | 2400 | 3.6 | 2.3 | Tr. | _3760 | _1600_ | 36.: |
| • | 3 | 7.3 | Tr. | 17 | 2400 | .2 | 2.5 | .10 | 2600 | 1450 | 22. |
| | 14 | 7-3 | Tr. | 23 | 2550_ | -4 | 5.3 | 1.5 | 280 | 1300 | 2. |
| | 5 | 7.1 | 01 | 80 | 2050 | 1.0 | 6.1 | 3.1 | 180 | 1600 | 1. |
| | 6 | 7.3 | .01 | _33 | 2050 | .4 | 6.5 | .01_ | 115 | _1300 | <u>.</u> |
| | 7 | 7.3 | .01 | 25 | 2550 | .4 | 4.7 | .08 | 300 | 1600 | 2. |
| | 8 | 7.3 | Tr. | 8 | 2400 | .1 | 6.2 | .03 | 83 | 1450 | <u>•</u> |
| { | 9 | 7.1 | Tr. | 37 | 2700 | .6 | _5.4 | .06 | 23 | 1600_ | <u>.</u> |
| • | 10 | 7.6_ | Tr | 7 | 2700 | .1 | _5.6 | 2.5 | 280 | 1450 | 2. |
| } | 11 | 7.7 | Tr. | 25 | 2400 | .4 | 7.8 | 2.0 | 53 | 1450 | • |
| | 12 | 4.7 | Tr. | 170 | 2200 | 2.2 | 2.9 | 3.1 | 1220 | 1600 | 11. |
| • 1 | 13 | 5.8 | Tr. | 170 | 2200 | 2.2 | 5.1 | 2.0 | 720 | 1170_ | |
| | 14 | 6.7 | Tr. | <u> </u> | 2550 | × .7 | 5.2 | 4.0 | 650 | 1300 | 5. |
| -{ | 15 | 7.6 | Tr. | 13 | 2550 | .2 | 3-3 | 4.0 | 890 | 1300 | 6. |
| | 16 | 7.6 | Tr. | - 17 | 2700 | •3 | 4.0 | 1.0 | 330 | 1450 | 2. |
| | 17 | 7.1 | .00 | 25 | 2700 | .4 | 6.8 | 2.5 | 75 | 1450 | • |
| | 18 | 3.5 | .02 | 276 | 3100 | 5.1 | 6.7 | 2.1 | 139 | 1450 | 1.: |
| | 19 | 5.5 | .01 | 169 | 1450 | 1.5 | 7.1 | 1.0 | 108 | 1300 | |
| • | 20 | 6.4 | Tr. | 130 | 2050 | 1.6 | 4.6 | Tr. | 230 | 1600 | 2. |
| | 21 | 6.9 | .01 | 92 | 2400 | 1.3 | 6.3 | -4 | 65 | 1600 | |
| | 22 | 7.8 | Tr. | - 0 - | 2400 | .01 | 4.0 | •3 | 260 | 1450 | 2. |
| | 23 | 7.9 | 0 | 8_ | 2200 | .1 | 3.3 | .06 | 550 | 1450 | 4. |
| | 24 | 7.9 | .01 | 11_ | 2400 | .2 | 3.4 | .10 | 550 | 1450 | 4. |
| | 25 | 7.8 | Tr. | 8 | 2550 | .1 | 6.7 | Tr. | 95 | 1600 | |
| | 26 | 6.9 | .01 | 71,71 | 1170 | .3 | 5.5 | 1.0 | 210 | 1300 | 1. |
| ▼ & | 27 | 7.1 | .01 | 86 | 2050 | 1.1 | 4.0 | .2 | 260 | 1450 | 2. |
| | 28 | 7.2 | .01 | 75 | 5,100 | 1.1 | 3.1 | -3 | 920 | 1450 | 8. |
| | 29 | <u> </u> | | | · - · · · · | <u> </u> | | | <u> </u> | | <u> </u> |
| • | 30 | 7.1 | .01 | 25 | 2400 | 0.4 | 4.1 | _4 | 350 | 1450 | 3. |
| _ | 31 | 7.8 | Tr. | 3 | 2550 | 0.1 | 3.1 | .15 | 890 | 1450 | 7. |

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| | Date | | Settled Solids Vol.% | P ₂ O ₅ | GPM | PPN:7 | | Settled Solids Vol.% | P ₂ O ₅ | GPM | PPAN. |
|---------------------------------------|----------|------------|----------------------------|-------------------------------|-------|--|--------------|----------------------------|-------------------------------|--------|--|
| i | 1 | 7./ | 1 | 10 | 2050 | | 2,6 | ٠, 6 | 81 | 1600 | |
| | 2 | 7, 3 | 1 | 11 | 1400 | | 2,3 | 1 | 8£ | 1600 | |
| | 3 ' | 7,3 | 1 | Ji | 2430 | / | 2.5 | 1.0 | 8 | 1450 | |
| | <u>1</u> | 7.3 | 1 | 113 | 2530 | 151.3 | 53 | 1,5 | 752 | 1300 | 1.4% |
| | 5 | 7./ | ./ | 10 | 2050 | - \ | 6.1 | 3.7 | 82 | 1603 | |
| | 6 | 7.3 | -/- | /2 | 2050 | <u> </u> | 6.5 | ./ | 75 | 1300 | <u> </u> |
| · . | 7 | 7.3 | ./ | 113 | 2550 | ¥ | 4,7 | .8 | 82 | 1600 | |
| | 8 | 7.3 | 1 | 7/ | 2400 | \ | 6.2 | .3 | 88 | 1450 | _ |
| | 9 | 7.1 | 1 | 12 | 2700 | | 5.4 | . 6 | 85 | 1600 | |
| | 10 | 7,6 | 1 | 12 | 2700 | | 5.6 | 2.5 | 3 | 1415 2 | |
| · · · · · · · · · · · · · · · · · · · | 11 | 7.7 | 1 | ./ | 2400 | 11,8 | 7.8 | 2,0 | 8 | 1452 | 45. |
| | 12 | 4.7 | 1 | 10% | 2200 | | 2,9 | 31/ | 8,7 | 1600 | |
| •(| 13 | 5.8 | 1. | 10% | 2200 | | 5.1 | 2,0 | | 1170 | |
| · . | 14 | 6,7. | 1 | 112 | 2007 | <u> </u> | 5.2 | 4,0 | 72 | 1300 | <u>/</u> |
| | 15 | 7,6 | 1 | 11.5 | 2550 | N N | _3, <u>3</u> | 4.2 | 72 | 1300. | |
| | 16 | 7:6 | T | 12. | 2700. | | 4,0 | 1.3 | 8 | 143 5 | <u> </u> |
| | 17 | 7.1 | 0 | /2 | 2703 | 1 | 6,8 | 615 | 8 | 145- | |
| · | 18 | 3,5 | نه ا | /3 | 3/02 | 3,0 | 6,7 | 2.1 | 8 | 145.0 | \ |
| | 19 | 5,5 | ./_ | 2 | 1950 | | 7,/ | 1,0 |) 2' | 1300 | |
| • <u> </u> | 20 | 6.4 | T | 10 | 2050 | 1 | 4,6 | 1 | 2/2 | 1600 | · <i> </i> |
| | 21 | 6.5 | | -// | 2430 | ' | 6,3 | . 4 | 82 | 1600 | γ· |
| | 55 | 7.8 | 7 | 11. | 2000 | | 4,0 | ,3 | 8 | 145 | <u> </u> |
| • | 23. | 7. 7 | 0 | 103. | 22.00 | | 3,3 | 6: - | 8 | 1450 | |
| | 24 | 7.5 | | _//_ | 24/22 | 7-2- | 3.71 | 1.0 | 8 | 145 5 | / |
| · · · · · · · · · · · · · · · · · · · | 25 | . 7, 8 | | 112 | 2550 | <u> </u> | 6.7 | 1 | 82 | 1600 | <u> </u> |
| • 1 | 26 | 4.7 | | <u> </u> Z | 11.70 | | 5.5 | 1,0 | 73 | 1300 | <u> </u> |
| - | 27 | 4,1 | ./ | 10 | 2000 | <u> </u> | 4,0 | ,2 | 8 | 1450 | |
| | 28 | 4,2 | ,/ | . // | 2455 | <u>/</u> | J. / | .3 | 8 | 1450 | / |
| | 29 | <u> </u> . | ļ | · . | | \ | | | | | |
| | 30 | 7./_ | ./_ | 11 | 2400 | 776.2 | 4./ | .4 | 8 | 1450 | 77 |
| | 31 | 1 7.9 | 1 | 111 | 25.50 | <u>Y</u> | 3.1 | 1.5 | 8 | 1450 | ! \ |

| | | EFFL | UENT | י דמי | ГСНЕ | S | | ٠ | | h or: |
|---|--------|-------|---------|-------------------------------|--------|-------------------------------|---------------------------------------|-------------------|---------|------------|
| | | | | | | Ē | | • | | no |
| Figure 1 to 1 to 1 to 1 to 1 to 1 to 1 to 1 t | | 271.7 | L.01) | \sim | 70270 | (0) | 111/2 | 31.5 | 1226 | 13670 |
| 42-383 | | | Settled | (57) | 15 | - 0 - | | Satta ad | 1 e/s t | 3.1 |
| | Date | (4,0 | Solids | P ₂ 0 ₅ | CTA | P ₂ 0 ₅ | (40 //6 | Séttled Splids | P205 | P205 |
| | Date 1 | | Vol.% | ppm | GPM_ | TPD | pH_ | / | /600 | GPM TPD |
| 1 | | 2.3 | 1. | 721 | 2410 | 13.6 | ر کی رائی ا این کی این ا | , (c. | 3760 | 1610 36,6 |
| - | 2 | 7.7 | 17 | 1-1 | | ₩ | 2,5 | 1: | 2600 | M. 22.1 |
| | 3 4 | 7.3 | Ta | -/ / - _よ う | 245 | 7 | , , , , , , , , , , , , , , , , , , , | 1,5 | フタン | 7 33 |
| | 5 | 7.1 | 01 | 80 | 2050 | 1.1) | , | 3.1. | 180 | |
| | 6 | 7.3 | · D / | 3 3 | 2010 | | 6.1 | . <i>D1</i> | 1/3 | 1300 .9 |
| • | 7 | 7.3 | · D1 | 25 | 1-2110 | . 4 | | .08 | 300 | |
| | 8 | 7.3 | / / / | - 3 | 2400 | | 4.7 | .o3 | 83. | 1450 7 |
| | 9 | 7.1 | 1/1 | | 2700 | . 6 | 5.4 | .96 | 23 | 1600 . 2 |
| | 10 | 7.6 | 1 | <u> </u> | 2700 | | 5. F | 7.5 | 270 | 2.4 |
| | 11 | 7. 7 | | 25 | 24 | | 7.8 | ن ج | 13 | 14.11.15 |
| | 12 | 4.7 | 1. | 170 | 2 | 2.2 | 2.9 | 7. 1 | 1220 | 1,-00 11.2 |
| | 13 | (0 | ,\ | 170 | 12.0 | 2.2 | | 2.0 | 720 | 1170 5.1 |
| • · · · · · · · · · · · · · · · · · · · | 14 | 6.7 | 1 | 44 | 2010 | | ゴレ | - , | 650 | |
| | 15 | 1.6 | 2 | / 3 | 2110 | 7 | | 4.0 | 890 | 1:0 6.9 |
| L | 16 | 7.6 | 1 | 17 | 2700 | .3 | 4.0 | 1.0 | 330 | 1450 2. |
| • | 17 | 2.1 | .0 | 25 | 2700 | Į . | 6.8 | 2.5 | 7 | 1450 . |
| | 18 | 3.5 | .07. | 276 | 3100 | 5.1 | 6.7 | 2.1 | 139 | 1450 1.2 |
| | 19 | 5.5 | .01 | 169 | 1450 | 1.5 | 7.1 | 1.0 | 108 | 1300 .8 |
| • | 20 | 6,4 | # | 130 | 2050 | . 1 | 4.6 | 21 | 230 | 16002.2 |
| | 21 | 6.9 | .0/ | ÍV | 2:00 | <i>j</i> . 3 | <u>6.3</u> | . 4 | 65 | 1600 .k |
| | 22 | 7.8 | In | -0- | 2600 | -0- | 40 | , 3 | 200 | 1450 2.3 |
| • | 23. | 7.9 | 0 | 8 | 2200 | -1 | <u>3. 3</u> | 06. | 550 | 1450 41 |
| · | 24 | 1.9 | .01 | // | 2400 | , 2 | <u> </u> | .10 | 550 | 1750 46 |
| 3 | 25 | 7.8 | 1 | 8 | 2550 | . 1. | h. 1 | 1 | 25 | 1310 1 |
| | 26 | 6.9 | .01 | 1/1/ | 1170 | .3 | <u>ک،ک</u> | 1.0 | 27 | 1300 1.6 |
| | 27 | 7.1 | , 01 | | 2050 | 1.1 | 4,0 | .2 | 210 | 1450 = |
| | 28 | 7.2 | .01 | 1/2 | 2400 | 1./ | <u> 3.1</u> | ,3 | 55 | 12150 8.1 |
| | 29 | | | | | · | | | | |
| | 30 | 1.7.1 | . 0 / | 25 | 2(1) | 6.4 | <u>41</u> | 4 | 350 | 1450 3.0 |
| - . | 31 | 7,8 | Tr | <u>ب</u> ب | JITO | 1 1 | 3.1 | ,/3 | 1560 | 1410 27 |

April 1967

| 42-333 | | _ | | E | ast | 42. | = 1.8 | | | lest | <u> </u> | 10. |
|---------------------------------------|------|------|-----|----------------------------|-------------------------------|------------|-------------------------------|-----|---------------------|-------------------|-------------------------|-------------------------------|
| • | Date | | | Settled Solids Vol.% | P ₂ O ₅ | - ♂ GPM | P ₂ O ₅ | На | Settled Solids Vol. | P2 ⁰ 5 | GPM | P ₂ O ₅ |
| | 1 | | 2.8 | Tr | 530 | 2400 | 7.5 | 6.5 | 1.80 | 330 | 1750 | 3.0 |
| | 2 | | 2.3 | .01 | 600 | 2550 | 9.0 | 4.6 | 1.95 | 1120 | 1600 | 10.5 |
| | 3 | | 5.9 | .01 | 57 | 2550 | 1.0 | 7.2 | 1.50 | 204 | 1600 | 2.0 |
| | 4 | | 3.6 | .61 | 173 | 3300 | 3.0 | 4.5 | 1.60 | 1980 | 1750 | 20.5 |
| · . | 5 | | 3.2 | .ol | 198 | 3100 | 3.5 | 3.8 | .55 | 800 | 1170 | 5.5 |
| · · · · · · · · · · · · · · · · · · · | 6 | | 4.0 | Tr. | 55 | 2700 | 1.0 | 2.9 | .45 | 1270 | 1300 | 9.5 |
| • | 7 | | 3.6 | Tr. | .420 | 2050 | 5.0 | 4.6 | •35 | 670 | 1170 | 4.5 |
| | 8 | | | | | | | , | | | | |
| | 9 | | 6.1 | .03 | 170 | 2400 | 2.5 | 5.3 | .20 | 550 | 1450_ | 5.0 |
| • | 10 | | 7.3 | Tr. | 11 | 2400 | 0.2 | 6.4 | .90 | 239 | 1600 | 2.0 |
| t • | 11 | | 6.1 | .01 | 127 | 2400 | 2.0 | 3.9 | .03 | 720 | 1450 | 6.0 |
| h.e | 12 | | 7.1 | Tr. | 23 | 2400 | .3 | 3.6 | .15 | 600 | <u>1¹450</u> | 5.0 |
| | 13 | | 6.7 | Tr: | 27 | 2550 | . 4. | 5.5 | 2.01 | 620 | 1600 | 6.0 |
| | 14 | | 6.6 | Tr. | 46 | 2050 | 16 | 2.7 | .20 | 1690 | 1450 | 15.C |
| | 15 | | 7.1 | .01 | 75 | 2050 | .9 | 4.5 | .35 | 830 | 1450 | 7.2 |
| | 16 | | 3.7 | Tr. | 135_ | 2400 | 2.0 | 5.2 | .51 | 500 | 1600 | 3.4 |
| 6 6 9 9 9 9 9 9 9 9 9 9 | 17 | | 7.4 | Tr. | 17 | 2550 | 3 | 4.4 | .15 | 650 | 1750 | 6.8 |
| · | 18 | | | | | | | | | | | <u> </u> |
| | 19 | | 3.4 | Tr. | 370 | 2400 | 5.3 | 3.3 | .23 | 1230 | 1600 | <u>11.8</u> |
| • | 20 | | 6.9 | Tr. | 30 | 2400 | .4 | 3.8 | .20 | 570 | 1450 | 5.C |
| | 21 | | 7.5 | .01 | 27 | 2050 | •3 | 5.1 | .85 | 1050 | 1300 | 8.2 |
| | 22 | | 6.8 | Tr. | 37 | 2200 | .5 | 4.0 | 2.0 | 600 | 1300 | 4.7 |
| | 23. | | 6.9 | Tr. | 23 | 2200 | .3 | 6.7 | .25 | 750 | 1300 | 5.ξ |
| · | 24 | | 7.4 | Tr. | 18 | 2400 | .3 | 2.8 | .20 | 1625 | 1450 | 14.1 |
| | 25 | | 7.1 | Tr. | 27 | 2200 | .4 | 3.2 | .10 | 750 | 1300 | 5.8 |
| | 26 | | 7.3 | Tr. | 25 | 2200 | •3 | 3.6 | Tr. | 460 | 1300 | 3.6 |
| | 27 | | 7.3 | Tr. | 15 | 2400 | .2 | 4.2 | .15 | 530 | 1450 | 4.6 |
| | 28 | | 4.1 | Tr. | 130 | 1750 | 1.4 | 2.9 | .03 | 1150 | 1450 | 10.0 |
| | 29 | | 7.1 | .01 | _37- | 1900 | .4 | 6.1 | .01 | 270 | 1450 | 2.3 |
| • | 30 | | 7.0 | Tr. | 53 | 2050 | 7_ | 5.9 | .15 | 37 | 1170 | 3 |
| | 31 | | | | İ | | ! ! | ! | | | | |

APRIL 1967

19 11.

West East P202 ppm PPIII Settled Settled P205 Solids Solids √ppm TPD TPD Date Vol.% Vol.% **GPM** pН **GPM** pН 11 " 175 O 1 2,8 1400 82 1600 2 25 : -19.50 8± 3 2550 1600 15,0 13: G 4 3300 3,1 3165 J.8 5 13 1170 <u>کے ج</u> 12 2700 6 1300 2050 150 7 10 1170 8 9 3 8 3 <u>-7 6 3</u> 11 4 500 8 % 10 7,3 // 6,4 9,5 1600 1400 3, 9 8 11 2400 450 3.6 8 12 1450 // 2400 87.1 13 1. 23 2050 515 ×37.2 14 6,6 25.50 10 2,7 15 7,1 1500 10 16 3.7 5.1 1622 9" 25:5 17 1750 4,4 18 8Í 19 3,4 3,3 1.3 1437 1600 6,9 3, 2 20 <u> 2500</u> 1450 7, 5 55.9 21 130 -2000 5,1 . د دنۍ 22 12:00 25. 4,0 Z £ 4.7 23. 1300 1200 2.5 2,8 24 7.4 11. 24:0 1455 10= 25 3,2 1300 7,1 ت ، *ایک* 10 3 26 7,3 3,6 1300 2300 7.3 21.8 27 7 1452 1450 28 4.1 9: 29 1450 2050 1170-30 ·

west Plant

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| | | | EFFI | UENI | DI | тсне | S | | | Monu | 1 01: | |
|-------------|-----------|---|---------|---------|-------------------------------|------------|---------------|------------------|----------|-----------|--|-------------|
| • | | | 100 | | 3456 | | = -490 | 127.2 | 14.37 | <u>()</u> | <u>, 1/</u> | |
| | | | | | ast | 4.700 | 11.5 | | | lest | 101110 | 169.5 |
| 42-383 | | | | Settled | () | (23/2) | 718 | (43) | Settled | | 1452 | TIX X |
| • 1. | Date | | | Solids | P ₂ 0 ₅ | - am | TPD | | Solids | P205/ | | P205 TPD |
| | Date 1 | | pH - | Vol.% | ppm 5/20 | GPM | TPD | рН | Vol.%_ | mqq | <u>GPM</u> / ^) | 7 <u>PD</u> |
| · · | 2 | <u> </u> | 2,3 | | | | 7 | () | 1.95 | 1120 | <u>/ </u> | 10.5 |
| | 3 | | 5.7 | .01 | 5/ | | / | | | 571/ | <u></u> |)_ |
| • | 4 | | | .01 | 173 | 3-0 | -(| - 1-2 | 1.60 | 1951 | | 20,3 |
| —. ——— | 5 | | 7) | | 19% | 27:1 | : | | | 81) | 1/20 | 5 1 |
| | 6 | | 1/2 | 7. | 55 | 2 | 1 | 2.9 | د/). | | | |
| • . | 7 | | 1: 6 | 7. | 1/2 | G(3) | - | \ <u>/</u> | | 670 | //20_ | 4/. |
| | 8 | | 2 | 1. | 1-420 | 663 | | | | 8 7 5 | <u> </u> | |
| | 9 | | // | 1.17 | 1-50 | : (/* .) | 5.5 | <u>, ; </u> | 0,20 | 5: 1 | 1413 | 5 |
| | 10 | | - > | 7 | 1: | - 1/- 1 | | 64 | 6. | | 1317 | |
| | 11 | | , | | 12- | | 2 | : / | .// 3 | 720 | : 1/2 : | 6. |
| L | 12 | | F. , | 7, | 23 | 24 | .3 | j. 6 | | 600 |) | 5 |
| | 13 | | 6-1 | 76 | | 1-71 | 4 | | 2,01 | 6211 | 75.77 | 1/2 |
| i., | 14 | | 6.14 | 7 | 46 | ,) . | 196 | | 120 | 1600 | $\overline{f_{ij}}$. | 15 |
| | 15 | | 7/ | , , | 75 | | ,7. | 1/ 1 | | 120 | , . ; ; . <u> </u> | 7.2 |
| | 16 | | 2.1 | | 135 | 240 | 2.0 | ٠ ـ ـ | 1.31 | (i) | 1442 | 1/. |
| | 17 | | 7,4 | 7 . | 17. | 0 (| 13 | 4.1 | ./5 | 620 | <u> /24)</u> | 1 |
| 6. * | 18 | , | | | | | | | | | | |
| | 19 | | 3.4 | 7 7 . | 570 | <u>-</u>) | | 2.3 | 0,23 | 1:31 | 1411 | |
| • | 20 | | 1.7 | | 30 | , , , | | | 2.0 | 520 | ((1) | 5.0 |
| | 21 | · ——— | |) | , | 1200 | 3 | : / | 1 | 1. | 1- | 8.2 |
| 1 2 | 22 | | 1./ | - | | 1200 | .5 | :/ ** | | 7, 2 | 1,. | 4.7 |
| • | 23 | | 14.9 | 1 | | (; ;) | ,3 | 400 | -> | | | 5.8 |
| - | 24 | · | 1711 | 7. | 18 | 71/ | | | ,20 | 1625 | | 14.1 |
| | 25 | | 7.1 | 12. | - | (2711) | 1 | <u>))) :</u> | 10 | 50 | / <i>y</i> / | 58 |
| | 26 | | 123 | 1 | 35 | <u> </u> | 1.3 | 3 | ļ , | 4/, 1) | | 3,6 |
| | 27 | · | 7.3 | 1.5, | 15 | 15.4 | <u> </u> | 11 2 | <u> </u> | | <u> </u> | 4.6 |
| | 28 | | 1.1 | 7, | 130 | 1750 | 1.4, | | | 1/2 | <u> </u> | 10, |
| | 29 | · · · · - · · · · · · · · · · · · · · · · | 7.1 | 01 | | 11719 | (/ | 10.1. | | 1 - 20 | 1/2/ | 2.3 |
| • | 30 | · | / | Ti | <u></u> | | 1.7 | <u> </u> | 1.15 | 37 | 1170 | <u> </u> |
| | 31 | | • | 1 | | | | 1 | ļ | . | | ! |

March 1967

| ı | 42-383 | | | E | ast | <u> </u> | 6.7 | | V | lest | 6-21 | 7.6 |
|----|--|------|------------|-------------------|-------------------------------|----------|-------------------------------|---------------|-------------------|-------------------------------|--------|-------------------------------|
| | : 80) | | | Settled Solids | P ₂ 0 ₅ | - 6 | P ₂ 0 ₅ | | Settled Solids | P ₂ 0 ₅ | U | P ₂ 0 ₅ |
| | | Date | p <u>H</u> | Vol.% | ppm | GPM | TPD | <u>pH</u> | Vol.% | ppm | GPM | _TPD_ |
| - | | 1 | 2.4 | Tr. | 390 | 2950 | 6.5 | 2.9 | .18 | 780 | 1050 | 5_ |
| - | | 2 | 2.4 | Tr. | 295 | 3300 | 5.5 | 3.7 | .20 | 610 | 1450 | 5 |
| •- | f | 3 | 2.1 | ļ | 460 | 3300 | 9.0 | 3.1 | | 530 | 1300 | 4 |
| - | | 4 | 2.3 | | 460 | 3100 | 8.0 | 5.0 | | 370 | 1170 | 2. |
| | , : | 5 | 2.4_ | Tr. | 325 | 3100 | 6.0 | _3.3 | 20 | 420 | 1450 | 3. |
| | J | 6 | 2.6 | Tr. | 268 | 3500 | 5.0 | 2.5 | .07 | 750 | 1600 | 7 |
| | · · · · · · · · · · · · · · · · · · · | 7 | 2.5 | Tr. | 300 | 2700 | 5.0 | 2.0 | .07 | 720 | 1600 | 7 |
| | | 8 | 2.7 | Tr. | 250 | 2750 | 4.0 | 3.0 | .10 | 600 | 1600 | 6.6 |
| _ | -i | 9 | 3.0 | Tr. | 165 | 2400 | 2.0 | 4.8 | .10 | 210 | 1600 | 2.0 |
| • | <u> </u> | 10 | 2.6 | Tr. | 330 | 2750 | 5.5 | 6.1 | .07 | 200 | 1300 | 1.5 |
| _ | · | 11 | 2.3 | Tr. | 370 | 2550 | 5.0 | <u>.</u> | | | | |
| | <u>ia</u> | 12 | 2.5 | Tr. | 370 | 3500 | 7.5 | 5.1 | •35 | 750 | . 1450 | 6.5 |
| • | r : | 13 | 3.0 | Tr. | 204 | 3300 | 4.0 | 6.8 | .20 | 75 | 1450 | .5 |
| | . | 14 | 2.9 | Tr. | 350 | 2700 | 5.5 | | | | | <u> </u> |
| | I | 15 | 2.7 | Tr. | 440 | 3100 | 8.0 | 2.4 | .05 | 1930 | 1600 | 18.c |
| | £ : | 1.6 | 2.5 | Tr. | 460 | 3300 | 9.0 | 2.5 | .08 | 1350 | 1450 | 12.€ |
| •_ | £ | 17 | 2.1 | Tr! | 670 | 3300 | 13.0 | 3.2 | .01 | 830 | 1300 | 6.5 |
| | <u> </u> | 18 | 2.1 | Tr. | 480 | 2400 | 7.0 | | | | | |
| _ | | 19 | 2.3 | Tr. | 460 | 3100 | 8.5 | | | | | <u> </u> |
| • | | 20 | 2.3 | Tr. | 440 | 3500 | 9.5 | 5.3 | 2.5 | 420 | 1600 | 4.0 |
| | | 21 | 2.2 | .02 | 420 | 3100 | 8.0 | 2.8 | .40 | 1200 | 1600 | 111. |
| | | 22 | 2.1 | Tr. | 460 | 2700 | 7.5 | 3.6 | •35 | 780 | 1170 | 5.(|
| • | | 23. | 2.4 | .01 | 440 | 2500 | 6.5 | 2.5 | 30 | 2300 | 1300 | 18. |
| _ | | 24 | 2.4 | .01 | 500 | 2700 | 8.0 | 2.3 | 1.2 | 2600 | 1300 | 20.0 |
| | | 25 | | | | | | | | | | |
| | 5 | 26 | | | | | | | | | | |
| • | | 27 | 2.7 | Tr | 230 | 2950 | 4.0 | 4.4 | -53 | 620 | 1600 | 6.0 |
| | | 28 | 2.6 | .01 | 350 | . 2700 | 5.5 | 3.0 | .45 | 1390 | 1450 | 12. |
| | 5 | 29 | 2.5 | .03 | 460 | 2550 | 7.0 | 4.7 | .58 | 720 | 1450 | 6. |
| • | | _30 | 2.5 | .01 | 420 | 2400 | 6.0 | 4.2 | 1.10 | 890 | 1600 | 8. |
| (| •••••••••••••••••••••••••••••••••••••• | 31 | 2.7 | ጥን | 780 | 2550 | 7-0 | 3.6 | 1.50 | 1550 | 1450 | 13. |

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| 42.383 | | | r | west | | | | | | | |
|--|------|----------|----------------------------|-------------------------------|----------|--|--------------|----------------------------|----------|------------------|---|
| • | Date | pH | Settled Solids Vol.% | P ₂ 0 ₅ | GPM | Ppn 7 | рН | Settled Solids Vol.% | P_0/5 | GPM | POPINIE POPINIE TPD |
| · | 1 | 2,4 | ア | 125" | 2950 | 2-27 | 2,9 | 7 | 62 | 105 | Þ-27 |
| | 2 | | 7 | 1.7 | 4 7 7 | 1 1 | | | | | 7 |
| | 3 | , | | | 1300 | 65-4 | 377 | | 2:: | 177 | >110 |
| | 4 | | | | | | | | | | |
| | 5 | . 2., | . / | /. | : 50 | | 3,3 | 1.0 | | 1451 | |
| | 6 | 15.6 | | 1-2 | 3810 | | | | 85 | رون <u>ما ر</u> | |
| • | 7 | | | | | | | | | 2.3. | / |
| | 8 | | 1 - | | 1770 | | | | | | 163 |
| ! | 9 | | | ,,,, | <u> </u> | 464 | . <i>)</i> . | 1,0 | 75 | | |
| • | 10 | | | | £ 18 3 | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | | ļ | | |
| | 11 | | | | 3. 14 | | | | <u> </u> | | |
| <u>.</u> | 12 | 5.5 | T | | <u> </u> | <u> </u> | 5,1 | ٢, ٢ | 2000 | | <u> </u> |
| •(1 | 13 | <u> </u> | | 13 = 1 | 3300 | | | . | 81 | 1250 | |
| <u> </u> | 14 | 2.7 | T | | 2700 | | | | | | |
| | 15 | | 17 | 15.11 | 3/22 | // | 2011 | .5 | 8: | 1:00 | 1/ |
| · | 16 | | 1 | · | <u> </u> | 47/ | X | 18. | <u> </u> | | 7/85 |
| | 17 | 2.1 | 1 | 13/2 | 3300 | | 3.5 | 1/ | 32 | <u>رد د تر ز</u> | \\ \ |
| - F B -> | 18 | 1.7 | 1 | 11 " | 2400 | · | | | | | |
| | 19 | £.5 | 1 | 13 " | 3100 | · <u> </u> | | | | | <u> </u> |
| • | 20 | | 1 | 1 / // | 3503 | <u> </u> | 5.7 | 25. | 3 3 | 1500 | <u> </u> |
| | 21 | 2,2 | . 2 | 13 | 2160 | | 2.2 | 4.3 | 86. | د ر ز | - |
| | 22 | <u></u> | 1 | 12 | 5 . , | | 3.6 | 3.5 | 2 | 1175 | 1/ |
| • | 23. | 5.4 | ./_ | 11:- | 25.70 | 828 | 2,5 | 3.00 | 72 | 1300 | 12 |
| | 24 | 2,7 | <u> </u> | 12 | 3703 | <u> </u> | 213 | 12,0 | 75 | 1700 | |
| | 25 | | | ļ | | ' ' | | | | <u> </u> | |
| • | 26 | | <u> </u> | <u> </u> | | <u> </u> | | | | | <u> </u> |
| _ | 27 | 2,7 | 1 | 123 | 2950 | | 414 | 5,3 | 85 | 16:0 | <u> </u> |
| | 28 | 2,6 | ./ | 2 | 2700 | <u> </u> | 3.0 | 4.5 | 8" | 1450 | |
| | 29 | 2.5 | 13 | 11. | 2555 | 1/ | 4,7 | 5,8 | 811 | 1450 | 175 |
| • | 30 | 2.5 | .1 | 11 " | 3400 | 1033 | 4.2 | 11.0_ | 81 | 1600 | |
| - | 31 | 0 - | 1 | 1114 | 1.0 | 10 | 76 | 153 | 8 | 11.00 | 1 |

| | | | EFFI | LUENT | DI | тсне | S | | | Monui | oi: | |
|---|------|---|-------------------|--|---|---------|--------------------------------------|--------------|-----------------|------------------|---------------------------|-------------------------------|
| • | • | | 7/8 | | | 8 /(ar) | = 193.0 | 91.9 | 14.59 | Dre | 1. h | |
| The second | /\ | .) = | | | 2.7 | 19 | | 2 | 10.59 | 12311 1 e sit | 35% | 17. |
| 49-383 | | 0 (| 7. 5) | Settled | a st | (2921) | (6.7) | (3.7) | | | A(1:0) | (7/i) |
| | Date | | Hor | Solids Vol.% | P ₂ 0 ₅ | CTM | P ₂ O ₅ TPD | | Solids Vol.% | P205 | GPM_ | P ₂ O ₅ |
| | l l | | Dn D U | 7 | ppm | GPM | (i) | pH | VO1.70 | _ppm | _GPM /:/_50 | |
| | 2 | し | <i>J</i> | 7, | 5 a - | 2.70 | 10.1 | 3. | , 20 | 3.1 | <u></u> | \ |
| | 3 | v | 4,7 | | 1/7 | | , | . / | | | | 1/ |
| , • [| 4 | | | | | | 8 | | | | | <i>→</i> |
| | 5 | | 24 | 1/2 | 3.1 | 7/10 | 6 | 5, 3 | .20 | 75.2 | 175) | 3,5 |
| | 6 | | 26 | <u> </u> | | 1300 | 1 | عرب ا | | , | /4d) | 7 |
| • | 7 | | | 7/ | | | | | - | | , , | 77 |
| | 8 | | 2.1 | 7. | 250 | 27/11 | 1/ | / | A | 600 | City | 6 |
| · · | 9 | | 30 | 7 | /: 、 | 2000 | 2 | 47 | | -10 | 49. | 2 |
| • | 10 | | | 70 | 330 | 2750 | 3 5 | 61 | .07 | 20) | 2y 1 | 1.5 |
| | 11 | | 2 2 | 7. | 570 | | 5 | | | | | |
| <u></u> | 12 | | | TV | 37.0 | 1 | 7.5 | . / | 35 | 7:2 | 17.1 | 6 |
| • - | 13 | | 3,0 | 17 V | 204 | 3,20 | 4 | 6 | .21 | 75 | 1 6 | ر. د |
| | 14 | ļ | 2.1 | 17, | 37.0 | 2703 | 155 | | | | | |
| | 15 | | 2.7 | TV | 4/1/.) | 3/0 | 8 | 2.1 | .05 | 1730 | /) | 18 |
| L: | 16 | | م ر | 70 | (150) | 3310 | 9 | | . ù ċ | 1311 | 1/3 | 12. |
| | 17 | C. | 2.1 | 7. | 470 | 331 | . 13. | ラン | 27 | 3 ; . | 131 | 5 |
| | 18. | \ | | 7. | A. A. | / \ | 7 | | | | | |
| | 19 | <u> </u> | 2:3 | 71. | 11 | -11) | 85 | | | | | |
| • | 20 | | 23 | 170 | 4.1. | 200 | 55 | 5,3 | 2.5 | 420 | 11,11 | 4 |
| | 21 | | - > | ,02 | 1/50 | 3/112. | 8 | - 5 | 41, | 1200 | 140) | //: |
| - | 22 | \ | 2.1 | Tr | 2/1,0 | = 70 U | 75 | 36 | 35 | 7.3 | 1170 | 5 |
| | 23 | | a./ | 01 | 490 | 12.12 | 6.5 | _ د | . 5.) - | 2500 | 1500 | 18 |
| - | 24 | | 24 | 01 | 2013 | 2700 | 8 | 2.3 | 1.2 | 2010 | 1-11-1 | 3 |
| | 25 | · | | · | | | | | <u> </u> | | | <u> </u> - |
| • | 26 | · | ļ | | | | | | ! | | | <u>:</u> |
| - · · · · · · · · · · · · · · · · · · · | 27 | <u>.</u> | 2.7 | Tr | 230 | 2950 | 1 | <u>(j. 1</u> | 27 | 620 | | 6 |
| | 28 | | 2.6 | 1.77 | 320) | 3 70) | 5,> | <u> </u> | 1.1/5 | 1370 | JV.5. | 12 |
| | 29 | <u> </u> | 2.5 | 2 | <u> </u> | 25.7 | 7 | 47 | 152 | | 11/50 | 6 |
| | 30 | | 25 | | , , , , , , , , , , , , , , , , , , , | 2:193 | 6 | 4/2 | 1.10 | 290 | | |
| · · | 31 | | lo o | 7 7 7 | 1 1/ 0 | | 17 | | | 1/2/201 | (\mathcal{O}_{i},\cdot) | 13 |

February 1967

| I | 42-383 | | | | E | ast | <u> </u> | 6.6 | | V | lest | G. | 5./ |
|------------|---------------------------------------|------|-------------|-----|----------------------------|-------------------------------|----------|-------------------------------|-------|----------------------------|-------------------------------|----------|--------------------------------------|
| •_ | | Date | | | Settled Solids Vol.% | P ₂ 0 ₅ | GPM_ | P ₂ O ₅ | рН | Settled Solids Vol.% | P ₂ 0 ₅ | GPM | P ₂ O ₅ TPD |
| _ | · | 1_1 | | 3.5 | .01 | 130 | 2700 | 2 | 2.8 | .6 | 1430 | 1300 | 11_ |
| _ | | 2 | | 2.7 | .01+ | 440 | 3700 | 10 | 2.8 | .5 | 700 | 1300 | 5_ |
| • | · | 3 | ···· | 2.6 | | 390 | 1900 | 4 | . 3.3 | | 920 | 1300 | 7 |
| - | | 14 | | 2.8 | .01 | 230 | 3500 | 5 | 4.4 | 1.2 | 860 | 1450 | 8_ |
| <u>-</u> | | 5 | | 2.6 | .01_ | 620 | 3900 | 15 | 3.4 | .3_ | 790 | 1300 | 6 |
| | | 6 | | 2.8 | .01_ | 300 | 3900 | 7 | 2.9 | 1.4 | 1780 | 1300 | 1 /r |
| _ | · · · · · · · · · · · · · · · · · · · | 7 | · | 2.7 | .05 | 350 | 3700 | 8 | 3.6 | .7_ | 1050 | 1300 | 8 |
| _ | | 8 | | 2.3 | .01 | 370 | 4700 | 10 | 4.3 | .7_ | 570 | 1050 | 3.5 |
| ' - | _[` | 9 | | 2.5 | .01_ | 305 | 3300 | 6 | 2.8 | .2 | 670 | 1170 | 4.5 |
| • | | 10 | | | | ļ | | | | ļ | | | |
| : <u>-</u> | | 11 | · | 2.4 | .01 | 295 | 3500 | . 6 | 5.7 | .8 | 600 | 490 | 1.5 |
| _ | <u> </u> | 12 | ····· | 2.4 | .01_ | 270_ | 3100 | 5 | 3.3 | .85 | 1200 | 1170 | 8 |
| . | / ¹ | 13 | | 2.3 | .01 | 270 | 3500 | 5.5 | 2.5 | -35 | 1530 | 1170 | 10 |
| | • | 14 | | 2.7 | Tr. | 270 | 3300 | ~ 7.5 | 2.7 | •75 | 1390 | 1170 | 9 |
| _ | <u> </u> | 15 | · | 2.5 | Tr. | 460 | 3100 | 8.5 | 2.8 | .30 | 920 | 1300 | |
| _ | ¥ | 16 | | 2.8 | .01 | 440 | 3500 | 9. | 3.4 | .30 | 570 | 1170 | 4 . |
| _ | | 17 | | | | | | | | | | ļ | <u> </u> |
| | | 18 | | | | | <u>.</u> | | | | | | <u> </u> |
| | | 19 | · | 2.4 | .02 | 430 | 3500 | 9. | 2.9 | .40 | 830 | 920_ | <u> </u> |
| •_ | | 20 | | 2.6 | Tr | 380 | 3900 | 9. | 6.8 | .45 | 169 | 1170 | 1 |
| _ | <u> </u> | 21 | | | | | <u> </u> | | | | | <u> </u> | <u> </u> - |
| | | 22 | · | 2.6 | Tr | 244 | 3300 | 5 | 6.8 | -35 | 143 | 1050 | 1_ |
| • | | 23. | | 2.5 | .01 | 70 [°] . | 3300 | 1 | 6.6 | .41 | 215 | 1050 | 1.5 |
| | | 24 | | 2.4 | Tr | 250 | 2700 | 4 | 7.5 | 1.2 | 270 | 1300 | 2. |
| | | 25 | | 2.4 | Tr | 336_ | 2700 | 5 | 6.4 | 1.8 | 204 | 1300 | 1.5 |
| | | 26 | | 2.4 | Tr | 460 | 3500 | 10 | 6.5 | .50 | 350 | 1170 | 2.5 |
| | ** | 27 | | 2.8 | Tr | 193_ | 3500 | 14 | _6.6 | 1.0 | 305 | 1170_ | |
| | | 28 | | 2.5 | 01_ | 460 | 2700 | 7.5 | 6.7 | 1.0 | 350 | 1170 | 2 |
| | | 29 | | | | | | | | | <u> </u> | | <u> </u> |
| • | | 30 | | | ļ | | | | · | <u> </u> | | <u> </u> | <u>.</u> |
| | | 31 | • | | <u>i</u> | ÷ | <u> </u> | | | - | İ | | ì |

Month of:

Fibrary 1967

| 49-383 | | | I | ast | | | | 7 | West | . • | |
|---------------------------------------|--------|--|----------------------------|--|------------|-------------------------------|---------|----------------------------|---|-------|--|
| ●_ [[i] | Date | | Settled Solids Vol.% | P ₂ O ₅ | - GPM | P ₂ O ₅ | pH | Settled Solids Vol.% | P ₂ O ₅ | GPM | P2 ^O 5 |
| | 1 | 3.5 | ,01 | 120 | 27oil | 3 | 1. C + | 1,6, | (431) | 1200 | // |
| | 2 | | .01 | Upon | | <i>y</i> ,- | 28 | | 70 | 1300 | 5 |
| • | 3 | 2.6 | | | 16 .) | 4 | | | 920 | 1300 | 7 |
| | 4 | 2)_ | | 23.7 | 1) | <i>-</i> , | 4.1/ | | 50 | 1440 | 3 |
| <u> </u> | 5 | 1.6 | | 1 | = 700 | 15 | 5 (/ | <u> </u> | . , | 1900 | 0 |
| | 6 | | .01 | 300 | 3 39 3 | 7 | | 1.1/ | | | 14 |
| · · · · · · · · · · · · · · · · · · · | 7 | 2.7 | .01 | 250 | 3700 | | 3.6 | 7 | 1930 | 1300 | 1 |
| | 8 | 7 3 | ,01 | | 4700 | <u> </u> | 4.3 | .7 | 570 | 1050 | - - |
| -i | 9 | 2.5 | .01 | <u>کرہ 5</u> | 7300 | 6 | 3.8 | 12 | 670 | 117.1 | \(\frac{1}{2}\) |
| • | 10 | | | | | | ļ | | <u></u> | | |
| | 11 | | . () | 295 | ÷ ; ; | 6 | 5,7. | ./ | 600 | 470 | 1/5 |
| | 12 | . / | | 270 | 100 | | | ļ <u>-</u> | 12117 | 11. | <u> </u> |
| • (| 13 | | | 271 | | | | | 1550 | 1 | (11) |
| | 14 | | Tr | 3) | | 7 | | 73 | 13:11 | i i | <u> </u> |
| | 15 | 25 | ļ | 4/40 | - , | 8.5 | | 130 | 720 | 1300 | |
| | 16 | | .0/ | 447 | -200 | , | 31/ | | 570 | 1,-1 | <u> </u> |
| | 17 | | | | | | | | · . | | <u> </u> |
| - <u></u> | 18 | | | | | | | ļ. | | | |
| | .19 | / | , () | 4/3.) | | 9 | - 7 | .40 | | 72. | <u>t/</u> |
| • | 20 | 2.6 | 11 | 3.7 | 2116 | | 10.00 | , , , , , | 13 | 1170 | <u> </u> |
| <u> </u> | 21 | | | | | | | <u> </u> | | - | - |
| | 22 | | T | - | | 3 | | ļ | / / | | |
| • | 23. | 1=.5 | | | 5349 | / | 6,6 | 1.11 | . ; . | 11:10 | |
| | 24 | <u> </u> | 1 | 3.30 | | (/ | | 12- | - 29. | 1/200 | 12 |
| | 25 | = 1/ | 7. | <u> ` · · </u> | | 1.5 | / 1/ | 1.8 | - | 1 1 | 13 |
| • | 26 | -\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\-\ | TV | <u> </u> | | 10 | 4.5 | 1.57 | - | . 1** | <u> </u> |
| | 27 | 3,5 | | 173 | | - 1 | 6.13 | | () () () () () () () () () () | | |
| | 28 | 1215 | .01 | 1/1: | 27 | | 6/ | <u> </u> | 250 | 1 2 | 12 |
| | 29 - | 62.1 | | 8083 | 84117 | 164 | 1475 | 16.1 | 17/16 | 28240 |) [[] |
| - | 30 | | (.01) | X | you ! | 1 | 124 | 23 | 1-12 | 24 | 7 |
| • • | 1 31 / | ا (۱۵, دا | | 122-11 | 13 () A// | ///- | 11:11.5 | 7(.7) | 1747 | 91177 | 45 |

EFFLUENT DITCHES

January

42-363

East

West

| | : | Settled* | | | | | | | Settled* | | | |
|-----|------------------|-----------|----------|----------|----------|-------------------------------|-------|-------------------------------|----------|---------|-------------------------------|-------------------------------|
| • | | | | : | Solids | P ₂ 0 ₅ | am. | P ₂ O ₅ | ; | Solids | P ₂ 0 ₅ | P ₂ O ₅ |
| | ES. | Date 1 | | pH . | Vol.% | ppm / | 3012 | TPD | pH | Vol.% | ppm | GPM TPD |
| | 1 | 2 | ì | 2.3 | 120 | 1,510 | 3,300 | 30 | 4.0 | 4,500 | 1,230 | 2,550 18 |
| • | | 3 | | 2.4 | 160 | 1,120 | 3,300 | 22 | 4.0 | 2,600 | 950 | 2,700 15 |
| | | 4 | | 2.5 | 130 | | 2,700 | | 4.1 | 6,025 | | 2,500 |
| | | 5 | | | | 600 | | | | - | 980 | |
| _ ~ | ··· | 6 | | 2.4 | 20 | 750 | | | 4.9 | | 670 | |
| | • | 7 | | | | | | | | | | |
| | | 8 | | 2.3 | 70 | 700 | 3,950 | 17 | 2.8 | 3,500 | 1,600 | 2,200 21 |
| | | 9 | | 2.6 | 350 | 48 <u>0</u> | 3,300 | 9 | 5.3 | _7,500_ | 670 | 2,400 9 |
| • | : | 10 | | | | | | | ļ | i i | | |
| | | 11 | | 3.3 | 18,000 | 750 | 1,170 | 5 | 4.6 | 3,000 | 1,350 | 2,550 21 |
| | <u> </u> | 12 | | 3.4 | 1,200_ | 315 | 2,700 | 6 | 6.4 | 4,000 | 370 | 2,550 6 |
| • . | <u></u> | 13 | | <u> </u> | ļ | 250 | | , | | | 950 | |
| | | 14 | | | ļ | 370_ | | , p. | | 1 | 620 | |
| | <u></u> | 15 | | 3.1 | 2,000 | 370 | 2,700 | 6 | 3.4_ | 1,000_ | 1,830 | 2,700 30 |
| • | \$. | 16 | _ | 2.8 | 2,000 | 600 | 2,700 | 9 | 6.0 | 6,500 | 1,020 | 2,550 16 |
| | , | 17 | | 3.3 | 1,500 | 890 | 2,950 | 16 | 6.0 | 1,200 | 720 | 2,200 9 |
| _ | E3 | 18 | | 3.8 | 2,300 | 390 | 2,550 | 6 | 4.4 | 7,500 | 1,150 | 1,900 13 |
| | | 19 | <u> </u> | 3.7 | 4,00 | 370 | 3,100 | 8 | 2.5 | 4,050 | 2,100 | 2,700 35 |
| • | <u> </u> | 20 | | | | | | | | | | |
| | | 21 | | | <u> </u> | 860 | | | | | <u> </u> | |
| | f | 22 | | 2.7 | 170 | 330 | 2,700 | 6 | 7.3 | 1,600 | 250 | 3,100 4 |
| • | | 23 | | 2.7 | 170 | 276 | 2,950 | 5 | 6.1 | 1,500 | 285 | 3,100 6 |
| | · | 24 | | 3.3 | 2,000 | _530_ | 3,100 | 10 | 2.3 | 3,000 | 1,980 | 2,700 32 |
| | <u> </u> | 25 | | 2.1 | 140 | 620 | 3,100 | 11 | 4.2 | 1,250 | 460 | 2,950 8 |
| • | | 26 | | 2.5 | 400 | 390 | 3,300 | 8 | 5.0 | 5,000 | 570 | 2,950 10 |
| | · | 27 | | 2.2 | 70 | 390 | 3,300 | 8 | 2.4 | 6,500 | 1,120 | 3,100 / 2 |
| | | 28 | | 2.1 | 90 | 460 | 3,100 | 8 | | ! ! | | |
| i | - | 29 | | 2.7 | 70 | 415 | 3,300 | 2 | 6.7 | 3,000 | 380 | 3,300 7 |
| , | | 30 | | 3.0 | 40 | 250 | 3,500 | 5 | 5.1 | 4,500 | 700 | |
| | | 21 | | 2.7 | .i 8∩ | 285 | 3.500 | 6 | <u> </u> | 2.700 | 920 | 1.750 10 |

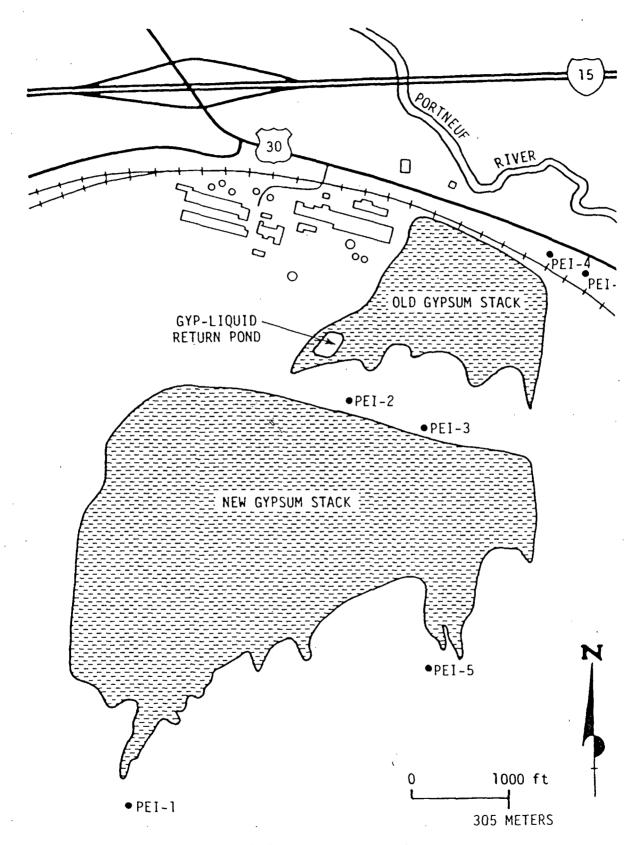


Figure 6-4.* PEI groundwater monitoring program at the J. R. Simplot study site.

6-10

Exhibit #22

| | | | | | - | | | |
|------|---------------------|------|-------------|----|--------------|----------|--------------|-------|
| CASE | MO-DA-YR | | · | | | | | |
| 1 | 09/28/78 | ALK | 226. | | CU | .006 | PO4 | .02 |
| | | AL | .015 | | CN | 0 | K | |
| | | NH3 | 0 | | F | .70 | RES | |
| | | AS | 0 | | ALFA | 2.5 | SE | 0 |
| | | BA | .12 | | BETA | 8.5 | SIC | |
| | | 8E | 0 | | OH | | AG | 0 |
| | | HC03 | | | FE | .037 | SAR | |
| | | В | .10 | | PB | 0 | NA | 32.90 |
| | | CD | 0 | | LI | .03 | S 0 4 | |
| | | CA | 58.40 | | MG | 23.50 | SUR | |
| | | CO3 | | | MN | .013 | TDS | |
| | | CL | 3 2. | | HG | 0 | KJE | |
| | | CR | 0 | | MO | Ö | VA | .04 |
| | | CO | 0 | • | NI | . 029 | ZN | .073 |
| | | COND | 530. | | NO3 | 1.20 | PH | 7.29 |
| | | · · | 350. | | 1100 | 1.20 | rn . | 1.27 |
| | | | · | | | | | |
| 2 | 05/28/79 | ALX | 236. | | CU | . 055 | P04 | .06 |
| - | **/ = -/ · · | AŁ | .02 | | CN | 0 | K | 6.04 |
| | | NH3 | .10 | | F | .63 | RES | |
| | | AS | .002 | | ALF A | 2.2 | SE | 0 · |
| | | BA | .09 | | BETA | 10.2 | SIO | |
| | | 8E | 0 | | OH | 10.2 | AG | 0 |
| | | HCO3 | V | | FE | .03 | | |
| | • | 8 | .23 | ٠. | PB | 0 .vž | SAR | |
| | | CD | .23 0 | | | | NA OOA | 36.11 |
| | | | 64. | | LI | .046 | \$04 | |
| | | CA | 04. | | MG | 19.20 | SUR | |
| | | C03 | 7.(| | MN | 0 | TOS | |
| | | CF | 36. | | He | 0 | KJE | |
| | | CR | .008 | | H0 | .01 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .054 |
| | | COND | 650. | | NO3 | . 78 | PH | 7.74 |
| | | | | | | | | |
| 3 | 09/10/79 | ALK | 236. | | CU | .009 | P04 | .10 |
| | , , | AL | .11 | | CN | 0 | X | 5.61 |
| | | NH3 | 0 | | F | .58 | RES | |
| | | AS | .001 | | ALFA | 2.6 | SE | 0 |
| | | BA | .08 | | BETA | 11. | SIG | |
| | | BE | 0 | | OH | | AG | 0 |
| | | HCD3 | 287. | | FE | .04 | SAR | |
| | | 8 | .14 | | PB | 0 | NA NA | 43 |
| | | CD | 0 | | LI | .048 | \$04 | |
| | | CA | 85.60 | | MG | 33.60 | SUR | |
| | | CO3 | 03.00 | | MN | .004 | TDS | |
| | | CL | 36. | | HG | 0 | KJE | |
| | | CR | .007 | | MO | 0 | VA | 0 |
| | | CO | .023 | | | 0 | | |
| | | | | | NI | | ZN | .054 |
| | | COND | 550. | | H93 | .82 | PH | 7.60 |

| CASE | MO-DA-YR | | | - | | | |
|------|----------|-------|---|------|-------|-------------|--------------|
| CHSE | אז-אט-טת | | | | | | |
| 4 | 04/28/80 | ALK | 224. | U3 | .01 | P04 | 10 |
| | | AL | . 15 | CN | .02 | K | 6.20 |
| | | NH3 | .15 | F | ,73 | RESD | |
| | | AS | 0 | ALFA | 3.5 | SE | 0 |
| | | BA | .16 | BETA | 12.5 | \$102 | 31. |
| | | BE | 0 | OH | | AG | 0 |
| | | HCO3 | 273.3 | FE | .01 | SAR | . 962 |
| | | 8 | .16 | P8 | 0 | NA | 34 |
| | | CD | 0 | LI | .048 | S04 | 45. |
| | • | CA | 63.20 | MG | 19.20 | SURF | 0 |
| | | CO3 | *************************************** | MN | 0 | TDS | 336. |
| | | CL | 32. | HG | 0 | KJEL | .50 |
| | | CR | 0 | H0 | .003 | VA | .002 |
| | | CO | .003 | NI | 0 | ZN | .03 |
| • | | COND | 510. | NO3 | 0 | . PH | 7.10 |
| | | COND | | NUS | | , гл | 7.10 |
| | | | | | | | |
| 5 | 07/23/80 | ALK | 252. | CU | .04 | P04 | . 46 |
| | | AL | 0 | CN | .139 | K | 5.30 / |
| | | NH3 | 0 | F | . 32 | RESD | |
| | • | AS | .002 | ALFA | 1.2 | SE | 0 |
| | BA | .10 | BETA | 1.5 | \$102 | 27.50 | |
| | | 8E | 0 | ОН | | AG | 0 |
| | | HCO3 | 307.4 | FE | .01 | SAR | 1.067 |
| | | В | .10 | PB | 0 % | na na | 38.50 |
| | | CD | .001 | LI | .048 | S04 | 40. |
| | | CA | 64. | HG | 21.12 | SURF | 0 |
| | | CO3 | | MH | .005 | TDS | 360. |
| | • | CL | 36. | HG | 0 | KJEL | 0 |
| | | CR - | .004 | HO | Ŏ | VA | Ŏ |
| | | CO | 0 | NI | 0 | ZN | .07 |
| | | COND | 550. | NO3 | . 92 | PH | 7.80 |
| | | | | | | | |
| 6 | 12/10/80 | ALK | 234. | CU | .01 | P04 | .07 |
| | | AL | 0 | CN | 0 | K | 5. |
| | | NH3 | 0 | F | .28 | RESD | |
| | | AS | . 002 | ALFA | .9 | SE | 0 |
| | | BA | .09 | BETA | 8.5 | \$102 | 29.50 |
| | | BE | 0 | OH | | AG | 0 |
| | | HC03 | 285.5 | FE | .02 | SAR | .99 8 |
| | | 8 | .195 | PB | 0 | NA | 36 |
| | | CD | 0 - | LI | .045 | S 04 | 43. |
| | | CA | 64.80 | MG | 20.64 | SURF | 0 |
| | | · C03 | • | MN | .005 | TDS | 340- |
| | | CL | 30.20 | HG | 0 | KJEL | .15 |
| | | CR | .034 | MO | 0 | VA | .003 |
| | | CO | .004 | . NI | 0 | ZN | .095 |
| | | COND | 520. | NO3 | 1.35 | PH | 7.40 |
| | | | - | | | * ** | |

| | | | • | - | | | |
|------|------------|------|-------|--------------|-------|---------------|--------------|
| CASE | MO-DA-YR | | | | | | |
| 7 | 03/23/81 | ALK | 224. | CU | . 005 | P04 | .27 |
| • | VV, 10, 01 | AL | .01 | CN | 0 | K | 5.80 |
| | | NH3 | 0 | F | .70 | , RESD | |
| | | AS | .002 | ALF a | 0 | SE | 0 |
| | | BA | .10 | BETA | Ŏ | \$102 | 30. |
| | | 8E | 0 | OH | V | AG | 0 |
| | | HCO3 | 273.3 | FE | .02 | SAR | 1.039 |
| | | B | .11 | PB | | NA NA | 38.10 |
| | | | | | 0 | | |
| | | CD | 0 | LΙ | .05 | \$04 800 F | 60. |
| | | CA | 75.20 | MG | 16.32 | SURF | 9 |
| | | CD3 | •• •• | MM | .01 | TDS | 3 65. |
| | | CL | 37.73 | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | . 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | . 025 |
| | | COND | 560. | NO3 | 1.07 | PH | 8.00 |
| | | | | | | | |
| 8 | 10/20/81 | ALK | 237.5 | CU | .007 | P04 | .30 |
| | ,, | AL | 0 | CN | 0 | x | 5.60 |
| | | NH3 | .09 | F | .60 | RESD | .179 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .11 | BETA | 0 | \$102 | 34.80 |
| | | BE | 0 | OH | · 0 | AG | 0 |
| | | HC03 | 289.8 | FE | .04 | SAR | 1.093 |
| | | В | .118 | PB | .005 | NA | 38 |
| | | CD | 0 | LI | .09 | SD4 | 42. |
| | | CA | 60. | MG | 19.20 | SURF | 0 |
| | | CO3 | 0 | HN | .014 | TDS | 310. |
| | | CL | 30.60 | HG | 0 | KJEL | .15 |
| | | CR | 0 | MO | 0 | VA | . 0 |
| | | CO | 0 | NI | 0 | ZN | |
| | • | | 490. | | | | .02 |
| | | COND | 470. | NO3 | .21 | PH | 7.90 |
| | | | | | | | |
| 9 | 03/10/82 | ALK | 245. | CU | .01 | P04 | .10 |
| | | AL | 0 | CN | .02 | K | 5.90 |
| | | NH3 | . 05 | F | .59 | RESD | .25 |
| | | AS | .002 | ALFA | 0 | SE | .001 |
| | | BA | . 105 | BETA | 0 | \$102 | 35.10 |
| | | BE | . 0 | OH | 0 | AG | 0 |
| | | HC03 | 298.9 | FE | .01 | SAR | 1.057 |
| | | 8 | .105 | PB | .003 | HA | 39 |
| | • | CD | .0 | LI | .092 | S04 | 52. |
| | | CA | 67. | MG | 22. | SURF | 0 |
| | | CO3 | . 0 | MN | .01 | TDS | 368. |
| | | CL | 34. | HG | 0 | KJEL | .12 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .028 |
| | | COND | 550. | NO3 | 1.17 | PH | 7.50 |

| CASE | MO-DA-YR | | | | - | | | |
|------|------------------|--------------|-------|---|------|-------------|------------|--------|
| 10 | 05/13/82 | ALK | 221.5 | | CU | .01 | P04 | .07 |
| | | AL | 0 | | CN | 0 | K | 4.80 |
| | | NH3 | .51 | | F | .60 | RESD | -0.854 |
| | | AS | . 003 | | ALFA | 1.4 | SE | 0 |
| | | BA | .11 | | BETA | 2. | \$102 | 31.80 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 270.2 | | FE | .01 | SAR | 1.043 |
| | • | В | . 095 | | PB | .003 | NA | 39 |
| | | CD | 0 | | LI | . 05 | S04 | 75. |
| | | CA | 68. | | MG | 23. | SURF | . 0 |
| | | C 03 | 0 | | MN | .005 | TDS | 398. |
| | | CL | 36.40 | | HG | 0 | KJEL | .65 |
| | | CR | .002 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .02 |
| | | COND | 600. | | NO3 | 1.40 | PH | 7.80 |
| | | | | - | | | | |
| 11 | 08/26/8 2 | ALK | 244. | | CU | .01 | P04 | .14 |
| | | AL | 0 | | CN | 0 | K | 6. |
| | | NH3 | 1.35 | | F | .62 | RESD | -0.290 |
| | | AS | .002 | | ALFA | 2.1 | SE | .001 |
| | | BA | .11 | | BETA | 2.4 | \$102 | 32.85 |
| | | 88 | 0 | | OH - | ·. 0 | AG | 0 |
| | | HCO3 | 297.6 | | FE | .01 | SAR | 1.068 |
| | | В | . 12 | | PB | 0 ** | NA | 39.50 |
| | | CD | 0 | | LI | .048 | S04 | 62. |
| | | CA | 69.60 | | MG | 20.64 | SURF | 0 |
| | | C O 3 | 0 | | MN | .003 | TDS | 379. |
| | | CL | 34.90 | | HG | 0 | KJEL | 1.58 |
| | | CR | 0 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .015 |
| | | COND | 580. | | NO3 | 1.31 | PH | 7.80 |
| | | | | • | | | | |
| 12 | 12/08/82 | ALK | 191. | | CU | .01 | P04 | .15 |
| | | AL | 0 | | CN | 0 . | K | 6.10 |
| | | NH3 | .07 | | F | .59 | RESD | 1.034 |
| | | AS | 0 | | ALFA | | SE | 0 |
| | | 8A | . 105 | | BETA | • | \$102 | 28. |
| | | 8E | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 233. | | FE | .02 | SAR | 1.102 |
| | | 8 | .11 | | PB | .002 | NA | 39.50 |
| | | CD | 0 | • | LI | .048 | S04 | 90. |
| | | CA | 69.60 | | MG | 16.80 | SURF | 0 |
| | | C03 | 0 | • | MN | .002 | TDS | 388. |
| | | CL | 35.10 | | HG | 0 | KJEL | .50 |
| | | CR | .002 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZH | .012 |
| | | COND | 580. | | HO3 | 1.77 | PH | 8.00 |

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|------|----------|-------|-------|------|-------|--------------|--------|
| CASE | MO-DA-YR | | | | | | |
| 13 | 02/22/83 | ALK | 240.7 | . CU | .01 | P04 | . 40 |
| | ,, | AL | 0 | CN | 0 | X | 6.10 |
| | | NH3 | .08 | F | .63 | RESD | -0.351 |
| | | AS | .002 | ALFA | 2. | SE | .002 |
| | | BA | .13 | BETA | 1.4 | \$102 | 27.50 |
| | | ΒE | 0 | OH | 0 | AG | 0 |
| | | HCD3 | 293.7 | FE | .01 | SAR | 1.055 |
| | | В | .12 | PB | 0 | NA | 39 |
| | | CD | 0 | LI | .048 | S04 | 74. |
| | | CA | 64. | HG | 24. | SURF | 0 |
| | | C03 | 0 | MN | .003 | TDS | 388. |
| | | CT | 24.60 | HG | 0 | KJEL | .10 |
| | | CR | .002 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .008 |
| | | COND | 600. | NO3 | 1.23 | PH | 7.50 |
| | • | COND | 000. | 1100 | 1.20 | FII | 7.30 |
| | | | | | | | • |
| 14 | 05/27/83 | ALK | 252. | CU | .03 | P04 | .08 |
| | | AL | .053 | CN | . 063 | K | 6. |
| | | NH3 | 0 | F | .53 | RESD | -0.048 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA . | .10 | BETA | 1.3 | \$102 | 28.80 |
| | | 38 | 0 | . OH | ·. 0 | AG | 0 |
| | | HCO3 | 307.4 | FE | .02 | SAR | 1.554 |
| | | В | .11 | PB | 0 %. | HA | 57 |
| | | CD | 0 | LI | .047 | S 0 4 | 62. |
| | | CA | 64. | MG | 23.04 | SURF | 0 |
| | | C03 | 0 | MN | .002 | TDS | 420. |
| | | CL | 40. | HG | 0' | KJEL | .20 |
| | | CR | .002 | MO | 0 | VA | 0 |
| | | CO. | 0 | NI | 0 | ZN | .035 |
| | | COND | 640. | NO3 | .24 | PH | 7.80 |
| | | | | | | | |
| 15 | 08/17/83 | ALK | 254. | CU | .02 | P 04 | .08 |
| | ,, | AL | .03 | CN | .002 | K | 6.10 |
| | | NH3 | .40 | F | .62 | RESD | .084 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .11 | BETA | 1.1 | \$102 | 27.40 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 309.8 | FE | .025 | SAR | 1.245 |
| | | В | .10 | PB | .003 | NA | 46 |
| | | CD | 0 | LI | .04 | S04 | 57. |
| | • | CA | 60. | MG | 26.40 | SURF | 0 |
| | | C03 | 0 | MN | .01 | TDS | 402. |
| | | CL | 40. | HG | 0 | KJEL | .70 |
| | | CR | .001 | MO . | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .03 |
| | | COND | 610. | NO3 | .30 | PH | 7.60 |
| | | 00110 | V. V. | 1100 | | 7 13 | |

| CASE | - MO-DA-YR | | | | | | • |
|------|------------|------|---------------|------|---------------|------------|--------------|
| 16 | 11/08/83 | ALK | 218. | cu | 0 | P04 | .10 |
| | | AL | .009 | CN | .005 | K | 4.70 |
| | | NH3 | . 80 | F | .59 | RESD | -0.862 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA | .093 | BETA | 1.3 | SI02 | 24.60 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 266. | FE | . 03 | SAR | .96 |
| | | В | .09 | PB | 0 | NA | 35.80 |
| | • | CD | 0 | LI | .04 | \$04 | 70. |
| | | CA | 62. | MG | 2 5.90 | SURF | 0 |
| | | C03 | 0 | HN | .001 | TDS | 380. |
| | | CL | 36. | HG | 0 | KJEL | 1.10 |
| | | CR | .001 | HO | 0 | VA . | 0 |
| | | CD | 0 | NI | 0 | ZN | .002 |
| | | COND | 570. | NO3 | 0 | PH | 7.70 |
| | | | | | • | | |
| 17 | 03/22/84 | ALK | 276. | CU | .02 | P04 | .10 |
| | | AL | 0 | CH | 0 | ĸ | 5.50 |
| | | NH3 | 0 | F | . 5 9 | RESD | 4.28 |
| | | AS | .002 | ALFA | · 0 | SE | 0 |
| | • | BA | .09 | BETA | 0 | \$102 | 25.10 |
| | | BE | 0 | OH | -, 0 | AG | 0 |
| | | HC03 | 336.7 | FE | 0 % | SAR | .801 |
| | | B . | . 08 | PB | 0 | NA | 41 |
| | | CD | 0 | LI | .05 | S04 | 230. |
| | | CA | 77.60 | MG | 27.96 | SURF | 0 |
| | | CD3 | 0 | MH | 0 | TDS | 640. |
| | | CL | 48. | HG | . 0 | KJEL. | .30 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | COND | 980. | NO3 | 1.93 | PH | 7.80 |
| | | | | | | | |
| 18 | 08/15/84 | ALK | 236. | CU | .012 | P04 | .08 |
| | , | AL | .03 | CN | . 0 | . K | 5.80 |
| | | NH3 | .32 | F | .53 | RESD | -0.192 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .12 | BETA | 3. | \$102 | 24.50 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 287.9 | FE | .02 | SAR | 1.749 |
| | | В | .174 | PB | .002 | NA | 63 |
| | | CD | 0 | ίΙ | .047 | SD4 | 5 3 . |
| | | CA | 63.20 | MG | 21.40 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 422. |
| | | CL | 75. | HG | 0 . | KJEL | .50 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | - 0 | NI | .02 | ZN | .018 |
| | _ | COND | 650. , | H03 | 1.83 | PH | 8.00 |
| | • | CUND | 000. | TUU | 1.00 | rii | J. VV |

| | | | | • | | | • |
|------|----------|------|---------------|------|-------------|---------------|---------------------------------------|
| CASE | MO-DA-YR | | | | | | |
| 19 | 11/12/84 | ALK | 240. | CU | .01 | P04 | .78 |
| | ,, | AL | .035 | CN | 0 | K | 5.83 |
| | | NH3 | .25 | F | .58 | RESD | .179 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .10 | BETA | 5. | SI02 | 27.29 |
| | | BE | 0 | . OH | 0 | AG | 0 |
| | | HC03 | 292.8 | FE | .02 | SAR | 1.433 |
| | | В | .111 | P8 | 0 | | |
| | | CD | 0 | LI | .05 | NA SO.4 | 52 |
| | | CA | 89.60 | MG | | \$04 | 48. |
| | | CO3. | 07.60 | | 6.20 | SURF | 0 |
| | | | | · MN | 0 | TDS | 430. |
| | | CL | 58. | HG | 0 | KJEL | .33 |
| | | CR | 0 | MO | 0 | VA | .006 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | COND | 650. | N03 | 1.43 | PH | 7.95 |
| | | | | | | | |
| 20 | 02/25/85 | ALK | 230. | CU | 0 | P04 | .02 |
| | | AL | . 005 | CN | 0 | K | 5.80 |
| | | NH3 | . 30 | F | .63 | RESD | -1.427 |
| | | AS | . 0 02 | ALFA | 0 | SE | 0 |
| | | BA | .10 | BETA | 6. | SI 0 2 | 32.53 |
| | | BE | 0 | ОН | ·. 0 | AG | 0 |
| | | HCO3 | 281. | FE | .0 8 | SAR | .977 |
| | | 8 | .12 | P8 | 0 ~ | NA | 39 |
| | | CD | 0 | LI - | .052 | S04 | 9 8. |
| | | CA | 81.70 | MG | 23.80 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 425. |
| | | CL | 38. | HG | 0 | KJEL | .55 |
| | | CR | .004 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | .06 | ZN | .048 |
| | | COND | 650. | NO3 | 1.51 | PH | 7.45 , |
| | | OOND | 030. | 1100 | 1.31 | rn . | , , , , , , , , , , , , , , , , , , , |
| 21 | 06/17/85 | ALK | 228. | CU | 0 | P04 | .38 |
| | 00/1//03 | AL | 0 | CN | 0 | K K | 6.10 |
| | | NH3 | Ŏ | F | .50 | RESD | - 0 .750 |
| | | AS | Ŏ | ALFA | 0 | SE | 0.730 |
| | | BA | .11 | BETA | 7. | SI02 | 26.33 |
| | | 8£ | 0 | 0H | ,. 0 | AG | 0 |
| | | HCO3 | 278.2 | FE | 0 | SAR | 1.148 |
| | | | | | | | |
| | | B | .17 | PB | .007 | NA SOA | 43 70 |
| | | CD | 0 | LI | .046 | S04 | 70. |
| | | CA | 72. | MG | 20.90 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 402. |
| | | CL | 40. | H6 | 0 | KJEL | .15 |
| | | CR | 0 | MO | .02 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 582. | NO3 | 1.48 | PH | 7.70 |

| CASE | MO-DA-YR | | | | | | |
|------|----------|--------------|----------|------|----------|-------|----------------|
| 22 | 08/19/85 | ALK | 230. | CU | 0 | P04 | .02 |
| | ,, | AL | .04 | CN | Ö | K | 5.20 |
| | | NH3 | 0 | F | .55 | RESD | -0.283 |
| | | AS | .003 | ALFA | 4. | SE | 0 |
| | | BA | .09 | BETA | i. 7. | \$102 | 28.03 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 281. | FE | Ö | SAR | 1.141 |
| | | В | .17 | PB | .005 | NA | 41 |
| | | CD | 0 | ĹĬ | .042 | \$04 | 51. |
| | | CA | 63.20 | MG | 21.12 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 376. |
| | | CŁ | 40. | HG | ŏ | KJEL | 0 |
| | | CR | .002 | MO | Ŏ | VA | 0 |
| | | CO | 0 | NI | 0 . | ZN | 0 |
| | | COND | 570. | NO3 | 1.59 | PH | 7.85 |
| | | COND | <i>'</i> | กบร | 1.37 | rπ | |
| | | | | | | | |
| 23 | 11/13/85 | ALK | 223. | CU | 0 | P04 | .04 |
| | | AL | 0 | CN | 0 | K | 6.70 |
| | | NH3 | 0 | F | .62 | RESD | -0.258 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .10 | BETA | 5. | \$102 | 27. 2 6 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 284. | FE | .02 | SAR | .993 |
| | | В | .17 | P8 | 0 ~ | NA | 35.80 |
| | | CD | 0 | LI | .043 | S04 | 48. |
| | | CA | 67.20 | MG | 19. | SURF | 0 |
| | | C O 3 | 0 | MN | . 0 | TDS | 370. |
| • | | CL | 36.30 | HG | 0 | KJEL | 0 |
| | | CR | .003 | MO | 0 | VA | .002 |
| | | CO | 0 | NI | 0 | ZN | .007 |
| | | COND | 550. | NO3 | 1.43 | PH | 7.65 |
| | | | | | | | |
| 24 | 02/19/86 | ALK | 240. | CV | 0 | P04 | .10 |
| | , , | AL . | 0 | CN | 0 | K | 5.25 |
| | | NH3 | . 20 | F | .55 | RESD | .465 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .10 | BETA | 5. | \$102 | 26.69 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 293. | FE | 0 | SAR | 1.061 |
| | | В | .21 | Ρ8 | .015 | NA | 39.60 |
| | | CD | 0 | LI | .045 | S04 | 51. |
| | | CA | 72.80 | MG | 19.90 | SURF | 0 |
| | | C03 | 0 | MH | 0 | TDS | 464. |
| | | CL | 40.50 | HG | 0 | KJEL | 5. |
| | | CR | 0 | MO | 0 | VA | .003 |
| | | CO | 0 | NI | .082 | ZH | .042 |
| | | COND | 672. | NO3 | 1.76 | PH | 8.03 |
| | | | | | | | |

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|------|----------|------|-------|---|------|-------|---|------|---------------|
| CASE | MO-DA-YR | | | | | | | | |
| 25 | 05/20/86 | ALX | 245. | | CU | 0 | | P04 | .07 |
| | | AL | 0 | | CN | 0 . | | K | 5.48 |
| | | NH3 | . 20 | | F | .49 | | RESD | -0.510 |
| | • | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .10 | | BETA | 0 | | SI02 | 27.52 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 299. | | FE | 0 | | SAR | 1.044 |
| | | В | .14 | | PB | 0 | | NA | 39.50 |
| | | CD | 0 | | LI | .041 | | S04 | 52. |
| | | CA | 73.80 | | MG | 21.10 | | SURF | 0 |
| | | C03 | 0 | | MN | .02 | | TDS | 410. |
| | | CL | 42.60 | | HG | 0 | | KJEL | .50 |
| | | CR | .002 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | .04 | | ZN | 0 |
| | | COND | 610. | | NO3 | 1.81 | | PH | 8.05 |
| | • | | | | | | | | |
| | | | | | | | | | |
| 26 | 07/07/86 | ALK | 226. | | CU | .02 | | P04 | .28 |
| | | AL | .08 | | CN | 0 | | K | 4.97 |
| | | NH3 | .21 | | F | .54 | | RESD | -0.372 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .09 | • | BETA | 0 | | SI02 | 23.11 |
| | | ΒE | 0 | | ОН | ·. 0 | | A6 | 0 |
| | | HCO3 | 275.7 | | FE | .026 | | SAR | 1.141 |
| | | 8 | . 183 | | PB | 0 " | | NA | 41 |
| | | CD | 0 | | LI | .038 | | S04 | 53. |
| | | CA | 65.60 | | MG | 19.70 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | TDS | 388. |
| | | CL | 47.90 | | HG | 0 | | KJEL | .30 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | . 0 | | NI | 0 | | ZN | .045 |
| | | COND | 550. | | NO3 | 1.49 | | PH | 8.10 |
| | | ٠. | | | | | | | |
| 27 | 11/06/86 | ALK | 228. | | CU | 0 | | P04 | 0 |
| | ,, | AL | 0 | | CN | Ō | | K | 5. 5 9 |
| | | NH3 | 0 | | F | .47 | | RESD | -0.450 |
| | | AS | 0 . | | ALFA | 0 | • | SE | 0 |
| | | BA | 10 | | BETA | 9. | | SI02 | 24.98 |
| | | 8E | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 278.2 | | FE - | 0 | | SAR | 1.014 |
| | | В | .12 | | PB | .008 | | NA. | 36.91 |
| | | CD | 0 | • | LI | .045 | | 504 | 40. |
| | | CA | 68.80 | | MG | 19.20 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | TDS | 365. |
| | | CL | 51.10 | | HG | Ö | | KJEL | 0 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | ŏ | | NI | Ö | | ZN | .009 |
| | | COND | 560. | | NO3 | 1.54 | | PH | 8.00 |
| | | | | | | | | | |

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|------|----------|------|-------|---|------|-------|-------------|------------|
| CASE | MO-DA-YR | | | | | | | |
| 28 | 03/03/87 | ALK | 222. | | CU | 0 | P04 | .08 |
| | ,, | AL | 0 | | CN | Ö | K K | 5.93 |
| | | NH3 | .27 | • | F | .66 | RESD | -0.538 |
| | | AS | 0 | | ALFA | 7. | SE | 0 |
| | | BA | . 09 | | BETA | 9. | \$102 | 26.54 |
| | | 8E | 0 | | OH. | 0 | | |
| | | HCO3 | 270.8 | | FE | 0 | AG | 0 1.054 |
| | | 8 | .16 | | PB | | SAR | |
| | | CD | 0 | | | 0 | NA SO4 | 38.24 |
| | | CA | 91.20 | | LI | .05 | \$04 | 53. |
| | | CO3 | 0 | | MG | 5.20 | SURF | 0 |
| | | | | | MN | 0 | TDS | 370. |
| | | CL | 40. | | HG | 0 | KJEL | . 29 |
| | | CR | 0 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZH | .007 |
| | | COND | 590. | | N03 | 1.51 | PH | 8.00 |
| | | | | | | | | |
| 29 | 05/06/87 | ALK | 246. | | CU | 0 | P 04 | .11 |
| | | AL | 0 | | CN | 0 | K | 6.15 |
| | | NH3 | .08 | - | F | .49 | RESD | -0.655 |
| | | AS | .003 | | ALFA | 0 | SE | 0 |
| | | BA | .10 | | BETA | Ö | \$102 | 25.07 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HC03 | 300. | | FE | | SAR | 1.106 |
| | | В | .16 | | PB | 0: | NA | 42.46 |
| | | CD | 0 | | LI | .046 | S04 | 52. |
| | | CA | 88. | • | MG | 14.40 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 418. |
| | | CL | 50. | | H6 | Ŏ | KJEL | .09 |
| | | CR | 0 | | MO | 0 | | |
| | | CO | . 0 | | | 0 | VA | 0 |
| | | COND | 650. | | NI | | ZN | |
| | | CUND | 630. | | NO3 | 1.73 | PH | 8.00 |
| 70 | 20/10/27 | | | | | | | |
| 30 | 08/19/87 | ALK | 242. | | CU | 0 | P04 | .08 |
| | | AL | 0 | | CH | .017 | K | 5.85 |
| | | NH3 | .08 | | F | . 54 | RESD | -0.164 |
| | | AS | 0 | | ALFA | _0 | SE | 0 |
| | | BA | . 09 | | BETA | 5. | \$102 | 28.45 |
| | | BE | 0 | | OH | 0 · | AG | 0 |
| | | HC03 | 295. | | FE | .02 | SAR | 1.122 |
| | | 8 | .10 | | PB | 0 | NA | 40.81 |
| | | CD | Q. | | LI | .04 | \$04 | 49. |
| | | CA | 62.85 | , | MG | 22.69 | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | TDS | 375. |
| | | CL | 41.30 | | He | 0 | KJEL | .10 |
| | | CR | 0 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI. | 0 | ZN | 0 |
| | | COND | 580. | | NO3 | 1.90 | PH | 7.60 |

| CASE | MO-DA-YR | | | | • . | | |
|------|----------|------|--------------|------------|---------------|--------------|--------------------|
| 31 | 11/13/87 | ALK | 205. | CU | 0 | P04 | .08 |
| | | AL | 0 | CN | 0 | K | 5.19 |
| | | NH3 | .07 | F | .51 | RES | SD -0.774 |
| | | AS | 0 | ALFA | 9. | SE | 0 |
| | | BA | .10 | BETA | 9. | SIC | |
| | • | BE | .002 | OH | 0 | AG | 0 |
| | | HC03 | 250. | FE | .08 | SAF | |
| | | 8 | .09 | PB | 0 | , NA | 37.99 |
| | | CD | 0 | LI | . 04 | \$04 | |
| | | CA | 60.89 | MG | 22.32 | SUF | |
| | | CO3 | 0 | MN | 0 | TDS | |
| | | CL | 35.70 | HG | 0 | KJE | |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | . ZN | 0 |
| | | COND | 560. | NO3 | 1.58 | PH | 7.80 |
| 32 | 03/16/88 | ALK | 222. | CU | Δ | 70 04 | 00 |
| 32 | 03/10/00 | AL | - 0 | CN | 0 0 | P04 | |
| | | NH3 | .14 | F | .62 | K | 5.93 |
| | | AS | .003 | r Alfa | 0 | RES | |
| | | BA | .003 | | | SE SZ | 0 70 04 |
| | | 8E | 0 | BETA Oh | 6. 0 | SIC | 30. 04 0 |
| | | HCO3 | 271. | FE | | AG Saf | |
| | | 8 | .12 | PB | 0. 0 | SAN NA | 42.90 |
| | | CD | 0 | LI | .04 | S04 | |
| | | CA | 93.60 | MG | 3.30 | SUF | |
| | | CO3 | 0 | HN | 0 | TDS | |
| | | CL | 40.50 | HG | 0 | KJE | |
| | | CR | .002 | MO | 0 | VA | . 0 |
| | | CO | .005 | NI | 0 | ZN | 0 |
| | | COND | 590. | NO3 | 1.55 | PH | 7.60 |
| | | CUND | 370. | NUS | 1.55 | rn | 7.00 |
| 33 | 06/07/88 | ALK | 208. | CU | . 0 | P04 | .07 |
| | | AL | 0 | CH | 0 | K | 5.66 |
| | | NH3 | 0 | F | .63 | RES | |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | . 0 9 | BETA | 6. | SIO | |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 254. | FE | . 0 | SAR | |
| | | 8 | .11 | P8 | 0 | HA | 34.25 |
| | | CD | 0 . | LI | .04 | \$04 | |
| | | CA | 96. | MG | 3.10 | SUR | |
| | | C03 | 0 | MN | 0 | TDS | |
| | | CL | 37.80 | He | 0 | KJE | |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI - | 0 | ZN | .08 |
| | | COND | 580. | NO3 . | 3. | PH | 7.80 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|----------|---------|-------------|--------|
| 34 | 10/07/88 | ALK | 218. | CU | 0 | P04 | .10 |
| | | AL | 0 | CN | 0 | K | 6.17 |
| | | NH3 | 0 | F | .58 | RESD | -0.725 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | ' BA | .10 | BETA | 0 | \$102 | 29.19 |
| | | BE | 0 | HO | 0 | AG | 0 |
| | | HCO3 | 266. | FE | 0 | SAR | .942 |
| | | 8 | .10 | PB | 0 | NA | 34.52 |
| | | CÐ | 0 | LI | . 05 | \$04 | 53. |
| | | CA | 96.80 | MG | 3.12 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 369. |
| | | CL | 42. | HG | 0 | KJEL | 0 |
| | | CR | 0 | . MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 580. | NO3 | 1.17 | PH | 8.30 |
| | | | | | | | |
| - 35 | 03/23/89 | ALK | 218. | CU | 0 | P04 | .13 |
| | • • | AL . | 0 | CN | 0 | X | 5.84 |
| | • | NH3 | 07 | F | .57 | RESD | -0.876 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .09 | BETA | 0 | \$102 | 29.25 |
| | • | BE | 0 | ОН | . 0 | AG | 0 |
| | | HC03 | 266. | FE | | SAR | .935 |
| | | 8 | .11 | PB | 0: 0 | NA | 34.81 |
| | | CD | 0 | LI | .05 | ` \$04 | 54. |
| | | CA | 84. | MG | 12.72 | SURF | 0 |
| | | C03 | 0 | MH. | 0 . | TDS | 378. |
| | | CL | 46. | HG | Ŏ | KJEL | .10 |
| | | CR | 0 | MO | Ŏ | VA | 0 |
| | | CO | 0 | NI | 0 | ZH | .01 |
| | | | | H03 | 1.51 | PH | 7.40 |
| | | COND | 780. | | 1.31 | ra | 7.40 |
| 36 | 05/15/89 | ALK | 221. | CU | .02 | P04 | .05 |
| | | AL | 0 | CN | .004 | K | 6.36 |
| | | NH3 | . 05 | F | .73 | RESD | -0.600 |
| | | AS | 0 | ALFA | 0 | . SE | 0 |
| | | BA | .09 | BETA | 0 | \$102 | 28.59 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 270. | FE | 0 | SAR | 1.055 |
| | | В | .11 | PB | 0 | NA | 38.47 |
| | | CD | 0 | LI | .05 | S04 | 55. |
| | | CA | 63.91 | MG | 22.36 | SURF | 0 |
| | | CO3 | 0 | MM | 0 | TDS | 368. |
| | | CL | 40.70 | He | Ö | KJEL | .08 |
| | | CR | 0 | H0 | Ö | VA | .01 |
| | | CO | Ö | NI NI | ŏ | ZN | 0 |
| | | COND | 580. | . NO3 | 1.52 | PH | 7.80 |
| | | COND | JOV. | กบว | 1.32 | rn | 7.00 |

| CASE | MO-DA-YR | | | | | | |
|------|----------|------|-------|------|------------------------|----------|---------|
| 37 | 09/11/89 | ALK | 193. | cu | 0 | P04 | .13 |
| | ,, | AL | 0 | CN | . 0 | K | 5.69 |
| | | HH3 | .06 | F | .66 | RESD | -0.880 |
| | | AS | 0 | ALFA | 3. | SE | 0 |
| | | BA | .09 | BETA | 5. | SI02 | 30.13 |
| | | BE | 0 | HO | 0 | AG | 0 |
| | | HC03 | 235. | FE | Ō | SAR | 1.01 |
| | | В | .12 | PB | 0 | NA | 35.66 |
| | | CD | 0 | LI | .05 | SD4 | 61. |
| | | CA | 59.69 | MG | 21.37 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 368. |
| • | | CL | 41.60 | HG | 0 | KJEL | .08 |
| | | CR | 0 | MO | 0 | YA | 0 |
| | | CO | 0 | HI | 0 | ZH | .06 |
| | | COND | 536. | N03 | 1.56 | PH | 7.70 |
| | | | | | | | |
| 38 | 10/11/89 | ALK | 208. | CU | 0 | PD4 | 0 |
| | ,, | AL | . 0 | CN | 0 | K | 5.66 |
| | | NH3 | 0 | F | .64 | RESD | -0.477 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .09 | BETA | 4. | SI02 | 31.20 |
| | | 8£ | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 254. | FE | | SAR | .989 |
| | | В | .08 | PB | . [.] 05 0 | NA NA | 34.65 |
| | | CD | 0 | LI | .05 | \$04 | 48. |
| | | CA | 58.73 | M6 | 20.82 | SURF. | 0 |
| | | C03 | 0 | MN | 0 | TDS | 325. |
| | | CL | 34.90 | He | 0 | KJEL | |
| | | CR | 0 | MO | 0 | VA | 0. 0 |
| | | | | | | | |
| | | COND | 0 | NI | 0 | ZH | .08 |
| | · | COND | 510. | N03 | 1.41 | PH | 7.80 |
| 39 | 03/26/90 | ALK | 220. | CU | 0 | PO4 | .08 |
| | • | AL | 0 | CH | 0 | K | 6.10 |
| | | NH3 | .09 | F | .58 | RESD | -0.504 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .10 | BETA | 6. | \$102 | 29.85 |
| | | 8E | 0 | OH | 0 | AG | .006 |
| | | HC03 | 268. | FE | 0 | SAR | 1.004 |
| | | В | .11 | PB | 0 | NA NA | 36.11 |
| | | CD | 0 | LI | .05 | S04 | 48. |
| | | CA | 63.93 | MG | 20.78 | SURF | 0 |
| | | CO3 | 0 | MN · | 0 | TDS | 436. |
| | | CL | 40.40 | HG | 0. | KJEL | .10 |
| | | CR | 0 | MO | 0 | VA | . 0 |
| | | CO | 0 | NI | 0 | ZN | .02 |
| | | COND | 583. | NO3 | 1.07 | PH | 7.80 |
| | | | | | | | |

| | | | | • | | | |
|------|----------|------|-------|------|-------|---------------|--------|
| CASE | MO-DA-YR | | | | | | |
| 40 | 07/05/90 | ALK | 213. | CU | 0 | P04 | .14 |
| | | AL | 0 | CN | 0 | K | 5.04 |
| | | NH3 | .13 | F | .66 | RESD | -0.243 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .08 | BETA | 4. | \$ 102 | 27.88 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 260. | FE | 0 | SAR | .977 |
| | | В | .08 | PB | 0 | NA | 33.72 |
| | | CD | 0 | LI | .04 | S04 | 56. |
| | | CA | 57.62 | MG | 19.84 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TOS | 376. |
| | | £L. | 39.50 | HG | 0 | KJEL | 2.18 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | . 02 |
| | | COND | 483. | NO3 | 1.38 | PH | 7.71 |
| | | | | | | | |
| 41 | 10/18/90 | ALK | 211. | CU | .03 | P04 | .69 |
| | | AL | .07 | CH | 0 | K | 4.97 |
| | | NH3 | 0 | F | .70 | RESD | -0.087 |
| | | AS | .004 | ALFA | 0 | SE | 0 |
| | | BA | .096 | BETA | 0 | \$102 | 39.30 |
| | | 8E | .002 | ОН | 0 | AG | 0 |
| | | HCO3 | 257. | FE | .21 | SAR | 1.25 |
| | | В | 0 | PB | .004 | NA | 35.51 |
| | | CD | .006 | LI | .05 | S04 | 51. |
| | | CA | 54.52 | MG | 18.62 | SURF | . 0 |
| | | C03 | 0 | MN | .02 | TDS | 404. |
| | | CL | 34.90 | H6 | 0 | KJEŁ | .05 |
| • | | CR | 0 | MO | .02 | . VA | 0 |
| | | CO | 0 | NI | 0 | ZN | . 04 |
| | | COND | 464. | NO3 | 1.47 | PH | 7.90 |
| | | | | | | | |

FRONTIER WELL - CHEMICAL ANALYSES

| AVERAGES | 09/28/7 | 78 TO 01/09/91 | | | | |
|----------|---------|----------------|------|--------|-------|---------|
| | ALK | 228.9 | CU | .009 | P04 | .151 |
| | AL | .016 | CN | . 007 | K | 5.718 |
| | NH3 | .149 | F . | . 584 | RESD | -17.230 |
| | AS | .001 | ALFA | 1.1 | SE | .00 |
| | BA | .10 | BETA | 4.1 | \$102 | 29.005 |
| | BE | .00 | OH | 0 | AG | .00 |
| | HCO3 | 279.4 | FE | .021 | SAR | 1.087 |
| | 8 | .124 | PB | .001 | · NA | 39.59 |
| | CD | .00 | LI | .048 | S04 | 60. |
| | CA | 70.406 | MG | 19.158 | SURF | 0 |
| | C03 | 0 | MN | .003 | TDS | 388. |
| | CL | 39.86 | HG | 0 | KJEL | . 433 |
| | CR | .002 | MO | .001 | VA | .002 |
| | CO | .001 | NI | .006 | ZN | .026 |
| | COND | 590. | NO3 | 1.315 | PH | 7.76 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | - | | | |
|------|----------|------|-------|------|---------------------------------------|---------|-------|
| 1 | 02/15/78 | ALK | 244. | CU | .009 | P04 | .15 |
| | | AL | .07 | CN | | K | 6.29 |
| | | NH3 | 0 | F | .74 | RESD | |
| | | AS | 0 | ALFA | 3.6 | SE | 0 |
| | | BA | .10 | BETA | 12. | \$102 | 37. |
| • | | BE | | OH | | AG | 0 |
| | | HCO3 | 297.6 | FE | .045 | SAR | 1.395 |
| | | 8 | .14 | PB | 0 | NA | 57 |
| | | CD | 0 | LI | 0 | S04 | 134. |
| | | CA | 84.80 | MG | 25.44 | SURF | 0 |
| | | C03 | 0 | MN | .008 | TDS | 504. |
| | | CL | 50. | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | | VA | |
| | | CO | | NI | .001 | ZN | .005 |
| | | COND | 775. | NO3 | ,65 | PH | 7.61 |
| | | | | | ` | | |
| 2 | 05/03/78 | ALK | 220. | cu | .021 | · P04 | .02 |
| | , , , | AL | .04 | CN | 0 | K | 7.39 |
| | | NH3 | 0 | F | .99 | RESD | |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .14 | BETA | 15. | \$102 | 35. |
| | | BE | | OH | ·. | AG | 0 |
| | | HCO3 | | FE | >023 | SAR | .49 |
| | | 8 | .10 | PB | 0 ~ | NA | 21 |
| | | CD | 0 | LI | 0 | S04 | 116. |
| | | CA | 77.60 | MG | 37.44 | SURF | 0 |
| | | C03 | 77.00 | MN | .009 | TDS | 435. |
| | | CF | 40. | HG | 0 | KJEL | 0 |
| | | CR | . 0 | MO | V | VA | V |
| | | CD | .003 | NI | 0 | . ZN | .013 |
| | | COND | 670. | NO3 | .80 | PH | 7.14 |
| | | | | | · · · · · · · · · · · · · · · · · · · | | • |
| 3 | 09/28/78 | ALK | 224. | cu | .004 | P04 | .04 |
| | | AL | .09 | CN | 0 | K | 7.35 |
| | | NH3 | 0 | F | 1.01 | RESD | |
| | | AS | 0 | ALFA | 3. | SE | 0 |
| | | BA | .11 | BETA | 8. | SI02 | 32.25 |
| | | BE | | OH | | AG | 0 |
| | | HCO3 | | FE | .009 | SAR | 1.209 |
| | | В | .17 | PB | .011 | NA | 45 |
| | | CD | 0 | LĪ | .017 | S04 | 110. |
| | | CA | 76. | MG | 17.70 | SURF | 0 |
| | | CO3 | | MN | .02 | TDS | 430. |
| | | CL | 32. | HG | 0 | KJEL | 0 |
| | * * * | CR | 0 | MO | · | VA | .03 |
| | | CO | Ó | NI | .003 | ZN | .024 |
| | | COND | 660. | NO3 | .90 | PH | 6.90 |
| | | | | | | • • • • | · · |

| CARE | MO-DA-VO | | • | | • | | | _ | |
|------|----------|--------------|--------|---|------|-------------|---|-------|-------|
| CASE | MO-DA-YR | | | | | | | | |
| 4 | 05/25/79 | ALK | 270. | | CU | .004 | | P04 | 0 |
| • | ,, | AL | .03 | | CN | 0 | | K | 7.83 |
| | | NH3 | .01 | | F | .85 | | RESD | |
| | | AS | .003 | | ALFA | 3.2 | | SE | .001 |
| | • | BA | .09 | | BETA | 9.5 | | SI02 | 38.50 |
| | | BE | 0 | | OH | /. . | | AG | 0 |
| | | HCO3 | U | | FE | 0 | | SAR | 1.303 |
| | | В | . 20 | | PB | 0 | | NA NA | 54.10 |
| | | CD | 0 | | | | | S04 | |
| | | | | | LI | .069 | | SURF | 135. |
| | | CA | 90.40 | | MG | 24.48 | | | 0 |
| | | C03 | | | MN | .003 | | TOS | 600. |
| | | CL | 40. | | HG | 0 | | KJEL | . 92 |
| | | CR | .003 | | H0 | 0 | | YA | 0 |
| | | CO | . 005 | • | NI | 0 | | ZN | .002 |
| | | COND | .920. | | ND3 | .82 | | PH | 7.63 |
| | | | | | | | | | |
| 5 | 09/10/79 | ALK | 242, | | CU | .009 | | P04 | .06 |
| | | AL | .021 | • | CN | 0 | | X | 6.98 |
| | | NH3 | 0 | | F | .83 | | RESD | |
| | | AS | .001 | | ALFA | 2.5 | | SE | 0 |
| | | BA | .07 | | 8ETA | 12. | | SI02 | 35. |
| | | BE | 107 | • | OH | ·. | | AG | 0 |
| | | HCO3 | 295.2 | | FE | .06 | | SAR | 1.448 |
| | | В | .15 | | PB | 0 | | NA | 54 |
| | | CD | 0 | | LI | .066 | • | S04 | 100. |
| | | CA | 98.40 | - | MG | 4.32 | | SURF | 0 |
| | | CO3 | 70.40 | | MN | .005 | , | TDS | 449. |
| | | CL | 32. | | HG | 0 | | KJEL | .05 |
| | | | | | MO | V | | VA | 0 |
| | | CR | .007 | | | 004 | | ZN | .027 |
| | | CO | .028 | | NI | .004 | | PH | |
| | | COND | 700. | | NO3 | . 53 | | PN . | 8.10 |
| 6 | 04/28/80 | ALK | 230. | | · CU | 0 | | P04 | .10 |
| | | AL | .065 | | CN | .002 | | K | 7. |
| | | NH3 | 0 | | F | .84 | | RESD | |
| | | AS | 0 ' | | ALFA | 2.5 | | SE | 0 |
| | | BA | .22 | | BETA | 8.5 | | \$102 | 35. |
| | | BE | 0 | | OH | | | AG | 0 |
| | • | HCO3 | 280.6 | | FE | .03 | | SAR | 1.251 |
| | | В | .125 | | PB | 0 | | NA | 48.50 |
| | | CD | 0 | | LΪ | .065 | | \$04 | 110. |
| | | CA | `78.40 | | MG | 21.60 | | SURF | 0. |
| | | C O 3 | | | MN | 0 | | TDS | 445. |
| | | CL | · 36. | | HG | Ö | | KJEL | 0 |
| | | CR | 0 | | MD | Ō | | VA | 0 |
| | | CO | .004 | | IH | .005 | | ZH | Ō |
| | | COND | 690. | | NO3 | 0 | | PH | 7.20 |
| | | COUD | 0,0. | | 1100 | V | | | |

| CASE | MO-DA-YR | | | | • | | | |
|------|----------|-------|-------|---|------|-------|-------------|-------|
| 7 | 07/23/80 | ALK | 300. | | cu | .02 | P0 4 | . 38 |
| | | AL | 0 | | CN | 0 | K | 8. |
| | • | NH3 | 0 | | F | 1.01 | RESD | |
| | | AS | .002 | | ALFA | 0 | SE | 0 |
| | | BA | .09 | | BETA | 0 | \$102 | 34.80 |
| | • | ΒE | 0 | | OH | | . AG | 0 |
| | | HC03 | 366. | • | FE | .01 | SAR | 1.951 |
| | | В | .13 | | PB | 0 | NA | 86 |
| | | CD | .002 | • | LI | .075 | S04 | 198. |
| | | CA | 100. | | MG | 28.80 | SURF | 0 |
| | | C03 | | | MN | .002 | TDS | 680. |
| | | CL | 50. | | HG | 0 | KJEL | 0 |
| | | CR | .004 | | MO | 0 | VA | .018 |
| | | CO | 0 | | NI | 0 | ZH | .01 |
| | | COND | 1050. | | NO3 | 1.41 | PH | 7.80 |
| | • | | | | | | 1 | |
| 8 | 12/10/80 | ALK | 314. | | CU | .01 | P04 | .09 |
| | | AL | 0 | | CN | 0 | K | 8. |
| | | NH3 | 0 | | F. | .46 | RESD | |
| | | AS | .003 | | ALFA | 1.9 | SE | 0 |
| | | BA | . 085 | | BETA | 10.7 | \$102 | 34.50 |
| | | BE | 0 | | DH | ٠. | AG | 0 |
| | | HCO3 | 383.1 | | FE | :02 | SAR | 1.528 |
| | | 8 | . 245 | | PB · | .001 | · NA | 69 |
| | | CD | 0 | • | LI | .07 | S04 | 174. |
| | | CA | 112. | | MG | 25.92 | SURF | 0 |
| | | C03 | | • | MN | 0 | TDS | 620. |
| | | CL | 41.70 | | HG | 0 | KJEL | .40 |
| | | CR | 0 | • | MO | 0 | VA . | 0 |
| | | CO | . 006 | | NI - | 0 | ZN | .005 |
| | - | COND | 950. | | N03 | 1.06 | PH | 7.30 |
| | | | | | | | | |
| 9 | 03/23/81 | ALK | 322. | | cu | .012 | P04 | .28 |
| | | AL | .07 | | CH | 0 | K | 8. |
| | | NH3 | 0 | | F | .83 | RESD | •• |
| | | AS | .002 | | ALFA | 0 | SE | .001 |
| | | BA. | .085 | | BETA | 0 | \$102 | 33. |
| | | BE | 0. | | OH | · | AG | 0 |
| | | HCO3 | 392.9 | | FE | .02 | SAR | 1.542 |
| | | В | .15 | | PB | .002 | NA | 70 |
| | | CD | .001 | | LI | .075 | S04 | 162. |
| | | CA | 112. | | MG | 26.88 | SURF | 0 |
| | | CO3 | | | MN | .015 | TDS | 620. |
| | | CL | 52.40 | | HG | .0041 | KJEL | 0 |
| | | CR | 0 | | MO | 0 | VA | Ō |
| | | CO | 0 | | HI | Ö | ZH | .01 |
| | | COND | 950. | | NO3 | 1.29 | PH | 7.70 |
| | | 40110 | /50. | | | 4.67 | 111 | /./V |

| | | | | | • | | | |
|------|----------|------|---------|---|----------|-------|-------------|-----------------|
| CASE | MO-DA-YR | | | | | • | | |
| 10 | 10/20/81 | ALK | 307. | | CU | .015 | P04 | .30 |
| 10 | 10/20/01 | AL | .01 | | CN | 0 | K | 8.60 |
| • | | NH3 | .36 | | F | .75 | RESD | -1.612 |
| | | AS | .005 | | ALFA. | 0 | SE | 0 |
| | | BA | .003 | | BETA | 0 | SI02 | 43.40 |
| | | | .006 | | | 0 | | 43.40 |
| - | | BE | 374.5 | | OH SE | | AG | |
| | | HCO3 | | | 34 00 | .06 | SAR | 1.59 |
| | | В | .155 | | PB | .003 | NA SOA | 72 |
| | | CD | 0 | | LI | .10 | S04 | 174. |
| | | CA | 100. | | 774 | 00.00 | SURF | 0 |
| | | C03 | 0 | | MN | .014 | TDS | 640. |
| | | CL | 52.50 | | HG | 0 | KJEL | .80 |
| | | CR | 0 | | MO | 0 | VA | .01 |
| | | CO | 0 | | NI | 0 | ZH | .012 |
| | | COND | 800. | | NO3 | .51 | PH | 7.50 |
| | | | | | | | | |
| 11 | 03/10/82 | ALK | 275.8 | | CU | .01 | 904 | .09 |
| | // | AL | 0 | | CN | .01 | . K | 8.20 |
| | | NH3 | .34 | | F | .81 | RESD | -0.725 |
| | | AS | .004 | | ALFA | 0 | SE | 0 |
| | | 8A | .08 | | BETA | 0 | SI02 | 18.95 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 336.5 | | FE | .01 | SAR | 1.775 |
| | | В | .145 | | PB | 0 | NA | 69.50 |
| | | CD | 0 | | ίΙ | 0 | \$04 | 190. |
| | | CA | 106. | | MG | 28. | SURF | 0 |
| | | CD3 | 0 | | MN | 0 | TDS | 615. |
| | | CL | 42.20 | | He. | Ŏ | KJEL | .50 |
| | | CR | 0 | | -MO | Ŏ | YA | 0 |
| | | CO | 0 | | NI | 0 | ZH | .01 |
| | | COND | 950. | | NO3 | .92 | PH | 7.20 |
| | | | | | | | | |
| 12 | 05/13/82 | ALK | 319.4 | | CU | 0 | P 04 | .15 |
| •• | 00/10/01 | AL | 0 | | CN | .012 | K | 4.80 |
| | | NH3 | 1.40 | • | F | .77 | RESD | -1.589 |
| | | AS | .004 | | ALFA | 1.7 | SE | 0 |
| | | BA | .075 | | BETA | 1.6 | \$102 | 42.20 |
| | | 8E | 0 | , | OH | . 0 | AG | 0 |
| | | HCO3 | . 389.7 | | FE | .01 | SAR | 1.959 |
| | | 8 | .135 | | PB | 0 | NA | 90 |
| | | CD | 0 | | LI | .0 | S04 | 210. |
| | | CA | 108. | | MG | 31.50 | SURF | 0 |
| | | CO3 | 0 | • | MN | .005 | TDS | 690. |
| | | CL | 47.30 | | HG | 0 | KJEL | 1.89 |
| | | CR | .002 | | MD | Ŏ | VA | 0 |
| | | CO | 0 | | NI | .012 | ZN | .01 |
| | | COND | 1050. | ٠ | NO3 | 1.33 | PH | 7.60 |
| | | OUND | 1070. | | | 1.40 | 111 | , . |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|--------------------|--------------------|--------------|-------------|------------|--------------|
| 16 | 05/27/83 | ALK | 268. | CU | .01 | P04 | .10 |
| | | AL | .81 | CH | .026 | K | 8.5 0 |
| | | NH3 | 0 | F | .81 | RESD | -1.477 |
| | | AS | .004 | ALFA | 0 | SE | 0 |
| | | BA | .08 | BETA | 1.1 | \$102 | 33.70 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HC03 | 326.9 | FE | .01 | SAR | 1.858 |
| | | В | .15 | PB | . 0 | NA | 79 |
| | | CD | 0 | LI | .072 | S04 | 182. |
| | | CA | 86.40 | MG | 30.72 | SURF | 0 |
| • | | C03 | 0 | MN | . 003 | TDS | 625. |
| | | CL | 52. | HG | 0 | KJEL | .08 |
| | | CR | .002 | MO > | . 005 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .002 |
| | | COND | 950. | NO3 | . 24 | PH | 7.80 |
| 17 | 08/17/83 | ALK | 330. | cu | 01 | P04 | 11 |
| 17 | VO/1//03 | | | CN . | .01 | | .11 |
| | | AL NH3 | .005 | F | .011 .81 | K Resd | 7.20 |
| | | | . 30 . 005 | • | | | 1.146 0 |
| | | AS | .085 | ALFA Beta | 0 1.2 | SE S102 | |
| | | BA | 0 | OH - | . 0 | 3102 AG | 32.60 0 |
| | | BE HCO7 | 402.6 | FE | | SAR | 1.878 |
| | | HC 0 3 B | .18 | PB | .015 0 | HA HA | 85 |
| | | CD | 0 | LI | .07 | 804 | 180. |
| | | CA | 92. | MG | 38.40 | SURF | 0 |
| | | C03 | 0 | MN | .004 | TDS | 650. |
| | | CL | 50. | HG | .0003 | KJEL | .80 |
| | • | CR | .001 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .006 |
| | • | COND | 990. | NO3 | .20 | PH | 7.60 |
| | | VOIID | | | | | ,,,,, |
| 18 | 11/08/83 | ALX | 268. | cu | .009 | P04 | .10 |
| | | AL | .014 | CN | .014 | K | 7.20 |
| | • | NH3 | 1.80 | F | .76 | RESD | -2.131 |
| | | AS | . 006 | ALFA | 0 | SE | 0 |
| | | BA | .079 | BETA | 1.5 | \$102 | 32. |
| | | 38 | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 327. | FE | . 02 | SAR | 1.431 |
| | | В | .15 | PB | 0 | , NA | 63.70 |
| | | CD | 0 | ŁI | .07 | \$04 | 180. |
| | | CA | 90. | MG | 36.50 | SURF | 0 |
| | | CO3 | 0 | MN | .012 | TDS | 680. |
| | | CL | 44. | HG | 0 | KJEL | 2.15 |
| | | CR | . 002 | MO | 0 | VA . | .01 |
| | | | | | | | |
| | | CO COND | 0 9 00 . | NI NO3 | 0 .14 | ZN Ph | .002 7.20 |

| | | | | | - | | | |
|------|----------|------|--------|---|------|-------------|--------|--------|
| CASE | MO-DA-YR | | | | | | | |
| 19 | 03/22/84 | ALK | 284. | | CU | 0 | P04 | .12 |
| | | AL | .005 | | CH | 0 | K | 7.37 |
| | | NH3 | 0 | | F | 1.01 | RESD | 1.85 |
| | | AS | .005 | | ALFA | 0 | SE | . 0 |
| | • | BA | .10 | | BETA | 0 | \$102 | 31. |
| | | 8E | 0 . | | OH | 0 | AG | 0 |
| | | HCO3 | 346.5 | | FE | 0 | SAR | 3.13 |
| | | В | .05 | | PB | .069 | NA | 70 |
| | | CD | 0 | | LI | .07 | 504 | 334. |
| | | CA | 102.80 | | MG | 29.28 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 840. |
| | | CL . | 52. | | HG | 0 | KJEL | . 20 |
| | • | CR | .002 | | MO | Ö | VA | .02 |
| | | CO | 0 | | NI | Ŏ | ZN | 0 |
| | , | COND | 1290. | • | NO3 | 1.33 | PH | 7.30 |
| | ` | | | | | | | |
| 20 | 08/15/84 | ALK | 276. | | CU | .014 | P04 | . 23 |
| | | AL | 0 | | CN | 0 | K | 8.30 |
| | | NH3 | 23 | | F | .78 | RESD | -2.626 |
| | | AS | .007 | | ALFA | 0 | SE | 0 |
| | | BA | .08 | | BETA | 5. | \$102 | 21.70 |
| | | BE | 0 | | OH | ·. 0 | AG | 0 |
| | | HCO3 | 336.7 | | FE | :.02 | SAR | 1.455 |
| | | В | .179 | | PB | .061 | NA | 67.50 |
| | | CD | 0 | | LI | .07 | \$04 | 172. |
| | | CA | 100. | | MG | 38.40 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 620. |
| | | CL | 75. | | HG | 0 | KJEL | .45 |
| | | CR | 0 | | MO | .02 | VA | 0 |
| | | CO | Ö | | NI | 0 | ZN | .008 |
| | | COND | 940. | | NO3 | 1.06 | PH | 7.90 |
| | | | | | | | . ' | |
| 21 | 11/12/84 | ALK | 288. | | CU | .01 | P04 | .35 |
| | | AL | .005 | | CN | 0 _ | K | 8.40 |
| | | NH3 | . 40 | | F | .79 | RESD | -1.560 |
| | | AS | .006 | | ALFA | 0 | SE | 0 |
| | | 8A | .08 | | BETA | 9. | \$102 | 37.10 |
| | | BE | 0 | | OH | 0 | AG | . 0 |
| | - | HCO3 | 351.4 | | FE | .02 | SAR | 3.012 |
| | | В | . 161 | | PB | .014 | NA | 67.60 |
| | | CD | 0 . | | LI | .074 | ~ \$04 | 162. |
| | | CA | 102.40 | | MG . | 26.90 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 595. |
| | | CL | 46. | | HG | 0 | KJEL | .65 |
| | | CR | .003 | | MO | .01 | VA | .007 |
| | | CO | 0 | | NI | 0 | . ZN | .005 |
| | | COND | 900. | | N03 | 1.12 | PH | 7.68 |
| | | | | | | | | |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|--------|--------------|-------|-------|--------|
| 22 | 02/25/85 | ALK | 279. | CU | 0 | P04 | .06 |
| | | AL | .004 | CN | 0 | K | 8.50 |
| | | NH3 | . 05 | F | . 82 | RESD | -3.310 |
| | | AS | .008 | ALFA | 0 | SE | 0 |
| | | BA | .08 | BETA | 7. | \$102 | 43.66 |
| | | 8E | 0 | НО | 0 | AG | 0 |
| | • | HCO3 | 340. | FE | 0 | SAR | 1.411 |
| | | В | .15 | PB | 0 | NA | 68.40 |
| | | CD | 0 | LI | .075 | S04 | 238. |
| | | CA | 125.70 | MG | 31.80 | SURF | 0 - |
| | | C03 | 0 | MN | 0 | TDS | 680. |
| | | CL | 44. | HG | 0 | KJEL | .16 |
| | | CR | .006 | MO | .03 | VA | .006 |
| | | CO | 0 | NI | 0 | ZN | .005 |
| | | COND | 1050. | NO3 | 1.17 | PH | 7.20 |
| | | | • | | | | |
| 23 | 06/17/85 | ALK | 266. | CU | 0 | P04 | . 38 |
| | | AL | 0 | CN | 0 | K | 8.60 |
| | | NH3 | 0 | F | .76 | RESD | -1.769 |
| | | AS | .008 | ALF A | 0 | SE | 0 |
| | • | 8A | .08 | BETA | 12. | \$102 | 37.06 |
| | | BE | 0 | OH | ·. 0 | AG | 0 |
| | | HC03 | 324.5 | FE | მ. ু | SAR | 1.502 |
| | | В | .19 | PB | .002 | NA | 65 |
| | | CD | 0 | ŁI | .06 | S04 | 174. |
| | | CA | 114.40 | MG | 16.80 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 610. |
| | | CL | 55. | HG | 0 | KJEL | 0 |
| | | CR | . 03 | · MO | 0 | VA | .005 |
| | | 03 | 0 | NI | 0 | ZN | 0 |
| | | COND | 940. | NO3 | 1.23 | PH | 8.20 |
| | | | | | | | |
| 24 | 08/19/85 | ALK | 290. | CU | 0 | P04 | . 39 |
| | | AL | 0 | CN | 0 | K | 7.90 |
| | | NH3 | .10 | F | .80 | RESD | 1.516 |
| | | AS | .009 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 6. | \$102 | 35.70 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 354. | FE | 0 | SAR | 1.819 |
| | | 8 | .20 | PB | 0 | NA | 80 |
| | | CD | 0 | LI | .067 | S04 | 191. |
| | | CA | 106.40 | MG | 24.48 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 654. |
| | | CĽ | 49.70 | HG | 0 | KJEL | .14 |
| | | CR | . 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .013 |
| | | COND | 980. | NO3 | 1.32 | PH | 7.45 |
| | | | | | | | |

| CASE | MO-DA-YR | | | | • | | | | |
|------|------------|----------|--------|---|------|---------|---|-----------|--------|
| | | | | | | | | | |
| 25 | 11/19/85 | ALK | 284. | | CU | 0 | | P04 | .41 |
| | | AL | 0 | | CN | 0 | | K | 7.58 |
| | | NH3 | .50 | | F | . 83 | | RESD | -1.808 |
| | | AS | .012 | | ALFA | 0 | | SE | .002 |
| | | 88 | .07 | | 8ETA | 6. | | \$102 | 34.57 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 346. | | FE | . 05 | | SAR | 1.349 |
| | | 8 | .17 | | PB | 0 | | NA | 60 |
| | | CD | 0 | ٠ | LI | .031 | | SD4 | 160. |
| | | CA | 114. | | MG | 21.80 | | SURF | 0 |
| | | C03 | 0 | | MH | 0 | | TDS | 509. |
| | | CL | 47. | | . HE | 0 | | KJEL | .95 |
| | | CR | .004 | | MO | ŏ . | | VA | .009 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | | COND | 912. | | NO3 | 1.23 | | PH | 7.40 |
| | | COND | 712. | | NUO | 1.25 | | rn | 7.40 |
| | | | | | | | | | |
| 26 | 02/19/86 | ALK | 279. | | CU | 0 | | P04 | .50 |
| | 02, 17, 00 | AL | 0 | | CN | Ŏ | | K | 7.90 |
| | • | NH3 | 1.40 | | F | .83 | | RESD | -1.710 |
| | | AS | .012 | | ALFA | 12. | | SE | 0 |
| | | BA | .08 | | BETA | 7. | | S102 | 35.30 |
| • | | 88 | 0 | | OH | . 0 | | AG | 0 |
| | | HCO3 | 340. | | FE | | | SAR | 1.504 |
| | | B | .27 | | PB | 0: 0 | | | 66 |
| | | | 0 | | | .07 | | NA CO4 | |
| | | CD Ca | | | LĪ | | | S04 | 160. |
| | | | 110.40 | | MG | 21.60 | | SURF | 0 |
| | | C03 | 0 | | MN | .02 | • | TOS | 620. |
| | | CL | 47. | | HG | 0 | | KJEL | 1.62 |
| | | CR | .002 | | MO | 0 | | VA | .002 |
| | | CO | 0 | | NI | 0 | | ZN | .006 |
| | | COND | 961. | | NO3 | 1.38 | | PH | 7.85 |
| | | | | | | | | | |
| 27 | 05/20/86 | ALK | 203. | | CU | 0 · | | P04 | .40 |
| | | AL | 0 | | CN | 0 | | K | 5.86 |
| | | NH3 | . 18 | - | F | . 91 | | RESD | -0.600 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .07 | | BETA | 7. | | \$102 | 35.03 |
| | | 8E | 0 | | OH | . 0 | | AG | 0 |
| | | HC03 | 247.6 | | FE | 0 | | SAR | 1.294 |
| | | В | .14 | | P8 | 0 | | NA | 50 |
| | | CD | 0 | • | LI | .057 | | S04 | 87. |
| | | CA | 67.60 | | MG | 15.60 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | TDS | 398. |
| | | CL | 36.30 | | HG | 0 | | KJEL | .35 |
| | | CR | 0 | • | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZH | . 0 |
| | | COND | 610. | | NO3 | 1.27 | | PH | 8.05 |

| | | | | - | | | |
|------|-------------------|------|----------------|--------|---------|----------|--------|
| CASE | HO-DA-YR | | | | | | |
| 28 | 11/06/86 | ALK | 206. | cu | 0 | P04 | . 41 |
| | ,, | AL | 0 | CN | 0 | K | 6.52 |
| | | NH3 | 0 | F | .76 | RESD | -0.656 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 6. | \$102 | 30.90 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 251.3 | FE | Õ | SAR | 1.308 |
| | | | | | 0 | NA NA | 46.49 |
| | | 8 | .13 | PB | .005 | S04 | 72. |
| | | CD | 0 72. | LI | | | |
| | | CA | | MG | 14.40 | SURF | 0 |
| | | C03 | 0 | MN | 0 | · TDS | 388. |
| | | CL | 50.80 | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .006 |
| | | COND | 600. | NO3 | 1.15 | PH | 8.00 |
| | | | | | | | |
| 29 | 0 3 /03/87 | ALK | 216. | CU | 0 | P04 | .33 |
| | . , | AL | 0 | CN | 0 | K | 6.85 |
| | | NH3 | .15 | F | .96 | RESD | -0.656 |
| | | AS | 0 | ALFA | 9. | SE | 0 |
| | | BA | .07 | BETA | 11. | \$102 | 32.39 |
| | | 8E | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 26 3 .5 | FE . | | SAR | 1.339 |
| | | В | .16 | PB | 0: 0 | NA | 48.55 |
| | | | | | .06 | . 504 | 91. |
| | | CD | 0 | £I | | SURF | |
| | | CA | 81.60 | MG | 11. | | 0 |
| | | C03 | 0 | MN | 0 | TDS | 410. |
| | | CL | 34. | HG | 0 | KJEL | .18 |
| | | CR | 0 | MO | | . VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 630. | NO3 | 1.02 | PH | 8.00 |
| | • | | | | | | |
| 30 | 05/06/87 | ALK | 230. | . CU | 0 | P04 | . 47 |
| | | AL | 0 | CN | 0 | . К | 7.07 |
| • | | NH3 | .08 | F | .81 | RESD | -1.084 |
| | | AS | .002 | ALFA - | 0 | SE | 0 |
| | | BA · | 07 | BETA | 7. | \$102 | 31.69 |
| | | 8E | 0 | НО | 0 | AG | 0 |
| | | HC03 | 281. | FE | 0 | SAR | 1.462 |
| | | В | .16 | PB | 0 | NA | 56.68 |
| | | CD | 0 | LI | .061 | \$04 | 118. |
| | | CA | 92.80 | MG | 12.90 | SURF | 0 |
| | | CO3 | 0 | · MN | 0 | TDS | 468. |
| | | CL | 39.90 | H6 | 0 | KJEL | .08 |
| | | CR | 0 | MO. | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | | | NO3 | 1.14 | PH | 7.80 |
| | • | COND | 730. | una | 1.14 | гп | 7.0V |

| CASE | MO-DA-YR | | | • | | | | |
|------|------------|------|-------------|----------|-------|---|-------|--------|
| 31 | 08/19/87 | ALK | 220. | CU | 0 | | P04 | .43 |
| | | AL | 0 | CN | 0 | | K | 5.84 |
| | | NH3 | . 07 | F | .92 | | RESD | -0.200 |
| | | AS | .01 | ALFA | 8. | | SE | 0 |
| | | 8A | .06 | BETA | 5. | | \$102 | 34.91 |
| | | 38 | 0 | OH | | | AG | 0 |
| | | HCO3 | 268. | FE | .02 | | SAR | 1.722 |
| | | В | .13 | PB | 0 | | NA | 60 |
| | | CD | 0 | LI | .06 | | S04 | 95. |
| | | CA | 62.43 | MG | 17.99 | | SURF | 0 |
| | | C03 | 0 | MN | 0 | | TDS | 412. |
| | | CL | 37. | HG | 0 | | KJEL | .10 |
| | | CR | 0 | MO | 0 | | VA | . 0 |
| | | CO | 0 / | NI | 0 | | ZN | 0 |
| | | COND | 650. | NO3 | 1.30 | | PH | 7.40 |
| | | | | | | | | |
| 32 | 10/13/87 | ALK | 172. | CU | 0 | | P04 | .11 |
| | , , | AŁ | 0 | CN | 0 | | K | 7.59 |
| | | NH3 | .08 | F | .82 | | RESD | -0.635 |
| | | AS | .004 | ALFA | 5. | | SE | 0 |
| | | BA | .08 | BETA | 6. | | \$102 | 37.30 |
| | | BE | 0 | OH - | - 0 | | AG | 0 |
| | | нсоз | 210. | FE | 0: × | | SAR | 1.311 |
| | | 8 | | PB | 0 | | NA | 43.03 |
| | • | CD | 0 | ĹĬ | .05 | • | S04 | 80. |
| | | CA | 52.72 | MG | 17.60 | | SURF | 0 |
| | | CO3 | 0 | MN | 0 | | TDS | 345. |
| | | CL | 33.50 | HG | Ö | | KJEL | .15 |
| | | CR | 0 | MO | Ŏ | | VA | 0 |
| | | CO | 0 | NI | 0 | | | 0 |
| | | | - | | | | ZN | |
| | | COND | 550. | NO3 | 1.21 | | PH | 7.50 |
| 33 | 03/16/88 | ALK | 203. | CU | 0 | | P04 | . 42 |
| ••• | 00, 20, 00 | AL | 0 | CN | Ö | | K | 6.26 |
| | | NH3 | .13 | F | .62 | | RESD | -1.797 |
| | | AS | .01 | ALFA | 0 | | SE | 0 |
| | | BA | .06 | BETA | 9. | | SI02 | 35.90 |
| | | BE . | 0 | 04 | 0 | | AG | 0 |
| | | HCO3 | 248. | FE | 0 | | SAR | 1.34 |
| | | В | .12 | PB | 0 | | NA | 54.90 |
| | | CD | | LI | .06 | | 504 | 154. |
| | | CA | .0 87.20 | MG | 18.40 | | SURF | 0 |
| | | CO3 | 0 | HH HH | | | TDS | 482. |
| | | | | | 0 | | KJEL | |
| | | CL | 36.70 | HG | 0 | | | 15 |
| | | CR | 0 | MO | 0 | | ۷A | .007 |
| | | COND | 740 | NI | 0 | | ZN | 0 |
| | | COND | 740. | NO3 | 1.12 | | PH | 7.60 |

| CASE | MO-DA-YR | | | | | , | |
|------|----------|-------|-------|------|--------------|--------|--------|
| 34 | 06/07/88 | ALK | 193. | cu | 0 | P04 | .32 |
| • | 00,00,00 | AL | 0 | CN | Ŏ | K. | 6.68 |
| | | NH3 | ŏ | F | .94 | RESD | -1.007 |
| | | AS | .009 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 0 . | \$102 | 37.28 |
| | | BE | 0 . | OH | 0 | AG | 0 |
| | | HCO3 | 235. | FE | 0 | SAR | 1.24 |
| | | | | PB | 0 | | |
| | | B | .12 | | | HA COA | 44.63 |
| | | CD | 0 | LI | .06 | S04 | 84. |
| | | CA | 92.80 | MG | 2.80 | SURF | 0 |
| | | C03 | 0 | HN | 0 | TDS | 410. |
| | | CL | 36.50 | HG | 0 | KJEL | 0 |
| | | CR - | 0 | MO | 0 | VA | .02 |
| | • | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 620. | HO3 | 2.20 | PH | 7.60 |
| | | | | | | | |
| 35 | 10/07/88 | ALK | 194. | CU | 0 | PO4 | . 48 |
| | - | AL | 0 | CN | 0 | K | 6.51 |
| , | | NH3 | 0 | F | .79 | RESD | -0.659 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 5. | SI02 | 32.85 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 237. | FE | 0 : * | SAR | 1.194 |
| | | 8 | .10 | P8 | 0 *. | NA | 41.38 |
| | | CD | 0 | LI | .06 | \$04 | 77. |
| | | CA | 81.60 | MG | 5.76 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 369. |
| | | CL | 34.90 | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | Ŏ | VA | Ö |
| | | CO | Ŏ | NI | Ŏ | ZN | 0 |
| | | | - | NO3 | .81 | PH | 8.10 |
| | | COND | 565. | NUS | .01 | rn | 0.10 |
| 36 | 03/23/89 | ALK | 193. | CU | 0 | P04 | .35 |
| | | AL | 0 | CN | 0 | K | 6.17 |
| | | NH3 | .06 | · F | . 96 | RESD | 1.63 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .06 | BETA | 0 | SIO2 | 34.67 |
| | | BE | 0 | НО | 0 | AG | 0 |
| | | HCO3 | 235. | FE | 0 | SAR | 1.159 |
| | | 8 | .11 | P8 | 0 | NA | 42.20 |
| | | CD | 0 | ĹĪ | .06 | S04 | 80. |
| | | CA | 81.60 | MG | 11.52 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 394. |
| | | CL | 48. | HG | Ŏ | KJEL | .08 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZH | . 0 |
| | | COND | 600. | H03 | 1.12 | PH | 7.55 |
| | | COULD | 000. | nus | 1,14 | FII | 7.33 |

| | | | | | - | | | | | |
|------|----------|------|-------|---|------|--------------|-----|---|-------|------------------|
| CASE | MO-DA-YR | | - | | | | | | | |
| 37 | 05/15/89 | ALK | 203. | | CU | 0 | | | P04 | .32 |
| | , , | AL | 0 | | CN | .005 | | | K | 6.82 |
| | | NH3 | 0 | | F | 1. | | | RESD | -0.583 |
| | | AS | 0 | | ALFA | 0 | | | SE · | 0 |
| | | BA | .07 | | BETA | 6. | | | \$102 | 34.13 |
| | | 8E | 0 | | OH | 0 | | | AG | 0 |
| | | HC03 | 248. | | FE | 0 | | | SAR | 1.374 |
| | | В | .11 | | 98 | 0 | | | NA | 48.18 |
| | | CD | 0 | | LI | .06 | , | | S04 | 83. |
| | | CA | 61.95 | | MG | 18.96 | | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | | TDS | 376. |
| | | CL | 37.10 | • | HG | 0 | | | KJEL | 0 |
| | | CR | 0 | | MB | 0 | | | VA | . 02 |
| | | CO | 0 | | NI | 0 | | | ZN | 0 |
| | | COND | 610. | | NO3 | 1.18 | | | PH | 7.85 |
| | | | | | | | | | | |
| 38 | 09/11/89 | ALK | 180. | | cu | 0 | | | P04 | .40 |
| | | AL | 0 | | CN | 0 | | | K | 6.15 |
| | | NH3 | .15 | | F | .85 | | | RESD | -0.89 0 7 |
| | | AS | .005 | | ALFA | 0 | | | SE | 0 |
| | | BA | . 06 | | BETA | 6. | | | SI02 | 34.88 |
| | | BE | 0 | | OH | 0 | | | AG | 0 |
| | | HC03 | 220. | | FE | 0 . ∼ | | | SAR | 1.32 |
| | | В | .14 | | PB | 0 | | | NA | 45.51 |
| | | CD | 0 | | LI | .06 | • • | | S04 | 90. |
| | | CA | 60.46 | | MG | 18.05 | | | SURF | 0 |
| | | CO3 | 0 | | MN | - 0 | | | TDS | 369. |
| | | CL | 37.50 | | HG | 0 | | | KJEL | .17 |
| | | CR | 0 | | MO | 0 | | | VA | 0 |
| | | CO | 0 | | NI | 0 | | | ZN | 0 |
| | | COND | 580. | | N03 | 1.18 | | | PH | 7.60 |
| | | | | | | | | | | |
| 39 | 10/11/89 | ALK | 194. | | cu | 0 | | | P04 | .26 |
| | | AL | 0 | | CN | 0 | | | K | 6.39 |
| | | NH3 | 0 | | F | .91 | | | RESD | -0.592 |
| | | AS | .008 | | ALFA | 0. | | | SE | 0 |
| | | BA | . 07 | | BETA | 4. | | | \$102 | 36.36 |
| | | BE | 0 | | OH | 0 | | | AG | 0 |
| | | HC03 | 237. | | FE | 0 | | | SAR | 1.291 |
| | | 8 | .10 | | PB | 0 | | | NA | 44.43 |
| | | CD | 0 | | LI | .06 | | - | S04 | 78. |
| | | CA | 59.76 | | MG | 18.20 | | | SURF | 0 |
| | | CO3 | 0 | | HN | 0 | | | TDS | 360. |
| | | CL | 33.50 | | HG | 0 | | | KJEL | 0 |
| | | CR | 0 | | MO | 0 | | | VA | 0 |
| | | CO | 0 | | NI | 0 | | • | ZN | 0 |
| | | COND | 550. | | NO3 | 1.14 | | | PH | 7.30 |
| | | | | | | | | | | |

WELL #4 - CHEMICAL ANALYSES

| CASE | HO-DA-YR | | | | | | |
|------|----------|------|-------|------|---------------|-----------|--------|
| 40 | 03/26/90 | ALK | 202. | CU | 0 | PO4 | .35 |
| • | | AL | 0 | CN | 0 | K | 6.13 |
| | | NH3 | .05 | F | .74 | RESD | -0.467 |
| | | AS | .009 | ALFA | 0 | SE | 0 |
| | | 8A | .07 | BETA | 7. | SI02 | 33.68 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 246. | FE | 0 | SAR | 1.285 |
| | | В | .09 | Р8 | 0 | NA | 44.33 |
| | | CD | 0 | LI | .06 | \$04 | 71. |
| | | CA | 61.71 | MG | 17.29 | SURF | 0 |
| | | C03 | 0 | MN . | 0 | TDS | 384. |
| | | CL | 35. | HG | 0 | KJEL | . 05 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 · | NI | 0 | ZN | 0 |
| | | COND | 594. | NO3 | 1.01 | РН | 8.00 |
| | | | | | _ | •• | |
| 41 | 07/05/90 | ALK | 199. | CU | 0 | P04 | .41 |
| | | AL | 0 | CN | 0 | . К | 6.35 |
| | | NH3 | .14 | F | .99 | RESD | -0.549 |
| | | AS | .006 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 5. | \$102 | 34.90 |
| | | BE | 0 | ОН | · 0 | AG | 0 |
| | | HCO3 | 243. | FE | . '0,7 | SAR | 1.408 |
| | | В | .10 | PB | 0 | NA | 48.74 |
| | | CD | 0 | LI | .06 | \$04 | 92. |
| | | CA | 60.44 | . MG | 18.45 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 460. |
| | | CL | 40.90 | HG | 0 | KJEL | .53 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | . 0 | HI | 0 | ZN | 0 |
| | | COND | 503. | NO3 | 1.15 | PH | 7.51 |
| 42 | 10/18/90 | ALK | 205. | CU | .03 | P04 | . 35 |
| | | AL | .07 | CN | 0 | K | 6.05 |
| | • | NH3 | .04 | F | .90 | RESD | -0.610 |
| | | AS | .022 | ALFA | 0 | SE | 0 |
| | | BA | .066 | BETA | 0 | \$102 | 41.10 |
| | | BE | .001 | OH | 0 | AG | 0 |
| | | HCO3 | 250. | FE | .06 | SAR | 1.36 |
| | | 8 | .12 | PB | .003 | NA - | 47.32 |
| | | CD | 0 | LI | .07 | \$04 | 89. |
| | | CA | 63.84 | MG | 18.56 | SURF | 0 |
| | | C03 | 0 | HN | 0 | TDS | 462. |
| | | CL | 34.10 | HG | 0 | KJEL | 1.75 |
| | | CR | 0 | HO - | Ō | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .08 |
| | | COND | 516. | NO3 | 1.12 | PH | 7.60 |
| | | | | | - | | |

WELL #4 - CHEMICAL ANALYSES

| AVERAGES | 02/15/7 | 78 TO 01/09/91 | | | | |
|----------|---------|----------------|------|--------|-------|---------|
| | ALK | 248.7 | CU | .005 | PO4 | . 257 |
| | AL | .031 | CN | .002 | K | 7.239 |
| | NH3 | .24 | F | .839 | RESD | -21.871 |
| | AS | .005 | ALFA | 1.5 | SE | .00 |
| | BA | .082 | BETA | 5.4 | \$102 | 34.854 |
| | BE | .00 | OH | 0 | AG | 0 |
| | HCO3 | 304.4 | FE | .015 | SAR | 1.594 |
| | 8 | .144 | PB | .004 | · NA | 58.92 |
| | CD | .00 | ŁI | .057 | \$04 | 150. |
| | CA | 89.31 | MS | 22.461 | SURF | 0 |
| | C03 | 0 | MN | .003 | TDS | 539. |
| | CL | 42.89 | HG | .0001 | KJEL | .427 |
| | CR | .002 | MO | .002 | ٧A | .004 |
| | . co | .001 | NI | .001 | ZN | .007 |
| | COND | 815 | NO3 | 1 031 | PH | 7.59 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|------|-----------|-------|-------|
| 1 - | 02/23/78 | ALK | 180. | CU | .01 | P04 | .02 |
| | | AL | .08 | CN | | K | 5.28 |
| | | NH3 | 0 | F | .88 | RESD | |
| | | AS | 0 | ALFA | 8. | SE | 0 |
| | | BA | .05 | BETA | 10. | \$102 | 35. |
| | | 8E | | OH | | AG | 0 |
| | | HCO3 | 219.6 | FE | .06 | SAR | 1.213 |
| | | 8 | .12 | P8 | 0 | NA | 39.50 |
| | | CD | 0 | LI | 0 | S04 | 70. |
| | | CA | 52. | MG | 17.28 | SURF | 0 |
| | | C03 | | MN | .01 | TDS | 324. |
| | | CL | 32. | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | • | VA | .08 |
| | | CO | .026 | NI | 0 | ZN | . 04 |
| | | COND | 500. | NO3 | .54 | PH | 7.79 |
| | | •••• | | 1100 | | (1) | 1.77 |
| | | | | • | | | |
| 2 | 05/03/78 | ALK | 180. | CU | .03 | P04 | .03 |
| | | AL | .07 | CH | 0 | K | 6.24 |
| | | NH3 | .0 | F , | 1. | RESD | |
| | | AS | 0 | ALFA | 9. | SE | 0 |
| | | BA | .12 | BETA | 17. | \$102 | 34. |
| | | BE | | OH | ٠. | AG | 0 |
| | | HC03 | | FE | 5.05 | SAR | |
| | • | В | .11 | PB | .003 | NA | |
| - | | CD | .001 | LI | 0 | S04 | 76. |
| | | CA | 56. | MG | 33.60 | SURF | 0 |
| | | C03 | | нн | .02 | TDS | 357. |
| | | CL | 50. | HG | 0 | KJEL | 0 |
| | | CR | 0 | HO | • | VA | ٧ |
| | | CO | .002 | NI | 0 | | A1./ |
| | | COND | 550. | NO3 | .73 | ZN | .016 |
| | | COND | 330. | cun | .73 | PH | 7.29 |
| 3 | 10/13/78 | ALK | 192. | CU | 0 | P04 | 00 |
| · | 10/10/10 | AL | .02 | CN | 0 | K | .02 |
| | | NH3 | 0 | F | 1.08 | RESD | 7.18 |
| | | AS | Ō | ALFA | | | ۸ |
| | | BA | .09 | | 3. | SE | 0 |
| | | BE | .07 | BETA | 6. | \$102 | 33. |
| | | HCO3 | | 0H | 0 | AG | 0 |
| | | | 17 | FE | | SAR | 1.228 |
| | | B | .16 | PB | .002 | NA | 42.30 |
| | | CD | 0 | LI | .02 | 504 | 85. |
| | | CA | 62.40 | MG | 16.80 | SURF | 0 |
| | | C03 | ** | MN | .02 | TDS | 365. |
| | | CL | 32. | HG | 0 | KJEL | 0 |
| | | CR | 0 | HO | | VA | .06 |
| | | CO | 0 | HI | 0 | ZN | .033 |
| | | COND | 555. | NO3 | .80 | PH | 6.93 |

| CASE | MO-DA-YR | | | | | | |
|------|----------|------------|-------|------------|-------|-------------|-------|
| 4 | 06/01/79 | ALK | 196. | CU | .003 | P04 | 0 |
| | . , | AL | .01 | CH | 0 | K | 6.90 |
| | | NH3 | 0. | F | 1. | RESD | |
| | | AS | .004 | ALFA | 4. | SE | .001 |
| | | BA | .09 | 8ETA | 8. | \$102 | 39. |
| | | 88 | .001 | OH | | AG | 0 |
| | | HC03 | | FE | .01 | SAR | 1.114 |
| | | В | .165 | PB | . 0 | NA | 42.39 |
| | | CD | .001 | LI | .057 | S 04 | 74. |
| | | CA | 62.40 | MG | 28.80 | SURF | 0 |
| | | C03 | | MM | 0 | TDS | 370. |
| | | CL | 30, | .HG | 0 | KJEL | .10 |
| | | CR | .003 | # 0 | 0 | VA | 0 |
| | | C O | .003 | NI | 0 | ZN | .003 |
| • | | COND | 570. | N03 | .04 | PH | 7.76 |
| r | 00/10/70 | A1 W | .00 | | 200 | 004 | 47 |
| 5 | 09/10/79 | ALK | 198. | CU | .009 | P04 | .07 |
| | | AL | .06 | CN | 0 | K | 6.48 |
| | | NH3 | 0 | F | . 92 | RESD | ^ |
| | | AS | .004 | ALFA | 2. | SE | . 0 |
| | | BA | . 06 | BETA | 10. | \$102 | 34. |
| | | BE | 544.5 | OH | | AG | 0 |
| | | HCO3 | 241.5 | FE | .04 | SAR | 1.129 |
| | • | В | • | PB | U | NA 204 | 46 |
| | | CD | 0 | LI | .058 | S04 | 68. |
| | • | CA | 78.40 | MG | 28.80 | SURF | 0 |
| | | CD3 | *. | MN | .006 | TDS | 359. |
| | | CL | 34. | H6 | 0 | KJEL | .10 |
| | | CR | .007 | MO | Ā | VA | 0 |
| | | CO | .025 | NI | 0 | ZN | .015 |
| | | COND | 550. | N03 | .54 | PH | 7.40 |
| 6 | 04/28/80 | ALK | 190. | . CU | 0 | P04 | .20 |
| | | AL | .05 | CN | .002 | K | 6.30 |
| | | NH3 | 0 | F | .99 | RESD | |
| | | AS | 0 | ALFA | 2.4 | SE | 0 |
| | | 8A | . 265 | BETA | 10. | \$102 | 33.50 |
| | | BE | 0 | OH · | | AG | 0 |
| | | HC03 | 231.8 | FE | .02 | SAR | 1.174 |
| | | В | .13 | PB | 0 | NA | 38.80 |
| | | CD | 0 | LI | . 057 | \$04 | 54. |
| | | CA | 59.20 | MG | 14.40 | SURF | 0 |
| | | C03 | | MN | 0 | TDS | 460. |
| | | CL | 36. | HG | 0 | KJEL | 0 |
| | | CR | 0 | HO | 0 | VA | .002 |
| | | CO | .003 | NI | 0 | ZN | .0 |
| | , | COND | 700. | NO3 | 0 | PH | 7.30 |

| CASE | MO-DA-YR | | | | | | |
|------|------------|------|-------------|-------|----------|-------------|--------------|
| 7 | 07/23/80 | ALK | 206. | CU | .01 | P04 | .49 |
| | | AL | 0 | CN | 0 | K | 5.90 |
| | | NH3 | 0 | F | .81 | RESD | |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA | .08 | BETA | 0 . | SI02 | 33.90 |
| | | 8E | 0 | HO | | AG | 0 |
| | | HCO3 | 231.3 | FE | .12 | SAR | 1.277 |
| | | 8 | .10 | PB | 0 | NA | 43 |
| | | CD | .002 | LI | . 058 | 504 | 66. |
| | | CA | 56. | MG | 18.24 | SURF | 0 |
| | | C03 | | MN | .011 | TDS | 350 . |
| | | CŁ | 32. | HG | 0 | KJEL | 0 |
| | | CR | .004 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | COND | 540. | NO3 | .62 | PH | 7.90 |
| | | | | | | | |
| 8 | 12/10/80 | ALK | 210. | cu | .01 | P04 | .06 |
| | | AL | 0 | CN | 0 | K | 5.30 |
| | | NH3 | 0 | F | .64 | RESD | |
| | | AS | .003 | ALFA | 2. | SE | 0 |
| | | BA | .075 | BETA | 12. | \$102 | 33. |
| | | BE | 0 | OH | | AG | 0 |
| | | HCO3 | 256.2 | FE | .02 0 | SAR | 1.271 |
| | | 8 | .13 | PB | 0 🖟 | NA | 43 |
| | | CD | 0 | LI | .057 | S0 4 | 56. |
| | | CA | 61.60 | MG | 15.36 | SURF | 0 |
| | | C03 | | MM | 0 | TDS | 320. |
| | | CL | 27.50 | HG | 0 | KJEŁ | .15 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | .004 | NI | · 0 | ZN | .005 |
| | | COND | 490. | NO3 | .92 | PH | 7.30 |
| 9 | 03/23/81 | ALK | 204. | CU | 0 | P04 | . 28 |
| .* | 00, 20, 01 | AL | .04 | CN | Ŏ | X | 6.60 |
| | | NH3 | 0 | F | 1.02 | RESD | 0.00 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA | .085 | BETA | 1.5 | \$102 | 32. |
| | | 8E | 0 | ОН | 110 | AG | 0 |
| | | HC03 | 248.8 | FE | .01 | SAR | 1.30 |
| | | 8 | .11 | PB | .001 | NA | 44.80 |
| | | CD | .001 | LI | .06 | S04 | 65. |
| | | CA | 69.60 | HG F1 | 12.48 | SURF | 0 |
| | | C03 | | MN | .007 | TDS | 357. |
| | | CL | 37.40 | не | 0 | KJEL | 0 |
| | | CR | 0 | MO | Ö | VA | Ö |
| | | CO | 0 | NI | 0 | ZN | .01 |
| • | | COND | 550. | H03 | 1.17 | PH | 7.80 |
| | | | | | | | |

WELL #5 - CHEMICAL ANALYSES

| CASE | MO-DA-YR | | | | | | • | | |
|------|----------|-------|-------|---|------|-------|---|-------|--------|
| 10 | 10/20/81 | ALK | 204.6 | | CU | .002 | | P04 | .20 |
| | | AL | .033 | | CN | 0 | | K | 6.30 |
| | | NH3 | .27 | | F | . 94 | | RESD | -0.678 |
| | | AS | .004 | | ALFA | 0 | | SE | 0 |
| | | BA | .09 | | BETA | 0 | | \$102 | 39.60 |
| | | 38 | 0 | | OH | 0 | | AG | 0 |
| | | HCO3 | 249.6 | | FE | .015 | | SAR | 1.216 |
| | | В | .116 | | 98 | .002 | | NA | 43.20 |
| | | CD | 0 | | LI | .08 | | S04 | 76. |
| | | CA | 60. | | MG | 21.60 | | SURF | 0 |
| | | CO3 | 0 | • | MN. | .01 | | TDS | 380. |
| | | CL | 38.10 | | HG | 0 | | KJEL | .50 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | .009 |
| | | COND | 500. | | NO3 | .42 | | PH | 7.80 |
| | | | | | | | | | |
| 11 | 03/10/82 | ALK ' | 190.4 | | CU | .01 | | P04 | .07 |
| | | AL | 0 | | CN | .01 | | K | 6.10 |
| | | NH3 | .08 | | F | .86 | | RESD | -0.450 |
| | | AS | .004 | | ALFA | 0 | • | SE | 0 |
| | | BA | . 075 | | BETA | 0 | | SI02 | 34.50 |
| | | BE | 0 | | OH . | . 0 | | AG. | 0 |
| | | HCO3 | 232.2 | | FE | .005 | | SAR | 1.326 |
| | | В | .105 | | PB | 0 | | NA | 31 |
| | | CD | 0 | | LI | 0 | | S04 | 51. |
| | | CA | 59. | | MG | 16. | | SURF | 0 |
| | | C03 | 0 | • | MN | 0 | | TDS | 315. |
| | | CL | 32.30 | | HG | 0 | | KJEL | .13 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | ō | | NI | 0 | | ZN | .005 |
| | | COND | 480. | | NO3 | .71 | | PH | 7.40 |
| | | | | | | | | | |
| 12 | 05/17/82 | ALK | 169.2 | | CU | 0 | | P04 · | .19 |
| | | AL | 0 | | CN | .007 | | X | 5.50 |
| | | NH3 | . 60 | | F | .95 | | RESD | -1.048 |
| | | AS | - 006 | | ALFA | 1.9 | | SE | 0 |
| | | BA | .07 | | BETA | 2. | | S102 | 33.70 |
| | | 8E | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 206.4 | | FE | .005 | | SAR | 1.30 |
| | | В | .095 | | P8 | .002 | | NA | 44.50 |
| | • | CD | 0 | | LI | 0 | | S04 | 100. |
| | | CA | 60. | | MG | 17.50 | | SURF | 0 |
| | | CO3 | 0 | | MN | .001 | | TDS | 371. |
| | | CL | 32.50 | | HG | 0 | | KJEL | .75 |
| | | CR | .001 | | MO | 1 0 | | VA | 0 |
| | | CO | . 0 | | NI | .015 | | ZN | .011 |
| | | COND | 560. | | NO3 | .89 | | PH | 7.90 |
| | | | | | | | | | |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|-------|-------|-------|--------|
| 13 | 08/26/82 | ALK | 188. | CU | 0 | P04 | .26 |
| | | AL | 0 | CN | 0 . | K | 6.60 |
| | | NH3 | 1.29 | F | i. | RESD | -0.500 |
| | | AS | .003 | ALFA | 2. | SE | 0 |
| | | BA | .08 | BETA | 2.1 | \$102 | 37.43 |
| | | 38 | 0 | НО | 0 | AG | 0 |
| - | | HCO3 | 229. | FE | . 02 | SAR | 1.312 |
| | | 8 | .11 | P8 | . 0 | NA | 44 |
| | | CD | 0 | LI | .059 | \$04 | 90. |
| | | CA | 58.40 | MG | 16.32 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 358. |
| | | CL | 30.50 | HG | 0 | KJEL | 1.40 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .004 |
| | | COND | 550. | NO3 | .54 | PH | 7.80 |
| 14 | 12/08/82 | ALK | 188.7 | CU | 0 | P04 | . 20 |
| | , , | AL | 0 | CN | 0 | K | 6.30 |
| | | NH3 | . 28 | F | .94 | RESD | . 402 |
| | | AS | .004 | ALFA | | SE | 0 |
| | | BA | .07 | BETA | • | SI02 | 31.50 |
| | | BÉ | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 230.2 | FE | .01 | SAR | 1.294 |
| | | 8 | .10 | PB | 0 | NA | 43 |
| | | CD | 0 | ŁI | .057 | S04 | 84. |
| | | CA | 57.60 | Me | 15.84 | SURF | 0 |
| | | CO3 | 0 | HN | 0 | TDS | 350. |
| | | CL | 27.40 | He | .0002 | KJEL | . 46 |
| | | CR | .002 | MD | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .023 |
| | | COND | 540. | . NO3 | 1.08 | PH | 7.70 |
| 15 | 02/22/83 | ALK | 192.6 | CU | 0 | P04 | .24 |
| | 01/11/00 | AL | . 0 | CN | 0 | K | 6.3Ò |
| | | NH3 | .10 | F | .99 | RESD | -0.126 |
| | | AS | .005 | ALFA | 2. | SE | 0 |
| | | BA | .10 | BETA | 1.4 | SIO2 | 31.50 |
| | | 8E | . 0 | ОН | 0 | AG | 0 |
| | | HC03 | 234.9 | FE - | .01 | SAR | 1.341 |
| | | В | .10 | PB | 0 | NA | 43.50 |
| | | CD | 0 | LI | .055 | S04 | 72. |
| | | CA | 54.40 | MG | 15.36 | SURF | 0 |
| | | CO3 | 0 | MN | .004 | TDS | 345. |
| | | CL | 26.80 | HG | 0 | KJEL | .22 |
| | | CR | .002 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .003 |
| | | COND | 530. | NO3 | .84 | PH | 7.50 |

| CASE | MO-DA-YR | | | | - | | | | |
|------|----------|------|-------|---|------|-----------|---|------|--------|
| 16 | 05/27/83 | ALK | 188. | | CU | 0 | | P04 | .12 |
| | | AL | .46 | | CN | .02 | • | K | 6.40 |
| | | NH3 | .11 | | F | .94 | | RESD | -0.336 |
| | | AS | .004 | | ALFA | 0 | | SE | 0 |
| | | BA. | .08 | | BETA | 12.3 | | SI02 | 31.20 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HCO3 | 229.4 | | FE | .01 | | SAR | 1.367 |
| | | В | .12 | | PB | 0 | | NA | 45 |
| | | CD | 0 | | LI | . 057 | | 504 | 80. |
| | | CA | 57.60 | | MG | 14.88 | | SURF | 0 |
| | | CO3 | 0 | | MN | .001 | | TDS | 365. |
| | | CL | 32. | | HG | .0002 | | KJEL | .12 |
| | | CR | .002 | | MD | . 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | .002 |
| | | COND | 550. | | N03 | .08 | | PH | 7.80 |
| | | | | | | | | | |
| 17 | 08/17/83 | ALK | 204. | | CU | .005 | | P04 | .15 |
| | | AL | 0 | | CN · | .004 | | K | 6.50 |
| | | NH3 | . 30 | | F | . 97 | | RESD | .092 |
| • | | - AS | .003 | | ALFA | 0 | | SE | 0 |
| | | BA ` | . 088 | | BETA | 1.4 | | SI02 | 31.50 |
| | | BE | 0 | | ОН | . 0 | | AG | 0 |
| | | HCO3 | 248.8 | • | FE | | | SAR | 1.746 |
| | | 8 | .14 | | PB | 01 | | NA | 58 |
| | | CD | 0 | | LI | .045 | | S04 | 74. |
| | | CA | 48. | | MG | 21.60 | | SURF | 0 |
| | | C03 | 0 | | MN | .003 | | TDS | 388. |
| | | CL | 50. | | HE | 0 | | KJEL | .75 |
| | • | CR | .002 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | ŏ | | ZN | .004 |
| | | COND | 590. | | NO3 | .10 | | PH | 7.60 |
| | | | | | | | | | |
| 18 | 11/08/83 | ALK | 170. | | CU | .004 | | P04 | .14 |
| • | | AL | .016 | | CN | .005 | | K | 5.40 |
| | | NH3 | .25 | | F | .92 | | RESD | -0.605 |
| | | AS | .005 | | ALFA | 0 | | SE | 0 |
| | | BA | .065 | | BETA | 2.4 | | SI02 | 32.10 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HCO3 | 207.4 | • | FE | .018 | | SAR | 1.211 |
| | | В | .10 | | PB | 0 | | NA | 39.40 |
| | | CD | 0 | | LI | .05 | | S04 | 75. |
| | | CA | 46. | | MG | 20.80 | | SURF | 0 |
| | | CO3 | 0 | | MN | .005 | | TDS | 380. |
| | | CL | 30. | | HG | 0 | | KJEL | .40 |
| | | CR | .003 | | MD | 0 | | VA | .01 |
| | | CO | 0 | | NI | 0 | | ZN | .003 |
| | | COND | 510. | | NO3 | .10 | | PH | 7.60 |
| | | | | | | - | ٠ | | |

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|-------|---|------|-------|--------------|--------|
| | | A W | 100 | | 011 | | | 4.8 |
| 19 | 03/22/84 | ALK | 189. | | CV | 0 | P04 | .10 |
| | | AL | 0 | | CN | 0 | K | 5.40 |
| | | NH3 | | | F | .87 | RESD | 2.054 |
| | | AS | .003 | | ALFA | 0 | SE | 0 |
| | | BA | .06 | | BETA | 0 | \$102 | 32.40 |
| | | BE | 0 | | 0H | 0 | AG | 0 |
| | | HCO3 | 230.5 | | FE | .01 | SAR | .95 |
| | | 8 | .10 | | PB | .10 | NA SOA | 39 |
| | | CD | 0 | | LI | .06 | S04 | 150. |
| | | CA | 54. | | MG | 44.16 | SURF | 0 |
| | | C03 | 0 | | MN | .01 | TD\$ | 450. |
| | | CL | 40. | | , HG | 0 | KJEL | .30 |
| | | CR | .002 | • | MO | 0 | VA | .03 |
| | | CO | 0 | | NI | 0 | ZN | 0 |
| | | COND | 690. | | NO3 | . 94 | PH | 7.70 |
| | | • | • | | | | | |
| 20 | 08/15/84 | ALK | 189. | | CU | 0 . | P04 | .08 |
| | | AL | 0 | | CN | 0 | K | 5.85 |
| | | NH3 | .21 | | F | .93 | RESD | -1.885 |
| | | AS | .005 | • | ALFA | 0 | SE | 0 |
| | | BA | .08 | • | BETA | 0 | \$102 | 30.30 |
| | | 8 E | 0 | • | OH | . 0 | AG | 0 |
| | | HCO3 | 230.6 | | FE | .02 | SAR | 1.473 |
| | | В | . 152 | | PB | . 125 | NA | 57 |
| | | CD | 0 | | LI | .055 | S04 | 130. |
| | | CA | 76. | | MG | 22.80 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 560. |
| | | CL . | 60. | | HG | 0 | KJEL | .33 |
| | | CR | 0 | | MO | .05 | VA | .018 |
| | | CO | 0 | | NI | .01 | · ZN | .007 |
| | | COND | 850. | | NO3 | .99 | PH | 7.90 |
| | | | | | | | | |
| 21 | 11/12/84 | ALK | 178. | | CU | 0 | P04 | 1.02 |
| - | , - , | AL | 0 | | CN | 0 . | K | 6.02 |
| | | NH3 | .25 | | F | .84 | RESD | -0.420 |
| | | AS | .003 | | ALFA | 0 | SE | . 0 |
| | | BA | .08 | | BETA | 6. | SI02 | 37.25 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| • | | HC03 | 217.2 | | FE | .02 | SAR | 1.573 |
| | • | В | .116 | | PB | .033 | NA | 51 |
| | • | CD | 0 | | LI | .059 | S 0 4 | 65. |
| | | CA | 70.40 | | MG | 5.70 | SURF | 0 |
| | | CO3 | 0 | | MM | 0 | TDS | 370. |
| | | CL | 50. | | HG | 0 | KJEL | .35 |
| | | CR | 0 | | MO | .01 | VA | .011 |
| | | CO | 0 | | NI | 0 | ZN | .005 |
| | | COND | 570. | | NO3 | 1. | PH | 8.08 |
| | | | | | | | | |

WELL #5 - CHEMICAL ANALYSES

| CASE | MO-DA-YR | | | | - | | | | |
|------|----------|--------------|-------|-----|------|--------|---|------------|--------------|
| 22 | 02/25/85 | ALK | 183. | | CU | 0 | | 904 | .04 |
| | | AL | 0 | | CN | 0 | | K | 6.20 |
| | | NH3 | 0 | | F | .92 | | RESD | -2.127 |
| | | AS | .003 | | ALFA | 0 | | SE | 0 |
| | | BA | .08 | | BETA | 0 | | \$102 | 36.96 |
| | | 38 | . 0 | | CH | 0 | • | AG | 0 |
| | | HCO3 | 223. | | FE | 0 | | SAR | 1.155 |
| | | В | .13 | • | PB | 0 | | NA | 41.80 |
| | | CD | 0 | | LI | .06 | | \$04 | 108. |
| | | CA | 68.60 | • | MG | 18.60 | • | SURF | 0 |
| | | C O 3 | 0 | | MN. | 0 | | TDS | 395 . |
| | | CL | 33. | | HG | 0 | | KJEL | .10 |
| | | CR | 0 | | MO | .03 | | VA | . 0 |
| | • | CO | 0 | | NI . | 0 | | ZN | .003 |
| | | COND | 600. | | NO3 | 1. | | PH | 7.50 |
| | | | | | | | | | |
| 23 | 06/17/85 | ALK | 182. | • | CU | 0 | | P04 | . 23 |
| | | AL | .21 | | CN | 0 | | K | 6.30 |
| | | NH3 | 0 | | F | .87 | | RESD | -0.461 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | 8A | . 08 | | BETA | 7. | | \$102 | 32.01 |
| | | 38 | 0 | | OH | , 0 | | AG | 0 |
| | | HC03 | 222. | . • | FE | ٥٠ - (| | SAR | 1.185 |
| | | В | .17 | | PB | . 004 | | NA | 39 |
| | | CD | 0 | | LI | .057 | • | S04 | 67. |
| | | CA | 61.60 | | MG | 12.50 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | TDS | 376. |
| | | CL | 34.90 | | HG | 0 | | KJEL | 0 |
| | | CR | 0 | | MO | . 01 | | ٧A | .003 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | · | COND | 563. | | NO3 | 5.40 | | PH | 7.85 |
| | | | | | | | | | |
| 24 | 08/19/85 | ALK | 182. | | CU | 0 | | P04 | .06 |
| | • | AL | 0 | | CN | 0 | | K | 4.30 |
| | | NH3 | .10 | | F | .99 | | RESD | -33.800 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 - |
| | | BA | .07 | | BETA | 4. | | \$102 | 32.19 |
| | | 8E | 0 | | OH | 0 | | AG | 0 |
| | | HCO3 | 222. | | FE | .03 | | SAR | 1.357 |
| | | 8 | .14 | | PB | .005 | | NA | 44 |
| | | CD | 0 | | LI | .052 | | S04 | 69. |
| | | CA | 57.60 | | MG | 13.44 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | TDS | 360. |
| | | CL | 35.20 | | HG | 0 | | KJEL | .15 |
| | | CR | 0 | | MO | 0 | | ۷A | 0 |
| | | CO | 0 | | NI | 0 | | ZN | .017 |
| | | COND | 550. | | NO3 | 1.09 | | PH | 7.80 |

| CASE | MO-DA-YR | | | ٠ | • | | | |
|------|----------|-------|-------|---|------|------------|-------|---------|
| 25 | 11/19/85 | ALK | 141. | | CU | 0 | P04 | 0 |
| | | AL | .02 | | CN | 0 | K | 5.20 |
| | | nh3 | 0 | | F | .98 | RESD | -1.141 |
| | | AS | 0 | • | ALFA | 0 | SE | 0 |
| | | BA | .07 | | BETA | 4. | \$102 | 31.15 |
| | | BE | 0 | | CH | 0 | AG | 0 |
| | | HC03 | 172. | | FE | 0 | SAR | 1.215 |
| | | 8 | .11 | | PB . | 0 | NA | 39.30 |
| | | CD | 0 | | LI | . 052 | S04 | 95. |
| | | CA | 56. | | MG | 14.20 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 348. |
| | | CL | 31.50 | | HG . | 0 . | KJEL | 0 |
| | | CR | 0 | | MO | 0 | VA | .007 |
| | | CO | 0 | | NI | 0 | ZN | 0 |
| | | COND | 518. | | NO3 | 1.01 | PH | 7.75 |
| - | | | | | | | | |
| 26 | 02/19/86 | ALK | 179. | | CU | 0 | P04 | .08 |
| | | AL | 0 | | CN | 0 | K | 5.37 |
| | | NH3 | .42 | • | F | .96 | RESD | -4.280 |
| | | AS . | .003 | | ALFA | 4. | SE | 0 |
| | | BA | .07 | | BETA | 6. | SI02 | - 30.86 |
| | | BE | 0 | | OH | ·. 0 | AG | 0 |
| | | HCO3 | 218. | | FE | 0 . | SAR | 1.248 |
| | | В | .17 | | PB | .003 | NA | 40.60 |
| | | CD | . 0 | | LI | .052 | S04 | 63. |
| | | CA | 61.60 | | MG | 11.30 | SURF | 0 |
| | | C03 | 0 | | MN | .02 | TDS | 358. |
| | | CL | 34.30 | | HG | 0 | KJEL | .65 |
| | | CR | 0 | | MO | 0 | VA | . 0 |
| | | CO CO | Ŏ | | NI | Ö | ZN | Ö |
| | | COND | 574. | | NO3 | 1.27 | PH | 8.08 |
| | | | | | | | | |
| 27 | 05/20/86 | ALK | 179. | - | CU | 0 | P04 | .18 |
| | | AL | 0 . | | CN | 0 | K | 5.24 |
| | | NH3 | .14 | | F | .94 | RESD | -0.480 |
| | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | . 07 | | BETA | 5. | \$102 | 35.40 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 218. | | FE ' | 0 | SAR | 1.222 |
| | | В | .12 | | P8 | 0 | NA | 40 |
| | | CD | 0 | | LI | .05 | 504 | 63. |
| | | CA | 57.20 | | MG | 14.60 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 289. |
| | | CL | 33.20 | | HG | 0 | KJEL | .20 |
| | | CR | 0 | | MO | Ö | VA | 0 |
| | | CO | Ō | | HI | .05 | ZN | Ö |
| | | COND | 435. | | NO3 | 1.15 | PH | 8.00 |

WELL \$5 - CHEMICAL ANALYSES

| CASE | MO-DA-YR | - | | | • | | | |
|------|----------|-----------|-------|---|-------------|--------------|---------------|--------|
| 28 | 07/07/86 | ALK | 188. | | CU | .02 | P04 | .15 |
| | , . | AL | .12 | | CN | .005 | K | 5.73 |
| | | NH3 | .04 | | F | .87 | RESD | -0.379 |
| | | AS | 0 | | ALFA | 0 | SE | . 0 |
| | | BA | 08 | | BETA | 0 | SI 0 2 | 30.12 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 229.4 | | FF | .10 | SAR | 1.436 |
| | | 8 | .15 | | PB (| 0 | NA | 47.50 |
| | | CD | 0 | • | LI | . 052 | \$04 | 73. |
| | | CA | 57.60 | | MG | 15.40 | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | TDS | 352. |
| | | CL | 42.20 | | He | 0 | KJEL | .10 |
| | | CR | . 0 | | HO | 0 | VA | 0 |
| | | CO | .009 | | NI | 0 | ZN | .03 |
| | | COND | 550. | | NO3 | 1.06 | PH | 7.90 |
| | | | | | | | | |
| 29 | 11/06/86 | ALK | 170. | | CU | 0 | P04 | .08 |
| | | AL | 0 | | CN | 0 | K | 5.95 |
| | | NH3 | 0 | | F | .86 | RESD | -0.455 |
| | | AS | 0 | | ALFA | 0 . | SE | 0 |
| | | BA | . 07 | | BETA | 4. | \$102 | 29.30 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 207.4 | | FE | 0 | SAR | 1.207 |
| | | В | .15 | | PB | 0 % | NA | 38.53 |
| | | CD | 0 | | LI | .062 | \$04 | 62. |
| | | CA | 55.20 | | MG | 13.40 | SURF | 0 |
| | | CO3 | 0 | | MM | 0 | TDS | 345. |
| | | CL | 38.90 | | HG | Ŏ | KJEL | . 0 |
| | | CR | 0 | | #0 | Ŏ | VA | 0 |
| | | CO | 0 | | NI | Ö | ZN | .007 |
| | | COND | 500. | | NO3 | 1.55 | PH | 8.40 |
| - | - | | | | | | | |
| 30 | 03/03/87 | ALK | 182. | | cu | 0 | P04 | .17 |
| | | AL | 0 . | | CN | 0 | • Х | 6.07 |
| | | NH3 | .17 | | F | 1.02 | RESD | -0.575 |
| | | AS | 0 | | ALFA | 10. | SE | 0 |
| | | BA | .07 | | BETA | 7. | \$102 | 31.05 |
| | | 8E | 0 | • | OH | 0 | AG | 0 |
| | | HCO3 | 222. | | FE | 0 | SAR | 1.211 |
| | | 8 | .13 | | PB | 0 | NA | 40.41 |
| | | CĐ | .002 | | LI | .05 | \$04 | 68. |
| | | CA | 68. | | MG | 10. | Surf | 0 |
| | | CO3 | 0 | | MN Î | 0 | TDS | 356. |
| | | CL | 35. | | HG | 0 | KJEL | .20 |
| | | CR | 0 | | MD | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | 0 |
| | | COND | 530. | | NO3 | 1.20 | PH | 8.00 |
| | | | | | | - | | |

| | | | | | - | | | | |
|------|----------|-----------|---------------|---|----------|-------|---|-------------|---------------|
| CASE | MD-DA-YR | | | | | | | | |
| 31 | 05/06/87 | ALK | 102 | | CH | | | 004 | 17 |
| 31 | 03/00/07 | AL | 182. | | CU Ch | 0 | | P04 | .13 |
| | | HL NH3 | 0 | | F | 0 | | K | 6.45 |
| | | | 0 | | | .89 | | RESD | -0.421 |
| | | AS | .08 | | ALFA | 0 | | SE | 0 |
| | | BA | | | BETA | 0 | • | \$102 | 29.91 |
| | | 8E | 0 | | OH | 0 | | AG | 0 |
| | | HCD3 | 222. | | FE | 0 | | SAR | 1.359 |
| | | 8 | .14 | | P8 | 0 | | NA | 44.56 |
| | | CD | . 0 | | FI | .051 | | S04 | 72. |
| | | CA | 72. | | MG | 5.70 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | 108 | 35 5 . |
| | | CL | 32.60 | | HG | 0 | | KJEL | 0 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | 00 | 0 | | MI | 0 | | · ZN | 0 |
| | | COND | 550. | | NO3 | 1.01 | | PH | 7.80 |
| | | | | | | | | | |
| 32 | 08/19/87 | ALK | 183. | | CU | 0 | | P04 | .09 |
| | | AL | 0 | | CH | 0 | | K | 5.32 |
| | | NH3 | .06 | • | F | 1.01 | | RESD | .003 |
| | | AS | .003 | | ALFA | 0 | | SE | 0 |
| | | 8A | .06 | | BETA | 0 | | \$102 | 32.75 |
| | | BE | 0 | | OH | . 0 | | AG | 0 |
| | | HCO3 | 2 2 3. | | FE | .03 | | - SAR | 1.545 |
| | | В | .08 | | PB | 0 ~. | | NA | 48 |
| | | CD | 0 | | LI | .05 | • | S 04 | 65. |
| | | CA | 48.01 | | MG | 15.29 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | | TDS | 331. |
| | | CL | 33.20 | | HG | 0 | | KJEL | .15 |
| | | - CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | | COND | 550. | | NO3 | 1.37 | | PH | 7.40 |
| | | | | | | - | | | |
| 33 | 11/13/87 | ALK | 248. | | CU | Ò | | P04 | .69 |
| | | AL | 0 | | CH | 0 | | K | 8.66 |
| | | NH3 | .09 | | F | .71 | | RESD | -1.605 |
| | • | AS | .012 | | ALFA | 0 | | SE | 0 |
| | | BA | .10 | | BETA | 7. | | SI02 | 38.47 |
| | | 8 E | 0 | | OH | 0 | | AG | 0 |
| | | HCO3 | 303. | | FE | 0 | | SAR | 1.504 |
| | | В | .13 | | PB | 0 | | NA | 62.70 |
| | | CD | 0 | | LI | .06 | | SD4 | 155. |
| | | CA | 88.36 | | MG | 26.32 | | SURF | 0 |
| | | C03 | 0 | | HH · | 0 | | TDS | 540. |
| | | CL | 43.50 | | HG | 0 | | KJEL | .12 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZH | 0 |
| | | COND | 828. | | N03 | 1.25 | | PH | 7.60 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------------|-------|------|-------|-------|--------|
| 34 | 03/16/88 | ALK | 182. | CU | 0 | · P04 | .14 |
| | | AL | 0 | CN | 0 | K. | 5.94 |
| | | NH3 | .08 | F | 1.06 | RESD | -1.381 |
| | | AS | .005 | ALFA | 0 . | SE | 0 |
| | | BA | . 06 | BETA | 8. | \$102 | 35.24 |
| | | 8 E | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 222. | FE | .12 | SAR | 1.331 |
| | | В | .11 | PB | 0 | NA | 48.50 |
| | • | CD | 0 | LI | .06 | S04 | 120. |
| | | CA | 72.80 | MG | 16.89 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TD\$ | 420. |
| | | CL | 36.30 | HG | 0 | KJEL | .10 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | • | COND | 630. | H03 | 1.19 | PH | 7.60 |
| | | | | | | | |
| 35 | 06/07/88 | ALK | 170. | CU | 0 | P04 | .10 |
| | | AL | 0 | CN | 0 · | K | 5.88 |
| | | NH3 | 0 | F | . 94 | RESD | .477 |
| | | AS | . 005 | ALFA | Ō | SE | 0 |
| | | BA | .07 | BETA | 4. | \$102 | 36.29 |
| | | BE | 0 | OH | . 0 | - AG | 0 |
| | | HCO3 | 207. | FE | Q: | SAR | 1.221 |
| | | 8 | .11 | PB | 0 % | NA NA | 39.05 |
| | | CD | 0 | LI | .05 | S04 | 66. |
| | | CA | 77.60 | MG | 0 , | SURF | 0 |
| | | C03 | 0 | MH | Ŏ | TDS | 345. |
| | | CL | 35.40 | He | ŏ . | KJEL | 0 |
| | | CR | 0 | MO | Ŏ | VA | .02 |
| | | CO | ŏ | NI | ŏ | ZN: | 0 |
| | | COND | 530. | H03 | 3.20 | PH | 7.80 |
| | | | | | | • | |
| 36 | 10/07/88 | ALK | 180. | CU | 0 | P04 | .09 |
| | | AL | 0 | CN | 0 | K | 6.05 |
| | | NH3 | 0 | F | .88 | RESD | -0.777 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 0 | \$102 | 33.43 |
| | | BE | .002 | , OH | 0 | AG | 0 |
| | | HCO3 | 220. | FE | 0 | SAR | 1.122 |
| | | 8 | .10 | PB | 0 | NA | 38.18 |
| | | CD | 0 | LI | .06 | \$04 | 64. |
| | | CA | 77.60 | MG | 6.24 | SURF | Ó |
| | | CO3 | 0 | MN | 0 | TDS | 348. |
| | | CL | 40. | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 550. | NO3 | .99 | PH | 8.10 |

| CASE | MO-DA-YR | | | • | | | | |
|------|----------|-------|-------|------|-------|---|-------|--------|
| 37 | 03/23/89 | ALK | 180. | CU | ´ 0 | | P04 | .19 |
| | , . | AL | 0 | CN | 0 | | K | 6.31 |
| | | NH3 | .09 | F | 1.03 | | RESD | -0.776 |
| | | AS | 0 | ALFA | 0 | | SE | 0 |
| | | BA | .07 | BETA | 0 | | \$102 | 34.73 |
| | | BE | 0 | OH | 0 | | AG | 0 |
| | | HCO3 | 220. | FE | 0 | | SAR | 1.143 |
| | | В | .10 | PB | 0 | | NA | 68.93 |
| | | CD | 0 | LI | .06 | | S04 | 67. |
| | | CA | 73.60 | MG | 8.64 | | SURF | 0 |
| | | C03 | . 0 | nn · | 0 | | TDS | 388. |
| | | CL | 41. | HG | 0 | | KJEL | 1.10 |
| | | CR | 0 | HO | 0 | | VA | 0 |
| | | CO | 0 | NI | 0 | | ZN | 0 |
| | · | COND | 600. | ND3 | 1.20 | | PH | 7.45 |
| 38 | 05/15/89 | ALK | 188. | CU | 0 | | P04 | .12 |
| 40 | 03/13/07 | AL | 0 | CN | 0 | | K | 6.79 |
| | | NH3 | .04 | F. | 1.08 | | RESD | -0.463 |
| | | AS | 0 | ALFA | 0 | | SE | 0 |
| | | BA | .08 | BETA | 0 | | 5102 | 33.94 |
| | | BE | 0 | OH | . 0 | | AG | 0 |
| | | HCO3 | 229. | FE | 0. | | SAR | 1.314 |
| | | В | .10 | PB | 0 - | | NA | 43.89 |
| | | CD | 0 | LI | .06 | | S04 | 71. |
| | | CA | 55.63 | MG | 17.55 | | SURF | . 0 |
| | | C03 | 0. | MN | 0 | | TDS | 355. |
| | | CL | 35. | HG | 0 | | KJEL | .06 |
| | | CR | 0 . | MO | 0 | | VA | .02 |
| | | CO | 0 | NI | 0 | | ZN | 0 |
| , | | COND | 560. | H03 | 1.29 | | PH | 7.80 |
| 39 | 09/11/89 | ALK | | CU | 0 | | PD4 | .44 |
| 37 | 07/11/07 | AL . | 0 | CN | 0 | | K | 5.98 |
| | | NH3 | .09 | F | .95 | | RESD | -7.060 |
| | | AS | 0 | ALFA | 0 | • | SE | 0 |
| | | BA | .06 | BETA | 5. | | \$102 | 34.50 |
| • | | 38 | 0 | OH | | | AG | 0 |
| | | HCO3 | 220. | FE | - 0 | | SAR | .72 |
| | | В | .12 | PB | 0 | | NA | 40.86 |
| | | CD . | 0 | tI | .06 | | S04 | |
| | | CA | 51.28 | MG | 16.48 | | SURF | 0 |
| | | CO3 - | | MM | 0 | | TDS | 340. |
| | | CL | 34.10 | He | 0 | | KJEL | |
| | | CR | 0 | MO | 0 | | VA | 0 |
| | | CO | 0 | NI | 0 | | . ZN | 0 |
| | | COND | | NO3 | 1.20 | | PH | |

| CASE | MO-DA-YR | | | | • | | | | |
|------|-----------|------|--------------|---|-----------|-------|---|-------------|--------|
| 40 | 10/11/89 | ALK | 176. | • | CU | 0 | | P04 | .11 |
| | | AL | 0 | | CN | 0 | | K | 6.20 |
| | | NH3 | 0 . | | F | 1.03 | | RESD | -0.490 |
| | | AS | .004 | | ALFA | 0 | | SE | 0 |
| | | BA | .07 | | BETA | 3. | | SI02 | 36.17 |
| | | 8E | 0 | • | OH | 0 | | AG | 0 |
| | | HCO3 | 215. | | FE | 0 | | SAR | 1.23 |
| - | | В | .09 | | PB | 0 | | NA | 40.09 |
| | | CD | 0 | | LI | .061 | | S04 | 63. |
| | | CA | 52.81 | | MG | 16.82 | | SURF | 0 |
| | | C03 | 0 | | MH | 0 | | TDS | 321. |
| | | CL | 33.50 | | HG | 0 | | KJEL | 0 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | | COND | 495. | | NO3 | 1.16 | | PH | 7.30 |
| | 27/07/202 | A. U | 104 | | Au1 | ٨ | | 004 | 11 |
| 41 | 03/26/90 | ALK | 184. | | CU | 0 | | P04 | .11 |
| | | AL | 0 | | CN | 0 | | K | 6.07 |
| | | NH3 | .09 | | F | .81 | | RESD | -0.393 |
| | | AS | .005 | | ALFA | 0 | | SE | 0 |
| | | BA | .07 | | BETA . | 6. | | SIO2 | 31.74 |
| | | 8E | 0 | | OH | . 0 | | AG | 0 |
| | | HCO3 | 224. | | FE | Q. | | SAR | 1.265 |
| | | В | .07 | | PB | 0 | | NA CO4 | 41.47 |
| | | CD | 0 | | LI | .06 | | \$04 | 57. |
| | | CA | 54.60 | | MS | 16.32 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 . | , | TDS | 330. |
| | | CL | 35.80 | | H6 | 0 | | KJEL | .10 |
| | • | CR | 0 | | MO | 0 . | | VA | . 0 |
| | | CO | 0 | | NI NO7 | 0 | | ZN | ` 0 |
| | | COND | 475 . | • | NO3 | 1.10 | | PH | 7.80 |
| 42 | 07/05/90 | ALK | 187. | | CU | 0 | | P04 | .24 |
| | | AL | 0 | | CN | 0 | | K | 5.67 |
| | | NH3 | .13 | | F | .95 | | RESD | -0.418 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .07 | | BETA | 6. | | S102 | 33.73 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 228. | | FE | 0 | | SAR | 1.276 |
| | | В | .09 | | PB | 0 | | NA | 42.29 |
| | | CD | 0 | | LI | .05 | | S 04 | 80. |
| | | CA | 54.62 | • | MG | 17.40 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | TDS | 440. |
| | • | CL | 37.70 | | HG | 0 | | KJEL | 1.14 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | | COND | 446. | | NO3 | 1.18 | , | PH | 7.50 |
| | | | | | | | | | |

| CASE | MO-DA-YR | | | | | | |
|------|----------|------|-------|------|-------|-------|--------|
| 43 | 10/18/90 | ALK | 180. | CU | .03 | 904 | .20 |
| | | AL | .11 | CN | . 0 | K | 6.42 |
| | | NH3 | .04 | F | 1.04 | RESD | -0.167 |
| | | AS | .009 | ALFA | 0 | SE | 0 |
| | | BA | .071 | BETA | 0 | \$102 | 41.40 |
| | | BE | 0 | GH | 0 | AG | 0 |
| | | HCO3 | 220. | FE | .07 | SAR | 2.25 |
| | | 8 | .04 | PB | .003 | NA | 53.11 |
| | | CD | 0 | LI | .07 | 504 | 66. |
| | | CA | 50.20 | HG | 15.44 | SURF | 0 |
| | • | C03 | 0 | MN | 0 | TDS | 394. |
| | | CL | 33.40 | HG | 0 | KJEL | .21 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | . 04 |
| | | COND | 432. | NO3 | 1 19 | PH | 7.70 |

WELL #5 - CHEMICAL ANALYSES

| AVERAGES | 02/23/ | 78 TO 01/09/91 | | | | |
|----------|--------|----------------|------|--------|------|---------|
| | ALK | 186.5 | CU | .003 | P04 | .176 |
| | AL | .03 | CN | .001 | K | 6.069 |
| | NH3 | .124 | F | . 937 | RESD | -22.132 |
| | AS | .003 | ALFA | 1.2 | SE | .00 |
| | BA | .08 | BETA | 4.2 | SI02 | 33.761 |
| | 8E | .00 | OH | 0 | AG | 0 |
| | HCO3 | 226.6 | . FE | .019 | SAR | 1.294 |
| | В | .117 | PB | .007 | NA | 44.31 |
| | CD | .00 | LI | .051 | S04 | 78. |
| | CA | 61.198 | MG | 16.764 | SURF | 0 |
| | C03 | 0 | ĦN | .003 | TDS | 372. |
| | CL | 36.05 | HG | 0.00 | KJEL | .249 |
| | CR | .001 | MO | .003 | VA | .006 |
| | CO | .002 | NI | .002 | ZN | .007 |
| • | COND | 557. | NO3 | 1.049 | PH | 7.70 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

WELL #6 - CHEMICAL ANALYSES

| 0405 | NO DA VO | | | • | | | |
|------|-----------|------|-----------------|------|-------|-------------|--------|
| CASE | MO-DA-YR | | | | | • | |
| 3 | 05/03/78 | ALK | 420. | CU | .005 | P04 | .04 |
| | , , , , , | AL | .05 | CN | 0 | K | 17.09 |
| | | NH3 | . 15 | F | .66 | RESD | 2 |
| | | AS | 0 | ALFA | 5. | SE | .003 |
| | | BA | . 10 | BETA | 18. | \$102 | 45. |
| | | BE | | OH | | AG | .002 |
| | | HC03 | | FE | .038 | SAR | 1.817 |
| | | 8 | . 30 | PB | .006 | NA | 110 |
| | | CD | 0 | iI | .01 | 504 | 400. |
| | | CA | 188. | MG | 54.72 | SURF | 0 |
| | | C03 | 100. | MH | .011 | TDS | 1169. |
| | | CL | 84. | HG | 0 | KJEL | 2. |
| | | CR | 0 | MO | • | VA | 0 |
| | | CO | .003 | IN | 0 | ZN | .03 |
| | | COND | 1790. | NO3 | 1.82 | PH | 7.11 |
| | | COND | 1770. | NOS | 1.02 | rn | 7.11 |
| 4 | 10/13/78 | ALK | 406 | CU | .008 | P04 | .05 |
| | | AL | .05 | CN | 0 | K | 12.16 |
| | | NH3 | 0 | F | .76 | RESD | |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .09 | BETA | 10. | \$102 | 37.75 |
| | | BE | | OH · | | AG | 0 |
| | | HCO3 | | FE | .044 | SAR | 2.501 |
| | | В | . 25 | PB | 0 ~ | NA | 120.70 |
| | | CD | 0 | LI | .013 | 304 | 270. |
| | | CA | 168. | MG | 5.30 | SURF | 0 |
| | | CO3 | | MN | .012 | TDS | 890. |
| | | CL | 64. | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | • | VA | .09 |
| | | CO | . 005 | NI | .021 | ZN | .013 |
| | | COND | 1365. | NO3 | 1.54 | PH | 7.11 |
| 5 | 06/01/79 | ALK | 260. | CU | .002 | PO 4 | 0 |
| • | 00/01/77 | AL | 0 | CN | 0 | . K | 7.78 |
| | | NH3 | 0 | F | .87 | RESD | 7.70 |
| | | AS | .003 | ALFA | 2.5 | SE | .002 |
| | | BA | .09 | BETA | 10. | 5102 | 40. |
| | | BE | 0 | OH | | AG | 0 |
| | | HC03 | • | FE | 0 | SAR | 1.286 |
| | | 8 | .16 | PB | 0 | NA NA | 53.20 |
| | | CD | 0 | LI | .068 | S 04 | 130. |
| | | CA | 90.40 | MG | 24. | SURF | 0 |
| | | C03 | 7 V. 4 V | WM . | .003 | TDS | 500. |
| | | CL | 38. | HG | 0 | KJEL | .15 |
| | | CR | .002 | MO | 0 | VA | 0 |
| | | CO | .002 | NI . | 0 | ZN | .003 |
| | | COND | .004 770. | NO3 | .02 | PH PH | 7.75 |
| | | עאטט | //V. | nuo | .02 | rn | 1.15 |

| CASE | MO-DA-YR | | | | • | | | |
|------|----------|------|--------|---|-------|-------|-----------|--------------|
| 6 | 09/10/79 | ALK | 412. | | cu | .01 | P04 | .08 |
| | | AL | .06 | | CN | 0 | K | 11.90 |
| | | NH3 | 0 | | F | .67 | RESD | |
| | | AS | 0 · | | ALFA | 3. | SE | .003 |
| | | BA | .06 | | BETA | 13. | \$102 | 41. |
| | | BE | | | OH | • | n AG | 0 |
| | | HCO3 | 502.6 | | FE | .04 | SAR | 1.951 |
| | | В | . 23 | | PB | 0 | · NA | 108 |
| | | CD | 0 | | LI | .096 | \$04 | 320 . |
| | | CA | 214.40 | • | MG | 11.04 | SURF | 0 |
| | | C03 | | • | MM | .006 | TDS | 985. |
| | | CL | 64. | | HG | 0 | KJEL | .10 |
| | | CR | .002 | | MO | V | VA | 0 |
| | | CO | .038 | | NI | 0 | ZN | .019 |
| | | COND | 1500. | | NO3 | 1.36 | PH | 7.90 |
| | | COND | 1500. | | , nus | 1.36 | rn | 7.70 |
| 7 | 04/28/80 | ALK | 532. | | CU. | .01 | PO4 | .10 |
| | | AL | .14 | | CN | .003 | K | 15.50 |
| | | NH3 | 0 | | F | .63 | RESD | |
| | | AS | 0 | | ALFA | 2.6 | \$E | 0 |
| | | BA | .21 | | BETA | 10.6 | \$102 | 44.50 |
| | | BE | 0 | | OH | | AG | 0 |
| | | HC03 | 649. | | . FE | .02 | SAR | 1.885 |
| | | В | .29 | | PB | 0 5. | NA | 120 |
| | | CD | 0 | | LI | .114 | \$04 | 380. |
| | | CA | 188.80 | | MG | 72. | SURF | 0 |
| | | CO3 | 100.00 | | MN | .01 | TDS | 1180. |
| | | CL | 82. | | H6 | 0 | KJĒL | 0 |
| | | CR | 0 | | MO | .002 | YA | .005 |
| | | CO | .008 | | NI | .039 | ZN | 0 |
| | | COND | 1800. | | NO3 | 0 | PH | 7.20 |
| 8 | 07/23/80 | ALK | 302. | | CU | .01 | P04 | .52 |
| U | 07/23/00 | AL | 0 | | CN | 0 | K | 7.70 |
| | | NH3 | 0 | | F | .39 | RESD | 7.70 |
| | | AS | .002 | | | | SE | 0 |
| | • | | .002 | | ALFA | 0 | | 36.10 |
| | | BA | 0 | | BETA | 0 | \$102 | 0 |
| | | BE | | | 0H | 10 | , AG | |
| | | HCO3 | 368.4 | | FE | .12 | SAR | 1.624 |
| | | B | .13 | | P8 | 0 | NA SOA | 75 204 |
| | | CD | .005 | | LI | . 076 | 504 | 204. |
| | | CA | 111.20 | | MG | 30.72 | SURF | 0 |
| | | C03 | | | MN | .01 | TDS | 660. |
| | | CL | 46. | | HG | 0 | KJEL | 0 |
| | | CR | .007 | | MO | 0 | VA | Ó |
| | | CO . | 0 | | NI | 0 | ZN | .02 |
| | | COND | 1000. | | NO3 | .88 | PH | 7.70 |

| CASE | MO-DA-YR | | | | - | | | | |
|------|----------|------|-------|---|------|-------|---|-------|--------|
| 9 | 12/10/80 | ALK | 314. | | CU | .01 | | P04 | .05 |
| | | AL | 0 | | CN · | 0 | | K . | 18.50 |
| | | NH3 | 0 | | F | .47 | | RESD | |
| | | AS | .003 | | ALFA | 1.3 | | SE | 0 |
| | | BA | .075 | | 8ETA | 9.6 | | \$102 | 34.50 |
| | | 38 | 0 | | OH | | | AG. | 0 |
| | | HCO3 | 383. | • | FE | .02 | | SAR | 1.558 |
| | | В | .205 | | PB | 0 | | NA | 70 |
| | | CD | 0 | | LI | .072 | | S04 | 165. |
| | | CA | 112. | | MG | 24.96 | | SURF | . 0 |
| | | CO3 | | | MN | 0 | | TDS | 610. |
| | | CL | 41.60 | | HG | 0 | | KJEL | . 20 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | .01 | | NI | 0. | | ZN | .005 |
| | | COND | 930. | | NO3 | 1.24 | | PH | 7.10 |
| | | | | | | | | | |
| 10 | 03/23/81 | ALK | 296. | | CU | 0 | | P04 | . 33 |
| | | AL | .11 | | CN | 0 | | K | 8.30 |
| | | NH3 | .10 | | F | .89 | | RESD | |
| | | AS | .002 | | ALFA | 1.1 | | SE | .002 |
| | | BA | .08 | | BETA | 0 | | \$102 | 36. |
| | • | BE | 0 | | OH | | | AG | 0 |
| | | HCO3 | 361.1 | | FE | .10 | | SAR | 1.501 |
| | | 8 | .15 | • | PB | .002 | | NA | 69.50 |
| | | CD | 0 | | LI | .075 | | S04 | 185. |
| | • | CA | 116. | | MG | 28.32 | | SURF | 0 |
| | | C03 | | | MN | | | TDS | 635. |
| | | CL | 52.40 | | HE | .0003 | | KJEL | .18 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | Ö | | NI | . 0 | | ZN | .01 |
| | | COND | 970. | | NO3 | 1.28 | | PH | 7.70 |
| | | | | | | | | | |
| 11 | 10/20/81 | ALK | 320. | | CU | 0 | | P04 | . 20 |
| | | AL | . 065 | | CN | .008 | | K | 8.50 |
| | | NH3 | .06 | | F | .73 | | RESD | -1.348 |
| | | AS | .003 | | ALFA | 1.3 | | SE | 0 |
| | | BA | .089 | | BETA | 0. | | \$102 | 43.10 |
| | | BE | . 0 | | OH | 0 | ~ | AG | 0 |
| | | HCO3 | 390.1 | | FE | 11 | | SAR | 1.767 |
| | | 8 | .16 | | P8 | .003 | | NA | 80 |
| | | CD | 0 | | LI | .085 | | S04 | 204. |
| | | CA | 96. | | MG | 36. | | SURF | 0 |
| | | C03 | 0 | | MN | .009 | | TDS | 665. |
| | | CL | 30.40 | | HG | 0 | | KJEL | .30 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | .011 |
| | | COND | 720. | | NO3 | .47 | | PH | 7.60 |
| | | | | | | | | | |

| | | | | | - | • | | |
|------|----------|------|--------|---|------|-------|-------|--------|
| CASE | MO-DA-YR | | • | | | | | |
| 12 | 03/10/82 | ALK | 524. | | CU | .01 | PO4 | .09 |
| | 00/10/01 | AL | 0 | | CN | .02 | X | 5.40 |
| | | NH3 | .13 | - | F | .71 | RESD | -9.330 |
| | | AS | .004 | | ALFA | 0 | SE | .003 |
| | | BA | .07 | | BETA | 0 | \$102 | 28.50 |
| | | BE | 0 | | OH | Ŏ | , AG | 0 |
| | | HCO3 | 639.3 | • | FE | .03 | SAR | 2.418 |
| | | В | .20 | | PB | 0 | NA | 175 |
| | | CD | 0 | | LI | .016 | 504 | 680. |
| | | CA · | 290 | | MG | 65. | SURF | .12 |
| | | C03 | 0 | • | MN | 0 | TDS | 1650. |
| | | CL | 97.10 | | HG | 0 | KJEL | .15 |
| | • | CR | .003 | | MO | .005 | VA | .02 |
| | | CO | .005 | | NI | | | • |
| | • | | | | | 0 | ZN | .006 |
| | | COND | 2500. | | N03 | 2.59 | PH · | 7.00 |
| | N. | | | | | | | |
| 13 | 05/13/82 | ALK | 541.2 | • | CU | .01 | P04 | .17 |
| - | , , | AL | 0 | | CN | .012 | K | 6.10 |
| | | NH3 | .61 | | F | .74 | RESD | -3.576 |
| | | AS | .004 | | ALFA | 1.5 | SE | .005 |
| | | BA | .07 | | BETA | 1.8 | \$102 | 58.20 |
| | | 8E | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 660.3 | | FE | .051 | SAR | 2.674 |
| | | В | .225 | | PB | 0 21 | NA | 165 |
| | | CD | 0 | | LI | .03 | S04 | 390. |
| | | CA | 184. | | MG | 63.50 | \$URF | 0 |
| | | CO3 | 0 | | MN | ,005 | TDS | 1250. |
| | | CL | 92.70 | | HG | 0 | KJEL | .70 |
| | | CR | .005 | | MO | 0 | VA | 0 |
| | | CO | 0 . | | NI | 0 | | |
| | | | | | | | ZN | .02 |
| | | COND | 1890. | | NO3 | 2.82 | PH | 7.30 |
| | | | | • | | | | |
| 14 | 08/26/82 | ALK | 278. | | CU | .01 | P04 | .17 |
| | | AL | 0 | | CN | .005 | K | 8.40 |
| | | NH3 | 1.41 | | F | .83 | RESD | -2.673 |
| | | AS | .002 | | ALFA | 1.6 | SE | .002 |
| | | BA | .085 | | BETA | . 1.9 | \$102 | 40.76 |
| | • | BE | 0 | | OH | 0 | AG | 0 |
| | | HC03 | 339. | | FE | . 02 | SAR | 4.052 |
| | | В | .15 | | PB | 0 | NA | 189 |
| | • | CD | 0 | | LI | .077 | S04 | 480. |
| | | CA | 110.40 | | ĦG | 33.12 | SURF | 0 |
| | | C03 | 0 | | MN | .003 | TDS | 1025. |
| | | CL | 43.50 | | Ke | 0.00 | KJEL | 1.65 |
| | | CR | . 0 | | MO | 0 . | , VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .003 |
| | | COND | 1570. | | NO3 | .80 | PH | 7.50 |
| | | | | | | | | |

WELL #6 - CHEMICAL ANALYSES

| CASE | MO-DA-YR | | • | • | | | |
|------|----------|------|--------|------|---------------|------------|--------|
| 15 | 12/08/82 | ALK | 269.6 | cu | .01 | · P04 | .16 |
| | | AL | 0 | CN | .008 | K | 8.20 |
| | | NH3 | .03 | F | .80 | RESD | 2.519 |
| | | AS | .003 | ALFA | | SE | 0 |
| | | BA | .075 | BETA | | \$102 | 35. |
| | | BE | 0 - | OH | 0 | AG | 0 |
| | | HCO3 | 328.9 | FE | .03 | SAR | 1.563 |
| | | В | .15 | PB | 0 | NA | 71.50 |
| | | CD | 0 | LI | .073 | S04 | 228. |
| | | CA | 101.60 | MG | 34.56 | SURF | 0 |
| - | | C03 | 0 | MN | .002 | TD3 | 651. |
| | | CL | 44. | HG | 0 | KJEL | .20 |
| | | CR | .002 | HO | 0 | VA | 0 |
| | | 60 | 0 | NI | 0. | ZN | .007 |
| | | COND | 990. | NO3 | 1.45 | PH | 7.40 |
| | | | | | | | |
| 16 | 02/22/83 | ALK | 289.4 | CU | 0 | P04 | .28 |
| • | | AL | 0 | CN | 0 | . K | 8.10 |
| | | NH3 | .08 | F | . 85 | RESD | -1.407 |
| | | AS | .003 | ALFA | 1.8 | SE | .0 |
| | | 8A | .10 | BETA | 1.3 | \$102 | 34.50 |
| | • | BE | 0 , | OH | . 0 | AG | 0 |
| | | HCO3 | 353.1 | · FE | .06 | SAR | 1.582 |
| | | 8 | .14 | PB | 0 % | . NA | 69 |
| | | CD | 0 | LI | .07 | S04 | 174. |
| | | CA | 96. | MG | 29 .28 | SURF | 0 |
| | | C03 | 1. | MH | .005 | TDS | 594. |
| | | CL | 39.50 | HG | 0 | KJEL | .18 |
| | | CR | .001 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .004 |
| | | COND | 900. | ND3 | 1.20 | PH | 7.50 |
| | 25/22/25 | | | ٠. | | | |
| 17 | 05/27/83 | ALK | 276. | CU | 0 | P04 | .12 |
| | | AL | .75 | CN | .008 | K | 8.50 |
| | | NH3 | . 50 | F | .82 | RESD | -1.718 |
| | | AS | .004 | ALFA | 0 | SE | 0 |
| | | BA | . 07 | BETA | 1,1 | \$102 | 34.90 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 336.7 | FE | .04 | SAR | 1.646 |
| | | 8 | .14 | PB | 0 | NA | 72 |
| | | CD | 0 | LI | .072 | \$04 | 180. |
| | | CA | 100. | MG | 27.36 | SURF | 0 |
| | | C03 | 0 | MN | .003 | TDS | 618. |
| | | CL | 52. | HG | 0 | KJEL | .22 |
| | | CR | . 002 | MO | .01 | . VA | . 0 |
| | | CO | 0 | NI | 0 | ZH | .002 |
| | | COND | 920. | NO3 | .16 | PH | 7.40 |

| | | | | • . | | | |
|------|----------|--------------|-----------|------|------------|-------|--------|
| CASE | MO-DA-YR | | | | | | |
| 18 | 08/17/83 | ALK | 294. | CU | .01 | P04 | .13 |
| | , , | AL | 0 | CN | .012 | K | 8.20 |
| | | NH3 | .60 | F | .81 | RESD | 1.675 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | • | BA | .069 | BETA | 1.1 | \$102 | 33.80 |
| | | BE | . 0 | НО | 0 | AG | 0 |
| | | HC03 | 358.6 | FE | .036 | SAR | 1.678 |
| | | В | .15 | PB | .002 | NA | 75 |
| | | CD | 0 | LI | .06 | S04 | 182. |
| | | CA | 100. | MG | 31.20 | SURF | 0 |
| | | C03 | 0 | MN | .018 | TOS | 636. |
| | | CL | 50. | HG | .0002 | KJEL | 1.10 |
| | | CR | .002 | MO | 0 | VA | 0 |
| | | CO | | NI | 0 | | .005 |
| | | COND | 0 970. | | | ZN | |
| | , | CUND | 7/0. | NO3 | .15 | PH | 7.80 |
| 19 | 11/08/83 | A1 V | 0/0 | All | A 1 | 004 | 10 |
| 19 | 11/00/03 | ALK | 268. | CU | .01 | P04 | .12 |
| | • | AL | .005 | CN - | .015 | K | 7.20 |
| | | NH3 | .30 | F | .81 | RESD | -2.193 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | 8A | .07 | BETA | 1.9 | \$102 | 33.10 |
| | | BE | 0 | OH | . 0 | A6 | 0 |
| | • | HC03 | 326.9 | FE | .044 | SAR | 1.43 |
| | | В | . 16 | PB | 0 | NA | 63.90 |
| | | CD | 0 | LI | .07 | S04 | 172. |
| | | CA | 98. | MG | 32.40 | SURF | |
| | | C03 | 0 | MN | .02 | TDS | 680. |
| | | CL | 44. | H6 | 0 | KJEL | .50 |
| | | CR | .002 | MO | 0 . | VA | 0 |
| | | CO . | 0 | NI | 0 | ZN | .004 |
| | | COND | 900. | NO3 | . 16 | PH | 7.80 |
| 22 | 07/00/04 | A1 I/ | 400 | | | ••• | |
| 20 | 03/22/84 | ALK | 422. | CU | 0 | P04 | .12 |
| | | AL | 0 | CN | 0 | K | 18.30 |
| | | NH3 | 0 | F | .85 | RESD | .76 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | • | BA | .05 | BETA | 0 | \$102 | 33.50 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 514.8 | FE | 0 | SAR | 3.60 |
| | | . B | .20 | PB | 0 | NA | 178 |
| | | CD | 0 | LĪ | .12 | 304 | 334. |
| | | CA | 166.80 | MG | 10.80 | SURF | 0 |
| | | C03 | 0 | MN | .01 | TDS | 1065. |
| | | CL | 79. | HG | 0 | KJEL | .25 |
| | | CR | 0 | MO | 0 | VA. | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 1600. | NO3 | 1.84 | PH | 7.30 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|--------|------|-------|-------|--------|
| 21 | 08/15/84 | ALK | 288. | CU | .007 | P04 | .43 |
| | | AL | 0 | CN | 0 | K | 8.10 |
| | | NH3 | .22 | F | .83 | RESD | -1.700 |
| | | AS | .006 | ALFA | 0 | SE | 0 |
| | | BA | .08 | 8ETA | 4. | \$102 | 21.70 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 351.4 | FE | .03 | SAR | 1.779 |
| | | В | .191 | PB | .07 | NA | 79 |
| | | CD | 0 | LI | .07 | 504 | 168. |
| | | CA | 100. | MG | 30. | SURF | 0 |
| | | C03 | 0 | . MN | 0 | TDS | 635. |
| | | CL | 70. | HG | 0 | KJEL | .35 |
| | | CR | 0 | MO | 0 | YA | 0 |
| | | CO | 0 | NI | 0 | ZN | .007 |
| | | COND | 980. | NO3 | 1.30 | PH | 7.85 |
| | | | | | | | |
| 22 | 11/12/84 | ALK | 284. | CU | .005 | P04 | .64 |
| | | AL | 0 | CN | 0 | K | 8.40 |
| | | HH3 | 0 | F | .69 | RESD | -1.731 |
| | | AS | . 006 | ALFA | 0 | \$E | 0 |
| | | BA | .08 | BETA | 10. | \$102 | 21. |
| | | BE . | 0 | . OH | . 0 | AG | 0 |
| | | HCO3 | 346.5 | FE | .02 | SAR | 2.952 |
| | | 8 | . 165 | PB | .01 | NA | 67 |
| | | CO | 0 | LI | .077 | \$04 | 162. |
| | | CA | 124. | MG | 14.90 | SURF | 0 |
| | | C03 | 0 | MH | 0 | TDS | 595. |
| | | CL | 46. | HG | 0 | KJEL | .10 |
| | | CR | 0 | HO | .01 | VA | .015 |
| | | CO | 0 | NI | 0 | ZN | .002 |
| | | COND | 900. | NO3 | 1.23 | PH | 7.82 |
| 23 | 02/25/85 | ALK | 286. | CU | 0 | PO4 | .10 |
| | 7 | AL | .002 | CN | 0 . | K | 8.30 |
| | | NH3 | 0 | F | .83 | RESD | -2.886 |
| | | AS | .008 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 8. | \$102 | 41.51 |
| | | 88 | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 349. | FE | .02 | SAR | 1.419 |
| | | В | .17 | PB | 0 | NA | 67.70 |
| | | CD | 0 | LI | .074 | S04 | 220. |
| | | CA | 122.10 | MG | 30.60 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 660. |
| | | CL | 45. | HG | 0 | KJEL | 3.15 |
| | | CR | .037 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | Ō | ZN | .005 |
| | · | COND | 1010. | NO3 | 1.18 | PH | 7.00 |
| | | Jung | 4444 | 100 | 1.10 | • • • | |

| CASE | MO-DA-YR | | | • | | | |
|------|-------------|------------|--------|------|------------|--------------|--------|
| 24 | 06/17/85 | ALK | 271. | CU | 0 | P04 | .46 |
| | 00/ = 1/ 00 | AL | .11 | CN | 0 | K | 8.50 |
| | | NH3 | 0 | F | .75 | RESD | -1.664 |
| | | AS | .015 | ALFA | 0 | SE | 0 |
| | | BA | .08 | BETA | 8. | \$102 | 35.99 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | ē | HCO3 | 330.6 | FE | 0 | SAR | 1.571 |
| | | В | .24 | PB | .002 | NA · | 68 |
| | | CD | 0 | LÎ | .071 | S04 | 169. |
| | | CA | 106.40 | We | 21.60 | SURF | 0 |
| | | CO3 | 0 | MN | . 0 | TDS | 642. |
| | | CL | 46.70 | HG | . 0 | KJEL | 0 |
| | | CR | 0 | MD | 0 | VA | .005 |
| | | | 0 | NI | 0 | ZN | .006 |
| | | CO Cond | 900. | NO3 | 1.79 | PH | 7.80 |
| | | COND | 700. | 100 | 1.// | rn | 7.00 |
| | | | | • | | | |
| 25 | 08/19/85 | ALK | 281. | CU | 0 | P04 | .46 |
| 23 | 06/17/63 | AL | .02 | CN | Ŏ | K | 4.80 |
| | | | .10 | F | .83 | RESD | -1.656 |
| | | NH3 | 0 | | | SE | 0 |
| | | AS | | ALFA | 6. | | 36.48 |
| | | BA | .10 | BETA | 7. | SI02 | |
| | | BE | 0 | 0H | . 0 | AG | 0 |
| | | HCO3 | 343. | FE | 0: • 5: | SAR | 1.801 |
| | | 8 | .20 | PB | 0 | NA | 79 |
| | | CD | .007 | LI | .061 | S04 | 190. |
| | | CA | 102.40 | MG | 26.40 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 640. |
| | | CL | 50.20 | HG | 0 | KJEL | .14 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .018 |
| | | COND | 970. | NO3 | 1.34 | PH | 7.85 |
| | | | | | | | |
| 26 | 11/19/85 | ALK | 289. | CU | .02 | P04 | .42 |
| | | AL | 0 | CN | 0 . | K | 7.85 |
| | | NH3 | .10 | F | .84 | RESD | -1.686 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 4. | \$102 | 34.94 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 352. | FE | . 02 | SAR | 1.645 |
| | | В | . 23 | P8 | 0 | NA | 73 |
| | | CD | 0 | LI | .07 | S 0 4 | 193. |
| | | CA | 104.80 | MG | 27.10 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 628. |
| | | ÇL | 44.90 | HG | 0 | KJEL | .15 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .005 |
| | | COND | 950. | NO3 | 1.54 | PH | 7.80 |

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|--------|---|------|-------|-------|------------------|
| 27 | 02/19/86 | ALK | 283. | | CU | ٨ | 004 | 50 |
| ٤, | V2/17/00 | AL | 200. | | EN | 0 | P04 | .50 |
| | | NH3 | .60 | | F | .81 | V K | 7.73 |
| | | AS | .014 | | ALFA | 0 | RESD | -1.751 |
| | | BA | 1 .07 | | BETA | | SE | 0 75 90 |
| | | BE | 0 | | | 7. | \$102 | 35.89 |
| | | HCO3 | | | HO | 0 | AG | 0 |
| | | | 345. | | FE | 0 | SAR | 1.54 |
| | | В | .17 | | PB | 0 | NA | 60 |
| | | CD | 0 | | LI | .067 | \$04 | 173. |
| | • | . CA | 113.20 | | MG | 21.40 | SURF | 0 |
| | | C03 | 0 | | MM | 0 | TDS | 632. |
| | | CL | 44.30 | | HG | 0 | KJEL | .80 |
| | | CR | 0 | | MO | 0 | VA | .004 |
| | | CO | 0 | | HI | 0 | ZN | .023 |
| • | | COND | 971. | | NO3 | 1.35 | PH | 8.04 |
| | | | | | | | | |
| 28 | 05/20/86 | ALK | 402. | | CU | 0 | P04 | .76 |
| | | AL | 0 | | CN | 0 | K | 12.37 |
| | | NH3 | .19 | | F | .68 | RESD | -3.660 |
| | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | .03 | • | BETA | 9. | \$102 | 42.04 |
| | | 8E | 0 | | OH | . 0 | AG | 0 |
| | • | HCO3 | 490. | | FE | Q. | SAR | 1.673 |
| | | В | .22 | | PB | 0 % | NA . | 93 |
| | | CD | 0 | | LI | .08 | \$04 | 327. |
| | | CA | 170. | | MG | 39.10 | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | TDS | 978. |
| | | CL | 56.70 | | HG | Ö | KJEL | .25 |
| | | CR | 0 | | MO | 0 . | VA | 0 |
| | | CO | Ö | | NI | Ŏ | ZN | . 0 |
| | | COND | 1503. | | NO3 | 1.80 | PH | 8.15 |
| | | | | | | | | |
| 29 | 11/06/86 | ALK | 410. | | cu | 0 | PD4 | .97 |
| | | AL | 0 | | CN | 0 | K | 15.07 |
| | | NH3 | .14 | | F | . 58 | RESD | -3.854 |
| | | AS | .004 | | ALFA | 0 | SE | 0 |
| | | BA | . 03 | | BETA | 10. | SI02 | 41.14 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HC03 | 500.2 | | FE | .04 | SAR | 1.865 |
| | | В | .22 | | PB | 0 | NA | 105.29 |
| | | CD | .002 | | LI | .08 | S04 | 300. |
| | | CA | 169.60 | • | MG | 43.70 | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | TDS | 9 88. |
| | | CL | 82. | | HG | 0 | KJEL | .18 |
| | | CR | .002 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | 0 |
| , | | COND | 1500. | • | NO3 | 1.70 | PH | 8.20 |

| CASE | MO-DA-YR | | | | | | |
|------|------------|------|---------------|------------|-------|------------|------------------|
| 30 | 03/03/87 | ALK | 412. | CU | 0 | P04 | .88 |
| | • | AL | 0 | CN | 0 | K | 14.94 |
| | | NH3 | .24 | F | .74 | RESD | -3,372 |
| | | AS | .01 | ALFA | 13. | SE | 0 |
| | | BA | .04 | BETA | 8. | \$102 | 43.66 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 502.6 | FE | 0 | SAR | 1.967 |
| | | В | . 24 | PB | 0 | NA | 108.96 |
| | | CD | 0 | LI | .08 | \$04 | 343. |
| | | CA | 168. | MG | 39.30 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 985. |
| | | ' CL | 52.20 | HG | 0 | KJEL | .29 |
| | | CR | . 0 | HO | .02 | VA | 0 |
| | | CO | . 0 | NI NI | 0 | ZH | Ŏ |
| | | COND | 1490. | NO3 | 1.67 | PH | 8.00 |
| | | CUND | 1470. | กบง | 1.07 | | 0.00 |
| 31 | 05/06/87 | ALK | 531. | cu | 0 | P04 | 1.15 |
| | 00, 00, 0. | AL | 0 | CN | 0 | K | 17.62 |
| | | NH3 | .18 | F | .54 | RESD | -6.792 |
| | | AS | .007 | ALFA | 15. | SE | 0 |
| | | BA | .06 | BETA | 8. | \$102 | 44.15 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 648. | FE | Q. | SAR | 2.206 |
| | | В | .29 | P8 | 0 ~ | NA | 149.67 |
| | | CD | 0 | l I | .103 | S04 | 536. |
| | | CA | 241.60 | We | 65.20 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 1430. |
| | | CL | 8 5.80 | HG | Ŏ | KJEL | .20 |
| - | | CR | 0 | MO | Ô | VA | 0 |
| | | CO | 0 | NI | Ŏ | ZN | Ŏ |
| | | COND | | NO3 | 2.30 | PH | 7.80 |
| | | CUND | 2190. | | 2.30 | | 7.00 |
| 32 | 08/19/87 | ALK | 417. | €U | 0 | PO4 | 1.32 |
| | | AL | 0 | CN | 0 | K | 11.70 |
| • | | NH3 | .12 | · F | .64 | RESD | -3.317 |
| | | AS | .022 | ALFA | . 0 | SE | 0 |
| | | 8A | .03 | BETA | 14. | SI02 | 44.15 |
| | | BE | . 0 | OH | 0 | AG | 0 |
| | | HCO3 | 509. | FE | 0 | SAR | 2.071 |
| | | 8 | .21 | PB | 0 | NA | 115 |
| | | CD | 0 | LI | .08 | S04 | 346. |
| | | CA | 163.30 | MG | 42.75 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 9 98. |
| | | CL | 62.40 | HG | . 0 | KJEL | .15 |
| | | CR | , 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | z n | 0 |
| | | COND | 1540. | NO3 | 1.77 | PH | 7.00 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|-----------|-------------|------|--------|-------------|-----------------|
| 33 | 11/13/87 | ALK | 481. | CU | 0 | P04 | 1.18 |
| | | AL | 0 . | CN | 0 | K | 22.44 |
| | | NH3 | .11 | F | .51 | RESD | -6.161 |
| | | AS | .005 | ALFA | 17. | SE | 0 |
| | | BA | .07 | BETA | 17. | \$102 | 57.95 |
| | | 38 | 0 | OH | 0 | - AG | 0 |
| | | HC03 | 587. | FE | .04 | SAR | 2.199 |
| | | В | . 25 | PB | 0 | NA | 142.04 |
| | | CD | 0 | LI | .11 . | . \$04 | 490. |
| | | CA | 219.70 | MG | 58.66 | SURF | 0 |
| | | C03 | 0 | MN | .04 | TDS | 1335. |
| | | CL | 81.90 | HG | 0 | KJEL | .18 |
| | | CR | 0 | MO | 0 | VA | .008 |
| | | CO | 0 | NI | 0 | ZH | 0 |
| | | COND | 2030. | NO3 | 1.53 | PH | 7.50 |
| | | | | | | | • |
| 34 | 03/16/88 | ALK | 406. | cu | 0 | P04 | 2.07 |
| - | ,, | AL | 0 | CN | 0 | K | 11.78 |
| | | NH3 | .10 | ·F | .68 | RESD | -6.574 |
| • | | AS | .022 | ALFA | 0 | SE | 0 |
| | | BA | .02 | BETA | 10. | SI02 | 45.55) |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 495. | FE | Ŏ. | SAR | 1.011 |
| | | В | .21 | PB | 0 % | NA NA | 63 |
| | | CD | 0 | LI | .09 | 504 | 375. |
| | | CA | 212.80 | HG | 49.52 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 1043. |
| | | CL | 66.80 | HE | 0 | KJEL | .15 |
| | | | | MO | 0 | VA | .012 |
| | | CR | 0 | | 0 | | |
| | | CO | 0 | NI | | ZN | 0 |
| | | COND | 1580. | NO3 | 1.62 | ₽H | 7.20 |
| 35 | 06/07/88 | ALK | | CU | 0 | P0 4 | 2 25 |
| 33 | 00/07/00 | | 415. 0 | CN | 0 | K K | 2.25 |
| | | AL NH3 | .04 | . F | .60 | RESD | 11.59 -3.898 |
| | | | | ALFA | | SE | |
| | | AS | .029 .04 | BETA | 0 0 | \$102 | 0 44.90 |
| | | BA BE | | | | AG | |
| | | | 0 | 0H | 0 | | 0 |
| | | HCO3 | 506. | FE | 0 , | SAR | 1.946 |
| | | 8 | .20 | PB | 0 | NA SOA | 110.49 |
| | | CD | 0 | LI | .08 | S04 | 353. |
| | | CA | 219.20 | MG | 15.30 | SURF | 0 |
| | | C03 | 0 | MN | 0 | IDS | 1035. |
| | | CL | 59.20 | HG | 0 | KJEL | .08 |
| | | CR | .002 | MO | 0 | VA TH | .03 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 1570. | NO3 | 3.70 | PH | 7.40 |

WELL #6 - CHEMICAL ANALYSES

| | | | | - | | | | |
|------|----------|------|--------|-------|-------|----|-----------|--------|
| CASE | MO-DA-YR | | | | | | | |
| 36 | 10/07/88 | ALK | 400. | CU | 0 | p | 04 | 2.87 |
| | | AL | 0 | CN | 0 | ĸ | | 11.46 |
| | | NH3 | .06 | F | . 49 | | ESD | -4.248 |
| | | AS | .016 | ALFA | 0 | | Ε | 0 |
| | | BA | .04 | BETA | 8. | | 102 | 41.92 |
| | | BE | 0 | OH | 0 | | 6 | 0 |
| | | HC03 | 488. | FE | 0 | | AR | 1.861 |
| | | В. | .19 | PB | Ö | | A A | 105.89 |
| | | CD | 0 | LI | .09 | | 04 | 364. |
| | | CA | 201.60 | MG | 26.64 | | URF | 0 |
| | | COS | 0 | | | | | 1025. |
| | | | 61.50 | MK MK | 0 | | DS TEL | |
| | | CL | | HG | 0 | | JEL | .09 |
| | | CR | .002 | MO | 0 | | A | 0 |
| | | CO | 0 | NI | 0 | | N | 0 |
| | | COND | 1580. | NO3 | 1.44 | | Н | 7.80 |
| | | | | | | | | |
| 37 | 03/23/89 | ALK | 362. | cu | 0 | Р | 04 | 3.80 |
| | | AL | 0 | CN | 0 | K | | 10.54 |
| | | NH3 | .08 | F | . 59 | | ESD | -4.359 |
| | | AS | .02 | ALFA | 0 | | E | 0 |
| | | BA | .04 | BETA | 5. | | 102 | 42.07 |
| | | BE | 0 | OH | . 0 | | 6 | 0 |
| | | HC03 | 442. | FE | O. | | AR | 1.776 |
| | | 8 | .19 | P8 | 0.5 | | A | 98.37 |
| | | CD | 0 | LI | .08 | | n 94 | 317. |
| | | CA | 217.60 | WG | 9.12 | | URF | 0 |
| | | CO3 | 0 | | | | | |
| | | | | MN | 0 | | DS | 946. |
| | • | CL | 76. | HG | 0 | | JEL | .10 |
| | | CR | 0 | HO | 0 | V | | 0 |
| | | CO | 0 | NI | 0 | 1 | | 0 |
| | | COND | 1450. | NO3 | 1.44 | ρ | H | 7.40 |
| | | | | | | | | |
| 38 | 05/15/89 | ALK | 387. | CU | . 0 | ρ | 04 | 3.25 |
| | | AL | 0 | CN | .003 | K | | 11.65 |
| | | NH3 | .07 | F | .73 | R | ESD | -3.822 |
| | | AS | .029 | ALFA | 0 | ·S | Ε | 0 |
| | | BA | .04 | BETA | 0 | S | 102 | 41.90 |
| | | BE | . 0 | OH | 0 | A | | 0 |
| | | HC03 | 472. | FE | 0 | | AR | 1.951 |
| | | В | .18 | PB | 0 | | A | 107.85 |
| | | CD | 0 | LI | .09 | | D4 | 336. |
| | | CA | 152.60 | HG | 48. | | URF | 0 |
| | | C03 | 0 | HN | 0 | | DS | 965. |
| | | CL | 59. | HG | 0 | | JEL | .10 |
| | | CR | 0 - | HO | 0 | | | .03 |
| | | CO | .02 | HI | 0 | Zi | | 0 |
| | | COND | 1480. | . NO3 | 1.63 | PI | | 7.60 |
| | | | 41001 | 1100 | **** | r: | , | 7.00 |

| CASE | MO-DA-YR | | | | • | | | | |
|------|----------|-------|-----------|---|------|------------|---|-------|--------|
| 39 | 09/11/89 | ALK | 389. | | CU | ٨ | | P04 | 3.20 |
| 37 | V7/11/07 | AL | 367. 0 | | CN | 0 | | X | 10.90 |
| | | NH3 | .10 | | F | .55 | | RESD | -4.030 |
| | | AS | .029 | | ALFA | 4. | | SE | 0 |
| | | BA | .04 | | BETA | 7. | | SIO2 | 43.87 |
| | | 38 | 0 | | DH | 0 | | AG | 0 |
| | | HCO3 | 474. | | FE | 0 | | SAR | 2.04 |
| | | 8 | 21 | | PB | 0 | | NA | 113.92 |
| | | CD | 0 | | LI | .09 | | S04 | 360. |
| | | CA | 154.80 | | MG | 49.62 | | SURF | 0 |
| | | CO3 · | 0 | | MN | 0 | | TDS | 990. |
| | | CL | 58.30 | | HG | 0 | | KJEL | .11 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | 0 |
| | • | COND | 1500. | | NO3 | 1.54 | | PH | 7.40 |
| | | COND | 1300. | | HUS | 1.34 | | РΠ | 7.40 |
| | | | | | | | | | |
| 40 | 10/11/89 | ALK | 403. | | Cυ | 0 | | P04 | 3.15 |
| | | AL | 0 | | CN | 0 | | K | 11.29 |
| | | NH3 | 0 | | F | .57 | | RESD | -4.414 |
| | | AS | .023 | | ALFA | 3. | | SE | 0 |
| | | BA | . 04 | | BETA | 3. | | \$102 | 44.77 |
| | | BE | 0 | | OH | ^ | | AG | . 0 |
| | | HCO3 | 492. | | FE | , U ,05 | | SAR | 1.975 |
| | | В | .19 | | PB | 0 5 | | NA | 113.42 |
| | | CD | 0 | | LI | .09 | | S04 | 380. |
| | | CA | 165.40 | | MG | 51.43 | | SURF | 0 |
| | | C03 | 0 | | MN | 0 | • | TDS | 1050. |
| | | CL | 56.70 | | HG | Ō | | KJEL | 0 |
| | | CR | 0 | | MO | 0 | | VA | .01 |
| | | CO | Ö | | NI | Ö | | ZN | 0 |
| | | COND | 1550. | | NO3 | 1.63 | | PH | 7.00 |
| | | | | | | | | | |
| 41 | 03/26/90 | ALK | 442. | | CU | 0 | | P04 | 4. |
| | | AL | 0 | | CN | 0 | | K | 11.57 |
| | | NH3 | .09 | | F | .47 | | RESD | -5.218 |
| | | AS | .03 | | ALFA | 3. | | SE | 0 |
| | | BA | . 05 | | BETA | 8. | | SI02 | 39.65 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 539. | | FE | .06 | | SAR | 2.038 |
| | | В | .21 | | ₽B | 0 | | NA | 124.20 |
| | | CD | 0 . | | LI | .10 | | S04 | 365. |
| | | CA | 191.60 | | MG | 54.68 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | TDS | 1252. |
| | | CL | 60.70 | | HG | 0 | | KJEL | .10 |
| | | CR | 0 | | MO | 0 | | ۷A | 0 |
| | | CO | 0 | | HI | 0 | | ZN | 0. |
| | | COND | 1533. | • | NO3 | 1.23 | | PH | 7.80 |

| CASE | MO-DA-YR | | • | • | | | |
|------|----------|------|--------------|-------|-------------|---------------|--------|
| 42 | 07/05/90 | ALK | 434. | CU | 0 | P04 | 4.60 |
| | | AL | . 0 | CN | 0 | K | 10.47 |
| | | NH3 | . 40 | F. | .52 | RESD | -4.939 |
| | | AS | . 036 | ALFA | 6. | SE | 0 |
| | | BA | .04 | BETA | 9. | \$102 | 42.61 |
| | | 8E | 0 | OH | 0 | AG | 0 |
| | • | HCO3 | 529 . | FE | 0 . | SAR | 1.929 |
| | - | 8 | .20 | PB | 0 | NA | 115.75 |
| | | CD | 0 | · LI | .08 | \$04 | 426. |
| | | CA | 181.70 | MG | 55.30 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 1180. |
| | | CL | 65. | HG | 0 | KJEL | 1.38 |
| | | CR | 0 | MO | 0 | VA | .01 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 1200. | NO3 | 1.48 | PH | 7.08 |
| | | | | | | | |
| | | | | | | | |
| 43 | 10/18/90 | ALK | 523. | CU | .03 | P04 | 5.60 |
| | | AL | .07 | CN | 0 | K | 13.67 |
| | | NH3 | . 04 | F | . 49 | RESD | -6.543 |
| | | AS | . 033 | ALFA | 4. | SE | 0 |
| | | BA | .073 | BETA | 8. | S1 0 2 | 5.90 |
| | | BE | .001 | OH | ·. 0 | AG | 0 |
| | | HCO3 | 638. | FE | .18 | SAR | .51 |
| | | В | .10 | PB | .007 | NA | 176 |
| | | CD | 0 | LI | .12 | S04 | 507. |
| | | CA | 218. | MG | 74.50 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 1488. |
| | | CL | 69. | He | 0 | KJEL | .12 |
| | | ÇR | 0 | MO | 0 | VA | .01 |
| | | CO | 0 | ΝI | 0 | ZN | .10 |
| | | COND | 1434. | · NO3 | 1.36 | PH | 7.20 |
| | | | | | | | |

WELL #6 - CHEMICAL ANALYSES

| AVERAGES | 05/03/78 | TO 01/09/91 | | | | |
|----------|----------|-------------|------|--------|------|---------|
| | ALK 37 | 71.2 | CU | .004 | P04 | .141 |
| | AL | .035 | CN | .002 | K | 10.941 |
| | NH3 | .17 | F | .689 | RESD | -21.892 |
| | AS | .01 | ALFA | 2.4 | SE | .00 |
| | BA | .067 | BETA | 6.3 | SI02 | 38.633 |
| | 8E | .00 | OH | 0 | AG | .00 |
| | | 53.7 | FE | .031 | SAR | 1.909 |
| | 8 | .197 | PB | .002 | NA | 102.47 |
| | CD | .00 | LI | .076 | S04 | 304. |
| | | 4.93 | MG | 36.807 | SURF | .003 |
| | C03 | .03 | MN | . 004 | TDS | 917. |
| | CL 5 | 9.62 | HG | .0001 | KJEL | .391 |
| | CR | .002 | MO | .001 | VA | .006 |
| | CO | .002 | NI | .001 | ZN | .008 |
| | COND 133 | | NO3 | 1.399 | PH | 7.53 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|-------|-------|-------|-------|-------|--------|
| 1 | 06/14/84 | ALK | 180. | | CU | .009 | P04 | .09 |
| | | AL | . 005 | | CN | 0 | K | 6. |
| | | NH3 | .22 | | F | .36 | RESD | .62 |
| | | AS | 0 | | ALFA | 6. | SE | 0 |
| | | BA | . 35 | | BETA | 11. | \$102 | 58. |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 219.6 | | FE | .12 | SAR | .449 |
| | | В | .05 | | PB . | .03 | NA | 15 |
| | | CD | .01 | | LI | .01 | S04 | 18. |
| | | CA | 59. | | MG | 15.50 | SURF | 0 |
| | | C03 | 0 | | HN | 0 | TOS | 268. |
| | | CF | 40.80 | | HG | 0 | XJEL | . 35 |
| | | CR | 0 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | .05 | ZN | .049 |
| | • | COND | 420. | | NO3 | .58 | PH | 7.10 |
| - | | | | | | | | |
| 2 | 08/22/84 | ALK | 165. | | CU | .021 | P04 | 0 |
| | | AL | . 05 | | CH | 0 | K | 5.96 |
| | | NH3 | .10 | | F | .18 | RESD | -1.180 |
| | | AS | .005 | | ALFA | 4. | SE | 0 |
| | | BA | . 07 | | BETA | 7. | \$102 | 51.25 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 201. | | FE | ,09 | SAR | 3.054 |
| | | В | .099 | • | PB | .04 | NA | 105 |
| | | CD | 0 | | LΙ | .008 | \$04 | 250. |
| | | CA | 60. | | MG | 18. | SURF | 0 |
| | | C03 | 0 | | MM | .01 | IDS | 580. |
| | | CL | 32. | | HG | .0005 | KJEL | .14 |
| | | CR | 0 | | MO | 0 | VA | .006 |
| | | CO | Ō | | NI | .02 | ZN | .037 |
| | | COND | 880. | | NO3 | 1.60 | PH | 7.20 |
| | | | | | | | | |
| 3 | 06/17/85 | ALK | 163. | | CU | 0 | P04 | .08 |
| | | AL | 0 | | CN | 0 | K | 6.46 |
| | | NH3 | .10 | | F | . 26 | RESD | .917 |
| | | AS | . 004 | | ALFA | 11. | SE | 0 |
| | | BA | . 07 | | BETA | 23. | \$102 | 57.28 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 199. | | FE | .03 | SAR | 1.865 |
| | | В | .11 | | PB | .008 | NA | 62 |
| | | CD | .002 | | LI | .009 | S04 | 120. |
| | | CA | 64. | | MG | 12. | SURF | 0 |
| | | CO3 | 0 | | HN | .02 | TDS | 450. |
| | | CL | 42.40 | | HG | 0 | KJEL | .18 |
| | | CR | 0 | | 10 MO | .01 | VA | 0 |
| • | | CO | 0 | • • • | NI | . 0 | ZN | .012 |
| | | COND | 700. | | H03 | .15 | PH | . 7.45 |

| CASE | MO-DA-YR | | | • | | | |
|------|------------|--------------|-------------|------------|---------|------------|----------|
| | 08/19/85 | AI V | 144 | CH - | | P04 | .04 |
| 4 | 70) 17) 03 | ALK AL | 164. 0 | CU - Cn | 0 | K | 4.60 |
| | | NH3 | .30 | F | .28 | RESD | -0.564 |
| | | AS | .003 | | 0 | SE | 0.364 |
| | | BA | .003 | ALFA | | \$102 | 58.40 |
| | | BE | 0 | BETA | 4. 0 | AG | 0 |
| | | HCO3 | | OH FE | .03 | SAR | .626 |
| | | | 200. .04 | | | NA NA | 20 |
| | | 8 | | PB | .014 | S04 | |
| | | CD | .001 | LI | .009 | SURF | 16. 0 |
| | | CA | 62.40 | MG | 8.88 | | 285. |
| | | C03 | 0 | HN. | 0 | TDS | |
| | | CL | 45. | HG | 0 | KJEL | . 44 |
| | | CR | 0 | MO | .01 | VA | 0 |
| | | CO | 0 | HI | 0 | ZN | .023 |
| | | COND | 443. | N03 | .74 | PH | 7.65 |
| | | | | | | | |
| 5 | 11/20/85 | ALK | 163. | CU | 0 | P04 | .08 |
| | | AL | 0 | CN | 0 | Κ . | 6.36 |
| | | NH3 | 0 | F | .30 | RESD | -0.776 |
| | | AS | 0 | ALFA | 0 | SE | 0 . |
| | | 8A | .05 | BETA | 0 | \$102 | 54.52 |
| | | BE | 0 | OH | ·. 0 | AG | 0 |
| | | HC03 | 199. | FE | 747 | SAR | .352 |
| | | 8 | .06 | PB | .004 | NA | 11.50 |
| | | CD | 0 | LI | 009 | S04 | 18. |
| | | CA | 64.80 | MG | 9.80 | SURF | 1.65 |
| | | C03 | 0 | MN | 0 | TDS | 316. |
| | | CL | 40.30 | HG | 0 | KJEL | .30 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | . 0 | ZN | 0 |
| | | COND | 448. | NO3 | .77 | . РН | 8.55 |
| | | | | | | | |
| 6 | 03/13/86 | ALK | 158. | CU | 0 | P04 | .08 |
| | | AL | .11 | CN | 0 | K | 5.86 |
| | | NH3 | 0 | F . | . 28 | RESD | -0.717 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .06 | BETA | 7. | \$102 | 56.76 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 193. | FE | .05 | SAR | .406 |
| | | 8 | .11 | PB | .006 | NA | 13.02 |
| | | CD | 0 | LI | .008 | \$04 | 12. |
| | • | CA | 62.80 | MG | 9.10 | SURF | 0 |
| | | CO3 | . 0 | MN | 0 | TDS | 245. |
| | | CL | 38.70 | HG | 0 | KJEL | .12 |
| | | CR | . 0. | MQ | . 0 | VA | 0 |
| | • | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 375. | NO3 | .69 | "PH | 7.81 |
| | | - | | · | | | |

| CASE | MO-DA-YR | | | . • | | | | |
|------|----------|------|-------|------|-------------|---|---------------|--------|
| 7 | 05/29/86 | ALK | 162. | cu | 0 | | P04 | .04 |
| | | AL | 0 | CH | 1.756 | | K | 6. |
| | | NH3 | .04 | F | .29 | | RESD | .66 |
| | | AS | .004 | ALFA | 0 . | | SE | 0 |
| | | BA | .07 | BETA | 8. | | SI02 | 55.81 |
| | | BE | 0 | OH | 0 | | AG | 0 |
| | | HCO3 | 198. | FE | 0 | | SAR | . 362 |
| | | 8 | .07 | PB | 0 | | NA | 11.60 |
| | | CD | 0 | LI | .015 | | S04 | 18. |
| | | CA | 63.20 | MG | 9.10 | | SURF | 0 |
| | | C03 | 0 | MN | 0 | | TDS | 304. |
| | | CL | 38.70 | HG | 0 | | KJEL | . 07 |
| | | CR | .001 | MO | 0 | | VA | . 0 |
| | | CO | 0 | NI | 0 | | ZN | .015 |
| | | COND | 470. | NO3 | .79 | | PH | 7.90 |
| | | | • | | | | | |
| 8 | 07/17/86 | ALK | 160. | CU | 0 | | P04 | .15 |
| | | AL | 0 | CN | 0 | | K | 6.62 |
| | | NH3 | . 20 | F | . 26 | | RESD | -0.779 |
| | | AS | .004 | ALFA | 0 | | SE | 0 |
| | | BA | .06 | BETA | 26. | | SI 0 2 | 61.07 |
| | | BE | 0 | OH | . 0 | | AG | 0 |
| | | HC03 | 195.2 | FE | ~ 02 | | SAR | .467 |
| | | В | .07 | PB | 0 7 | | NA | 15.14 |
| | | CD | 0 | LI | .01 | • | S04 | 6. |
| | | CA | 55.20 | MG | 14.90 | | SURF | 0 |
| | | C03 | 0 | MN | 0 | | TDS | 285. |
| | | CL | 50. | HG | 0 | | KJEL | .35 |
| | | CR | 0 | MO | 0 | | VA | 0 |
| • | | CO | Ō | NI | Ö | | ZN | .09 |
| | | COND | 400. | NO3 | .26 | | PH | 7.60 |
| | | | | | | | | • |
| 9 | 10/14/86 | ALK | 160. | CU | 0 | • | P04 | . 12 |
| .: | | AL | 0 | CN | 0 | | K | 7.20 |
| | | NH3 | . 43 | F | . 25 | | RESD | -0.657 |
| | | AS | .005 | ALFA | 0 | | SE | 0 |
| | | BA | .06 | BETA | 5. | | SI02 | 54.10 |
| | | BE | 0 | OH | 0 | | AG | 0 |
| | | HC03 | 195.2 | FE | 0 | | SAR | 11.70 |
| | | В | .08 | PB | .004 | | NA | 11.70 |
| | | ĊD | 0 | LI · | .009 | | S04 | 14. |
| | | CA | 54.40 | MG | 13.90 | | SURF | 0 |
| | | CO3 | 0 | HH | 0 | | TDS | 275. |
| | | CL | 40. | HG | 0 | | KJEL | .50 |
| | | CR | 0 | MO | . 0 | | VA | 0 |
| | • | CO | . 0 | NI | 0 | | ZN | .022 |
| | | COND | 430. | NO3 | .75 | • | PH | 7.80 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|------|-------|-------------|---------------|
| 10 | 02/13/87 | ALK | 158. | CU | 0 | P04 | .11 |
| | • | AL | 0 | CN | 0 | K | 6. |
| | | NH3 | .46 | F | . 34 | RESD | -0.620 |
| | | AS | 0 | ALFA | 5. | SE | . 0 |
| | | BA | .06 | BETA | 8. | \$102 | 59.64 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 192.7 | FE | 0 | SAR | .421 |
| | | 8 | .06 | PB | 0 | NA | 13.30 |
| | | CD | 0 | LI | 0 | S04 | 16. |
| | | CA | 53.60 | MG | 13.44 | SURF | 0 |
| | | C03 | 0 | MN | . 0 · | TDS | 245. |
| | | CL | 35. | HG | 0 | KJEL | .55 |
| | | CR | .012 | MO | 0 | VA | .015 |
| | | CO | 0 | NI | 0 - | ZN | .022 |
| | | COND | 380. | NO3 | .42 | PH | 7.80 |
| | | | | | | | |
| 11 | 06/22/87 | ALK | 182. | CU | 0 | P 04 | .11 |
| | | AL | .04 | CN | .73 | X | 6. |
| | | NH3 | .06 | F | . 28 | RESD | -0.258 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | . 06 | BETA | 11. | SI02 | 63.7 7 |
| | | 8E | . 0 | OH | 0 | AG | 0 |
| | | HCO3 | 222. | FE | . 02 | SAR | . 429 |
| | | В | .09 | PB | 0 ~. | NA | 12.86 |
| | | CD | 0 | LI | 0 | S04 | 14. |
| | | CA | 60. | Me | 11. | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 265. |
| | | CL | 27. | HG | 0 | KJEL | .10 |
| | | CR | 0 | HO | 0 | VA | 0 |
| | | CO | 0 | HI | .02 | ZN | .049 |
| | | COND | 390. | NO3 | .72 | PH | 7.60 |
| | | | | | • | | |
| 12 | 08/27/87 | ALK | 173. | CU | 0 | P04 | .09 |
| | | AL | .04 | ÇN | 0 | K | 5.89 |
| | | NH3 | .14 | F | .27 | RESD | -0.343 |
| | | AS | .005 | ALFA | 0 . | SE | 0 |
| | | BA | .06 | 8ETA | 11. | \$102 | 62.73 |
| | | 8E | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 211. | FE | 0 | SAR | . 552 |
| | | В | .07 | P8 . | .005 | NA | 17.50 |
| | | CD | 0 | ιī | 0 | \$04 | 16. |
| | | CA | 52.75 | MG | 14.24 | SURF | 0 |
| | | CO3 | 0 | MH | 0 | TDS | 251. |
| | | CL | 36.50 | HG | 0 | KJEL | .20 |
| | | CR | 0 . | MO | .0 | VA | 0 |
| • | | CO | 0 | NI | 0 | ZN | . 03 |
| | | COND | 390. | NO3 | .95 | ЬĤ | 7.40 |
| | | | | | | • | |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|-----------|-----------|----------|----------------|----------|-------------|
| 13 | 11/11/87 | ALK | 160. | CU | 0 | P04 | .13 |
| | | AL | 0 | CN | 0 | ĸ | 7.50 |
| | | NH3 | .07 | F | .14 | RESD | -0.897 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .05 | BETA | 9. | \$102 | 62.15 |
| | | BE | .002 | OH | 0 | AG | 0 |
| | | HCO3 | 195. | FE | 0 | SAR | . 426 |
| | | 8 | .02 | PB | 0 | NA | 14.02 |
| | | CD | 0 | ŧΙ | 0 | \$04 | 25. |
| | | CA | 57.18 | MG | 15.10 | SURF | 0 |
| | | CO3 | 0 | MN . | 0 | TDS | 255. |
| | | CF | 38.40 | HG | 0 | KJEL | .11 |
| | | CR | 0 | MO | 0 | . VA | 0 |
| | | CO | 0 | HI | 0 . | ZN | 0 |
| | | COND | 385. | H03 | 2. | PH | 7.80 |
| | | | | | | | |
| 14 | 03/30/88 | ALK | 152. | CU | 0 | P04 | .04 |
| | | AL | 0 | CN | 0 | K | 5.96 |
| | | NH3 | 0 | F | .25 | RESD | -0.952 |
| | | AS | .005 | ALFA | 0 | SE | 0 |
| | | BA | .06 | BETA | 8. | \$102 | 63.21 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | | HC03 | 185. | FE | Q _: | SAR | . 399 |
| | | В | .06 | PB | 0 5. | NA | 12.96 |
| | | CD | 0 | LI | 0 | \$04 | 24. |
| | | CA | 73.60 | MG | 3.80 | SURF | 0 |
| | | CO3 | 0 | MN | 0 . | TDS | 300. |
| | | CL | 38.40 | H6 | 0 | KJEL | 0 |
| | | CR | 0 | MO | 0 | VA | .028 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | COND | 385. | NO3 | .60 | PH | 7.80 |
| 15 | 06/13/88 | ALK | 154 | CU | ٥ | P04 | ۸۵ |
| 13 | 00/13/00 | AL | 156. 0 | CH | 0 | rua K | .08 6.32 |
| | | HL NH3 | .05 | F | .005 .25 | RESD | -0.868 |
| | | AS | .004 | ALFA | 0 | SE | 0.008 |
| | | BA | .07 | BETA | 0 | \$102 | 60.75 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 190. | FE | 0 | SAR | .369 |
| | | 8 | .03 | P8 | .004 | NA | 11.97 |
| | | CD | 0 | LI | 0 | S04 | 17. |
| | | CA | 68.80 | MG | 6.70 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 255. |
| | • | CL | 39.40 | HG | 0 | KJEŁ | .06 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI NI | 0 | ZN | .01 |
| | | COND | 390. | NO3 | .68 | PH | 8.00 |
| | | COND | 370. | nus | .00 | rn | 0.00 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------------|--------------------|----------------|------------|----------------|-----------|
| 16 | 10/07/88 | ALX | 160. | cu | 0 | P04 | .10 |
| | , , | AL | 0 | CN | Ō | K | 6.53 |
| | | NH3 | . 0 | F | .57 | RESD | 1.499 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .06 | BETA | 0 | \$102 | 59.96 |
| - | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 195. | FE | 0 | SAR | .367 |
| | | 8 | .03 | PB | .003 | NA | 12.93 |
| | | CD | . 0 | LI | 0 | S04 | 15. |
| | | CA | 70.40 | MG | 14.40 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 280. |
| | | CL | 63. | HG | 0 | KJEL | 0 |
| | | ER | . 0 | 0 K | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| • | | COND | 450. | N03 | .58 | PH | 8.10 |
| 4.7 | 07/07/00 | | | | | • | |
| 17 | 03/23/89 | ALK | 62. | CU | 0 | P04 | .15 |
| | | AL | 0 | CH | 0 | K | , 6.15 |
| | | NH3 | .05 | F | .57 | RESD | -2.417 |
| | | AS | 0 | ALFA | 4. | 38 | 0 |
| | | BA | .06 0 | BETA | 6. | \$102 | 60.22 |
| | | BE HCO3 | 198. | 0H | 0 | AG | 0 |
| | | B | .03 | FE PB | 0 | SAR | .313 |
| | | CD | 0 | LI | 0 | NA SD4 | 12.12 |
| | | CA | 104. | MG | 5.76 | S04 SURF | 86. O |
| | | C03 | 0 | MN | 0 | TOS | 360. |
| | • | CL | 42.20 | HG | Ö | KJEL | .20 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CD | 0 | NI | Ö | ZN - | .03 |
| | | COND | 560. | NO3 | .70 | PH | 7.70 |
| | | | | | | , | |
| 18 | 06/05/89 | ALK | 158. | CU | 0 | P04 | .15 |
| | | AL | | CH | 0 | K | 6.33 |
| | | NH3 | .06 | . F | .31 | RESD | -0.898 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .06 | BETA | 7. | \$102 | 59.34 |
| | | 8E | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 193. | FE | 0 | SAR | 4.174 |
| • | | B CD | .06 0 | PB | 0 | NA SO4 | 13.67 |
| | | CA | 5 6 .20 | LI MG | .02 | \$04 \$110E | 19. |
| | | CO3 | 0 | NN NO | 15.31 0 | SURF | 0 255. |
| | | CL | 42.20 | HG | 0 | TDS Kjel | .08 |
| | | CR | 0 | HO | 0 | VA | 0 |
| | | CO | Ŏ | NI | 0 | ZN | .03 |
| | | COND | 400. | HO3 | .72 | PH | 7.40 |
| | | 70.10 | | 1100 | . / 4 | rıı | |

| CASE | MO-DA-YR | | | | • | | | | |
|------|------------|------|-------|-----|------|-------|---|-------|--------|
| 19 | 09/11/89 | ALK | 158. | (| CU | 0 | | P04 | .09 |
| | | AL | 0 | | CN | 0 | | X | 5.95 |
| | | NH3 | .07 | | F | .31 | | RESD | -0.750 |
| | | AS | .006 | \$ | ALFA | 0 | | SE | . 0 |
| | | BA | .06 | 1 | BETA | 9. | - | S102 | 62.25 |
| | | BE | 0 | | 3H | Ö | | AG | 0 |
| | | HCO3 | 193. | | FE | 0 | | SAR | . 38 |
| | | В | . 04 | | PB | 0 | | NA | 12.23 |
| | | CD | 0 | | LI | 0 | | S04 | 15. |
| | | CA | 53.19 | | MG | 15.29 | | SURF | 0 |
| | | CO3 | 0 | | HN | 0 | | TDS | 310. |
| | | CL | 42.60 | | 16 | 0 | | XJEL | .10 |
| | | CR | 0 | | 10 | .06 | | VA | 0 |
| | | CO | 0 | | ΗI | 0 | | ZN | .02 |
| | | COND | 397. | . 1 | NO3 | .71 | | PH | 7.80 |
| 20 | 10/13/89 | ALK | 167. | (| CU | 0 | | PO4 | 0 |
| 20 | 10/10/07 | AL | 0 | | CN | . 0 | | K. | 6.20 |
| | | NH3 | Ö | | F. | .29 | | RESD | -0.699 |
| | | AS | ŏ | | ALFA | 0 | | SE | 0 |
| | | BA | .06 | | BETA | 7. | | \$102 | 58.76 |
| | | 8E | 0 | | DH | 0 | | AG | 0 |
| | | HC03 | 204. | | FE | ۸ | | SAR | .406 |
| | | В | .02 | | PB | 0 %. | | NA | 13.29 |
| | | CD | 0 | | LI | 0 | | S04 | 14. |
| | | CA | 55.94 | | 46 | 15.25 | | SURF | 0 |
| | | C03 | 0 | | 4N | 0 | | TDS | 320. |
| | | CL | 39.80 | | 16 | 0 | | KJEŁ | 0 |
| | | CR | 0 | | 40 | 0 | | VA | .01 |
| | | CO | 0 | | ١I | 0 | | ZN | .08 |
| | | COND | 448. | ١ | 103 | .72 | | PH | 7.70 |
| 21 | 04/02/90 | ALK | 173. | · | CU | 0 | | P04 | .07 |
| 21 | V4 V2 7V | AL | 0 | | CN | 0 | | X | 5.81 |
| | | NH3 | . 04 | | F | .41 | | RESD | -0.348 |
| | | AS | 0 | | ALFA | 0 | _ | SE | 0 |
| | • | BA | .05 | | BETA | 0 | • | \$102 | 60.78 |
| | | BE | 0 | | OH. | 0 | | AG | 0 |
| | | HCO3 | 211. | | FE | 0 | | SAR | . 458 |
| | | 8 | .02 | | 98 | 0 | | NA | 14.53 |
| | | CD | .002 | | I | 0 | | S04 | 14. |
| | | CA | 53.01 | | 1G | 14.14 | | SURF | 0 |
| | | C03 | 0 | | 4N | 0 | | TDS | 338. |
| | | CL | 39.90 | | 16 | 0.00 | | KJEL | |
| | • | CR | 0 | h | 10 | 0 | | VA | .02 |
| | | CO | 0 | | ΝI | 0 | | ZH | .07 |
| | | COND | 446. | | 103 | .61 | | PH | 7.70 |

PEI #1 WELL - CHEMICAL ANALYSES

| CASE | MO-DA-YR | | | • | | | |
|------|----------|-------|--------|------|------------|------------|-------------|
| 22 | 07/06/90 | ALK | 154. | CU | 0 | P04 | .07 |
| | | AL | 0 | CH | 0 | K | 5.41 |
| | , | NH3 | . 08 | F | .27 | RESD | -0.754 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .06 | BETA | 0 | \$102 | 59.53 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 188. | FE | 0 | SAR | . 426 |
| | | В | 0 | PB | 0 | NA | 13.57 |
| | | CD | 0 | LI | 0 | \$04 | 18. |
| | | CA | 52.13 | MG | 15.03 | SURF | 0 |
| | | C03 | 0 | HN | 0 | TDS | 350. |
| | | CL | 41.90 | HG | 0 | KJEL | .40 |
| | | CR | 0 | HO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .02 |
| 1 | | COND | 366. | NO3 | .66 | PH | 7.63 |
| 23 | 10/18/90 | ALK | 163. | CU | .03 | P04 | .08 |
| 23 | 10/18/70 | AL | .49 | CN | . u s 0 | | |
| | | NH3 | .05 | F | .34 | K NEED | 6.81 |
| | | AS | .006 | ALFA | . 34 | RESD SE | -1.171 0 |
| | | BA | .062 | BETA | • | SI02 | 32.78 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 199. | FE | _13 | SAR | .41 |
| | | 8 | .14 | PB | .10 | . NA | 11.96 |
| | | CD | 0 | LI | .01 | S04 | 16. |
| | | CA | 61.04 | MG | 16.89 | SURF | .14 |
| | | C03 | 0 | HN | 0 | TDS | 344. |
| | | CL | 35.70 | HG | 0 | KJEL | .05 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | Ö | NI | Ö | ZN | .72 |
| | | COND | 347. | NO3 | .67 | PH | 7.90 |
| | | VUITE | V 17 1 | nyo | | , ,, | |

PEI #1 WELL - CHEMICAL ANALYSES

| AVERAGES | 06/14/8 | 84 TO 01/09/91 | | | | |
|----------|------------|----------------|------|--------|-------|--------|
| | ALK | 158.7 | CU | .003 | P04 | .085 |
| | AL | .033 | CN | .108 | K | 6.17 |
| | NH3 | .11 | F | .307 | RESD | -0.520 |
| | AS | .002 | ALFA | 1.9 | SE | 0 |
| | 8A | .073 | BETA | 7.6 | \$102 | 57.959 |
| | BE | .00 | OH | 0 | AG | 0 |
| | HCO3 | 199.0 | FE | .026 | SAR | 1.253 |
| | B . | .059 | Р8 | .006 | NA | 19.65 |
| | CD | .001 | ŧΙ | .005 | S04 | 34. |
| | CA | 61.637 | MG | 12.501 | SURF | .078 |
| | CO3 | 0 | MN | .001 | TDS | 310. |
| | · CL | 40.43 | HG | .0001 | KJEL | .195 |
| | CR | .001 | МО | .003 | . VA | .003 |
| | CO | 0 | NI | .004 | ZN | . 059 |
| | COND | 448. | NO3 | .742 | PH | 7.71 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UNHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | - | | | |
|------|----------|------|--------|--------|--------|---------------|---------|
| 1 | 06/14/84 | ALK | 764. | cu | .045 | P04 | .11 |
| | | AL | .011 | CN | 0 | K | 23.60 |
| | | NH3 | . 40 | F | .24 | RESD | 14.69 |
| | | AS | 0 | ALFA | 23. | SE | 0 |
| | | BA | .24 | BETA | 15. | . SIO2 | 69.50 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 932. \ | FE | .10 | SAR | 1.41 |
| | | В | . 07 | PB | .032 | NA | 126 |
| | | CD | .021 | LI | .04 | \$04 | 780. |
| | | CA | 413. | MG | 113.90 | SURF | 0 |
| | | CO3 | 0 | MN | .02 | TDS | 2100 |
| | | CL | 14.90 | HG | 0 | KJEL | . 85 |
| | | CR | .01 | MO | .04 | ٧A | 0 |
| | | CD | 0 | NI | .07 | ZN | .102 |
| | | COND | 3200. | NO3 | 1.99 | PH | 7.25 |
| _ | | | | | | | |
| 2 | 08/22/84 | ALK | 750. | CU | .014 | PO4 | . 18 |
| | | AL | 0 | CH | 0 | K | 23.80 |
| | | NH3 | .10 | F | .09 | RESD | -15.420 |
| | | AS | .004 | ALFA | 38. | SE | .012 |
| | | BA | .07 | BETA | 16. | \$102 | 31.50 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 915. | FE | .01 | SAR | 1.383 |
| - | • | В | . 206 | . PB | .11 | NA | 124 |
| | • | CD | 0 | LI | .039 | 804 | 790. |
| | | CA | 410. | M6 | 121.20 | SURF | 0 |
| | | CO3 | 0 | HH | .02 | TDS | 2105. |
| | | CL | 160. | HG | .0007 | KJEL | . 25 |
| | | CR | .01 | MO | 0 | VA | .02 |
| | | CO | 0 | HI . | . 06 | ZN | .066 |
| | | COND | 3200. | NO3 | . 59 | PH | 7.80 |
| 3 | 06/17/85 | ALK | 565. | CU | 0 | P04 | . 56 |
| _ | | AL | 0 | CN | 0 | Х | 24.69 |
| | | NH3 | ^ | F | .15 | RESD | -13.345 |
| | | AS | .021 | ALFA | 48. | SE | .004 |
| | | BA | .05 | BETA | 24. | \$102 | 68.87 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 689. | FE | 0 | SAR | 2.602 |
| | | В | .24 | PB | 0 | NA | 210 |
| | | CD | 0 | LI | .04 | S04 | 904. |
| | | CA | 304. | MG | 115.20 | SURF | 0 |
| | | CO3 | 0 | MN | .03 | TDS | 2044. |
| | | CL | 18.40 | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | 0 | VA | .008 |
| | | CO | 0 | ΝΙ | 0 | ZN | .012 |
| | | COND | 3200. | . NO3 | 3.60 | PH | 7.25 |
| | | VUNU | OLVV. | . 1100 | U.UV | en en | 1.13 |

PEI #2.WELL - CHEMICAL ANALYSES

| AVERAGES | 06/14/ | 84 TO 01/09/91 | | | | |
|----------|--------|----------------|------|--------|--------|--------|
| | ALK | 693. | cu | . 02 | P04 | .283 |
| | AL | .004 | CN | 0 | K | 24.03 |
| | NH3 | .167 | F | .16 | . RESD | -4.692 |
| | AS | .008 | ALFA | 36.3 | SE | .005 |
| | BA | .12 | BETA | 18.3 | \$102 | 56.623 |
| | BE | 0 | ОН | 0 | AG | 0 |
| | HC03 | 845.3 | FE | .037 | SAR | 1.798 |
| | В | .172 | PB | .047 | NA | 153.33 |
| | CD | .007 | LI | .04 | S04 | 825. |
| | CA | 375.67 | MG | 116.77 | SURF | 0 |
| | C03 | 0 | ММ | .023 | TOS | 2083. |
| | CL | 64.43 | HG | .0002 | KJEL | .367 |
| • | CR | .007 | МО | .013 | VA | .009 |
| | CO | 0 | NI | .043 | ZN | .06 |
| | COND | 3200. | NO3 | 2.06 | PH | 7.43 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | | • | | | |
|------|----------|------|-----------|-----------------------|------|--------|----------|---------|
| 1 | 06/14/84 | ALK | 1270. | | CU | .033 | P04 | .04 |
| | , , | AL | .01 | | CN | 0 | K | 16.10 |
| | | NH3 | .29 | | F | .25 | RESD | 14.13 |
| | | AS | 0 | | ALFA | 0 | \$E | 0 |
| | | BA | .25 | | BETA | 12. | \$102 | 88. |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 1549.4 | • | FE | .09 | SAR | 7.12 |
| | | В | .10 | | PB | .016 | NA | 728 |
| | | CD | .028 | | LI | .04 | S04 | 2100. |
| | | CA | 590. | | MG | 122.80 | SURF | 0 |
| | | CO3 | 0 | | MN | .12 | TDS | 4430. |
| | | CL | 77.30 | | HG | 0 | KJEL | .70 |
| | | CR | .02 | • | MO | .03 | VA | .02 |
| | | CO | .02 | | NI | .02 | ZN | .192 |
| | | COND | 6800. | | NO3 | 2.04 | PH | 6.95 |
| _ | | | | | | | | |
| 2 | 08/22/84 | ALK | 1150. | | CU | .039 | P04 | .08 |
| | | AL | 0 · | | CN | 0 | K | 16.30 |
| | | NH3 | .10 | | F | .06 | RESD | -12.880 |
| | | AS | .006 | | ALFA | 0 | SE | .022 |
| | | BA | . 05 | | BETA | 8. | \$102 | 54.25 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 1403. | | FE | .07 | SAR | 6.879 |
| | | В | .188 | | PB | .16 | NA | 670 |
| | | CD | .002 | | LI | .044 | S04 | 1900. |
| | | CA | 476. | | MG | 147.60 | SURF | 0 |
| | | CO3 | 0 | | MN . | .09 | TDS | 4068. |
| | | CL | 124. | | HG | 0 | KJEL | .18 |
| | | CR | 0 | | MO | 0 | VA | 017 |
| | | CO | 0 . | | NI | .10 | ZH | .22 |
| | | COND | 6200. | | NO3 | .12 | PH | 7.15 |
| 3 | 06/17/85 | ALK | 1070. | | CU | 0 | PO4 | 2.40 |
| · | 00/11/03 | AL | 0 | | CN | 0 | K | 15.84 |
| | | NH3 | .02 | | F | .07 | RESD | 12.42 |
| | | AS | . 004 | | ALFA | 8. | SE | .004 |
| | | BA | .03 | | BETA | 14. | \$102 | 67.55 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCD3 | 1305. | | FE | Ö | SAR | 7.458 |
| | | В | .53 | | PB | 0 | NA NA | 705 |
| | | CD | .018 | | LI | .044 | · S04 | 2000. |
| | | CA | 480. | | MG | 120. | SURF | .50 |
| | | CO3 | 40V. 0 | | MN | .04 | IDS | 4006. |
| | | CL | 84.30 | | HG | | KJEL | .15 |
| | | CR | .03 | | MO | 0 | | |
| | | | | and the second second | | 0 | VA 7N | .007 |
| | | COND | (250 | | NI . | 0 | ZN | .016 |
| | | COND | 6250. | | NO3 | 1.49 | PH | 7.05 |

| | | | | - | | | |
|------|------------|-----------|-----------|-----------|-------------|----------------|----------|
| CASE | MO-DA-YR | | | | | | |
| 4 | 08/19/85 | ALK | 1180. | . cu | .03 | P04 | 3.50 |
| • | 00/17/03 | AL | 0 | CN | 0 | ¥ | 13.50 |
| | | NH3 | .15 | F | .10 | RESD | -12.210 |
| | | AS | .472 | , ALFA | 0 | SE | 0 |
| | | BA | .04 | | 0 | | 72.20 |
| | | | | BETA | 0 | \$102 | |
| | | BE | 0 | 0H | | AG | .001 |
| | • | HCO3 | 1440. | FE | .08 | SAR | 7.195 |
| | | 8 | .52 | PB | 0 | NA | 700 |
| | | CD | 0 | LI | .04 | 504 | 2030. |
| | | CA | 536. | MG | 110.40 | SURF | 0 |
| | | C03 | 0 | MN | .06 | IDS | 4250. |
| | • | CL | 84. | HG | 0 | KJEL | .23 |
| | | CR | 0 | HO | .01 | VA | .023 |
| | | CO | 0 | NI | 0 | ZN | . 205 |
| | | COND | 6500. | NO3 | 1.78 | PH | 7.20 |
| | | | | | <u>_</u> | | |
| 5 | 11/20/85 | ALK | 1105. | CU | .05 | P04 | 34. |
| • | 21, 20, 00 | AL | 0 | CN | 0 | X | 14.28 |
| | | NH3 | Ö | F | .09 | RESD | -14.457 |
| | | AS | .258 | ALFA | 0 | SE | .002 |
| | | BA | .04 | BETA | 0 | SI02 | 73. |
| | | BE | 0 | OH | . 0 | AG | 73. 0 |
| | | HCO3 | 1348. | FE | | SAR | 6.308 |
| | | B | .54 | PB | Q. 0 ⁵>. | | |
| | | | . 34 |) LI | .04 | NA SO4 | 620 |
| | | CD | | LI | | S04 | 1910. |
| | | CA | 620. | MG | 68.40 | SURF | 2.25 |
| | | C03 | 0 | MN | .02 | TDS | 4154. |
| | • | CL | 80.40 | HG | 0 | KJEL | .10 |
| | | CR | .004 | MO | .03 | VA | .023 |
| | | CO | 0 | NI | .13 | ZN | .216 |
| | | COND | 6120. | NO3 | 1.47 | PH | 7.00 |
| 6 | 03/13/86 | ALK | 1045. | CU | .04 | P04 | 35.50 |
| • | 74, 20, 00 | AL | 0 | CH | 0 | K | 15.09 |
| | | NH3 | 0 | F | .08 | RESD | -14.834 |
| | | AS | . 26 | ALFA | 0 | SE | .007 |
| | | BA | .04 | BETA | ŏ | \$102 | 75.60 |
| | | BE | 0 | 0H | Ŏ | AG AG | 0 |
| | | HCD3 | 1275. | FE | .18 | SAR | 6.992 |
| | | 8 | .63 | | 0 | | |
| | | CD | | PB | | NA SOA | 679.50 |
| | • | | .013 | LI | .041 | \$04 \$1105 | 1960. |
| | | CA CO3 | 566. 0 | MG Mu | 91.20 | SURF | 0 |
| | • | | | MN | .05 | TDS | 4126. |
| | | CL | 74.50 | HG | 0 | KJEL | .20 |
| | | CR | . 007 | MO . | 0 | VA 7N | .11 |
| | | COND | (200 | NI NOT | 0 | ZN | . 433 |
| | | COND | 6200. | ND3 | 2.05 | PH | 7.06 |

| | | | | | - | | | | • |
|------|----------|------|--------|---|------|--------|---|-------|---------|
| CASE | MO-DA-YR | | | | | | | | |
| 7 | 05/29/86 | ALK | 955. | | CU | . 05 | | P04 | 28. |
| | | AL | 0 | | CN | 0 | | K | 13.50 |
| | | NH3 | .64 | | F | .16 | | RESD | -14.130 |
| | | AS | .11 | | ALFA | 0 | | SE | 0 |
| | | BA | .03 | | BETA | 12. | | \$102 | 70.12 |
| | | BE | 0 | | OH | 0 | | AG | .001 |
| | | HCO3 | 1165. | | FE | .05 | | SAR | 6.358 |
| | | В | .59 | | PB | 0 | | NA | 595.80 |
| | | CD | .002 | | LI | .043 | | S04 | 1835. |
| | | CA | 482. | | MG | 111.60 | | SURF | 0 |
| | | CO3 | 0 | | MN | .06 | | TDS | 3720. |
| | | CL | 83.70 | | HG | 0 | | KJEL | .80 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | ZN | 1.284 |
| | | COND | 5700. | | NO3 | 3.40 | | PH | 7.15 |
| | | | | | | | | | |
| 8 | 07/17/86 | ALK | 778. | | cu | .02 | | P04 | 42. |
| | | AL | 0 | | CN | 0 | | K | 15.69 |
| | | NH3 | .08 | | F | .04 | | RESD | -16.035 |
| | | AS | .356 | | ALFA | 0 | | SE | .003 |
| | | 8A | .04 | | BETA | 11. | | S102 | 81.30 |
| | | 8E | 0 | | OH | 0 | | AG | .002 |
| | | HC03 | 949.2 | | FE | _29 | | SAR | 6.763 |
| | | В | .595 | | PB | .04 | | NA | 618 |
| | | CD | 0 | | LI | .043 | | SD4 | 1940. |
| | | CA | 392. | | MG | 146.40 | | SURF | 1.35 |
| | | CO3 | 0 | | MM | .05 | | TDS | 3698. |
| | | CL | 94.20 | | HG | 0 | | KJEL | .15 |
| | | CR | .013 | | MD | Ö | | VA | 0 |
| | | CO | 0 | • | NI | Ŏ | | ZN | . 235 |
| | | COND | 5650. | | HO3 | 1.64 | | PH | 8.20 |
| | | | | | | | | | |
| 9 | 10/14/86 | ALK | 860. | | CU | .03 | | P04 | 75. |
| | | AL | 0 | | CN | 0 | | K | 17.10 |
| | | NH3 | .71 | | F | . 06 | | RESD | -11.237 |
| | | AS | .066 | | ALFA | 0 | | SE | 0 |
| | | BA | .04 | | BETA | 0 | | SI02 | 83.40 |
| | | BE | 0 | | OH | 0 | · | AG | 0 |
| | | HCO3 | 1048.2 | | FE | .02 | | SAR | 8.017 |
| | | 8 | .52 | | P8 | 0 | | NA | 695 |
| | | CD | .005 | | LI | .041 | | S04 | 1900. |
| | | CA | 392. | | MG | 100. | | SURF | 1.50 |
| | | CO3 | 0 | | MN | .03 | | TDS | 3744. |
| | | CL | 97.60 | | HG | 0 | | KJEL | 1.10 |
| | | CR | .003 | | MO | 0 | | VA | 0 |
| | | CO | .07 | | NI | 0 | | ZN | .152 |
| | | COND | 5780. | | NO3 | 1.25 | | PH | 7.80 |
| | | | | | | | | | |

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|--------|---|------|--------|--------------|---------|
| 10 | 02/13/87 | ALK | 762. | | CU | .04 | P04 | 69. |
| | | AL | 0 | | CN | 0 | K | 13.77 |
| | | NH3 | . 20 | | F | .03 | RESD | -15.172 |
| | | AS | .15 | | ALFA | 0 | SE | 0 |
| | | BA | .03 | | BETA | 5. | SI02 | 90.61 |
| | | BE | 0 | | НО | 0 | AG | .001 |
| | | HCO3 | 929.6 | | FE | .04 | SAR | 8.124 |
| | | В | .58 | | PB | 0 | NA | 728.30 |
| | | CD | 0 | | LI | .033 | S 0 4 | 2150. |
| | | CA | 420. | | MG | 115. | SURF | 0 |
| | | C03 | 0 | | MN | .03 | TDS | 3960. |
| | | CL | 72.70 | | HG | 0 | KJEL | . 25 |
| | | CR | .002 | | MO | 0 | YA | 0 |
| | | CO | 0 | | NI | 0 | ZN | . 162 |
| | • • | COND | 6100. | • | NO3 | 4.50 | PH | 7.20 |
| | | | | | | | | |
| 11 | 08/27/87 | ALK | 900. | | CU | .03 | P04 | 3.45 |
| ** | V0/1//0/ | AL | 0 | | CN | 0 | . K | 14.64 |
| | | NH3 | .04 | | F | .10 | RESD | -17.372 |
| | | AS | .019 | | Alfa | 0 | SE | .002 |
| | | BA | .03 | | BETA | 7. | \$102 | 60.04 |
| | | 8E | 0 | | OH | 0 | AG | 0 |
| | | HC03 | 1098. | | FE | .05 | SAR | 5.688 |
| | | B . | .50 | | PB | 0 | NA | 550 |
| | | CD | 0 | | LI | .04 | \$04 | 1892. |
| | | CA | 514. | | MG | 118.30 | SURF | 0 |
| | | CO3 | 0 | | MN | .03 | TDS | 3750. |
| | | CL | 97.60 | | HG | 0 | , KJEL | .12 |
| | | CR | .03 | | MO | . 0 | VA | 0 |
| | | CO | 0 | | 'NI | Ŏ | ZN | .13 |
| | | COND | 5750. | | NO3 | .32 | PH | 6.60 |
| | | | | | | | | |
| 12 | 11/11/87 | ALK | 860. | | CU | .06 | P04 | 28.60 |
| | ,,, | AL | 0 | | CN | 0 | K | 15.45 |
| | | NH3 | .24 | | F | . 33 | RESD | -19.416 |
| | | AS | .18 | | ALFA | 0 | SE | 0 |
| | | BA | .04 | | BETA | 7. | \$102 | 74.07 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 1049. | | FE | .21 | SAR | 6.495 |
| | | В | .39 | | PB | .003 | NA | 638.90 |
| | | CD | .012 | | LI | .04 | S04 · | 2130. |
| | | CA | 530.30 | | MG | 123.50 | SURF | 0 |
| | | C03 | 0 | | MN | .06 | TDS | 4050. |
| | | CL | 94.80 | | HG | 0 | KJEL | .30 |
| | | CR | .01 | | MO | Ö | VA | .01 |
| | | CO | 0 | | NI | Ö | ZN | 2.98 |
| | | COND | 6250. | | NO3 | 3.20 | PH | 7.60 |
| | | OUND | OLJV. | | 1100 | 0.20 | FII | 7.00 |

| CASE | MO-DA-YR | | , | • | | | |
|------|----------|-----------|-----------|-----------|-----------|-------------|--------------|
| 13 | 03/30/88 | ALK | 750. | CU | .02 | P04 | 15.60 |
| | | AL | 0 | CN | 0 | K | 15.51 |
| | | NH3 | .23 | F | .11 | RESD | -22.060 |
| | | AS | .13 | ALFA | 0 | SE | 0 |
| | | BA | .04 | BETA | 10. | \$102 | 71.90 |
| | | 38 | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 915. | FE | .04 | SAR | 5.654 |
| | | В | .48 | PB | 0 | NA | 559.60 |
| | 1 | CD | 0 | LI | .04 | \$04 | 2100. |
| | | CA | 636. | MG | 64.80 | SURF | 0 |
| | | C03 | 0 | MM | .03 | TDS | 3924. |
| | • | CŁ | 87.80 | HG | 0 | KJEL | . 30 |
| | | CR | 0 | MO | . 0 | VA | .043 |
| | | CO | .0 | NI | 0 | ZN | .14 |
| | | COND | 6050. | N03 | .57 | PH | 7.00 |
| 14 | 06/13/88 | At V | 904 | CU | | P04 | E4 |
| 14 | VO/13/00 | ALK AL | 890. 0 | CN | 0 | FU4 K | 54. 14.68 |
| | | NH3 | .10 | , CM F | .03 | RESD | -12.112 |
| | | AS | .269 | r ALFA | .03 | SE | 0 |
| | | BA | .04 | BETA | | \$102 | 85.11 |
| | | BE | 0 | OH | 4. . 0 | AG | 0 |
| | | HC03 | 1086. | . FE | .08 | SAR | 7.619 |
| | | 8 | .49 | PB | 0 , | NA NA | 677.50 |
| | | CD | 0 | LI | .04 | S04 | 1850. |
| | | CA | 568. | MG | 19.20 | SURF | |
| | | CO3 | 0 | MN | .03 | TDS | 0 3860. |
| | | CL | 96. | HG | 0 | KJEL | .10 |
| | | CR | . 002 | MO | ŏ | VA | .02 |
| | | CO | . 0 | NI | Ō | ZN | .24 |
| | | COND | 5780. | NO3 | 3,45 | PH | 7.00 |
| | | | | | | | |
| 15 | 10/07/88 | ALK | 618. | CU | 0 | P0 4 | 64. |
| | | AL | 0 | CN | 0 | X | 14.98 |
| | | NH3 | .04 | F | .04 | RESD | -15.012 |
| | | AS | .029 | ALFA | 0 | SE | .003 |
| | | BA | .03 | BETA | 0 | \$102 | 79.22 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 754. | FE | .16 | SAR | 7.769 |
| | | В | .49 | PB | .001 | NA | 660.80 |
| | | CD | 0 | LI | .04 | S04 | 1990. |
| | | CA | 320.80 | MG | 138.25 | SURF | 7920 |
| | | CO3 | 0 | MN | 0 | TDS | 3820. |
| | | CL | 104. | HG | 0 | KJEL | .05 |
| | | CR | .005 | HO | 0 | VA | 0 |
| | | COND | 0 | NI | 0 | ZN | .11 |
| | | COND | 5550. | NO3 | .73 | PH | 7.30 |

| | | | • | - | | | |
|------|----------|------|-----------|------------|--------|----------------|---------|
| CASE | MO-DA-YR | | | | | | |
| 16 | 03/23/89 | ALK | 651. | CU | 0 | P04 | 48. |
| | , 20, 27 | AL | 0 | CN | Ō | K | 13.60 |
| | | NH3 | Ö | F | .29 | RESD | -16.253 |
| | | AS | .18 | ALFA | 0 | SE | .003 |
| | | BA | .03 | BETA | Ö | SI02 | 77.58 |
| | | BE | 0 | OH | ŏ | AG | .002 |
| | | HCO3 | 794. | FE | .06 | SAR | 6.971 |
| | | 8 | .47 | P8 | 0 | NA NA | 613.10 |
| | | CD | 0 | iI | .04 | S04 | 1980. |
| | | CA | | MG | | SURF | 0 |
| | | CD3 | 468. 0 | | 72. | | |
| | | | | MN | 0 | TDS | 3928. |
| | • | CL | 100. | HG | 0 | KJEL | 0 |
| | | CR | .003 | MO | 0 | ۷A | 0 |
| | | CO | 0 | NI | 0 | ZN | .22 |
| | | COND | 6000. | NO3 | 2.70 | PH | 7.00 |
| | | | | | | | |
| 17 | 06/05/89 | ALK | 555. | CU · | 0 | P04 | 16.90 |
| | • • | AL | 0 | CN | 0 | K | 14.90 |
| | | NH3 | .05 | F | .10 | RESD | -25.436 |
| | | AS | .082 | ALFA | 7. | SE, | .003 |
| | | BA | .03 | BETA | 11. | \$102 | 64.52 |
| | | 88 | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 677. | FE | .45 | SAR | 5.724 |
| | | В | . 44 | P8 | 0 % | NA NA | 562.50 |
| | | CD | 0 | LI | .04 | -504 | 2250. |
| | | CA | 536.60 | MG | 118.70 | SURF | .05 |
| | | C03 | 0 | MN | .03 | TDS | 3920. |
| (| | CL | 100. | HG | 0 | KJEL | .10 |
| | | CR | .003 | HO | 0 | VA | 0 |
| | | CO | 0 | | 0 | Z N | .12 |
| | | COND | | NI NO.7 | | | |
| | | CUND | 6030. | NO3 | .49 | PH · | 6.90 |
| | | | | | | | |
| 18 | 09/11/89 | ALK | 675. | CU | 0 | P04 | 37. |
| | | AL | 0 | CN | 0 | · K | 14.12 |
| | | NH3 | .07 | F | .12 | RESD | -23.080 |
| | | AS | .203 | ALFA | 9. | SE | 0 |
| | | BA | .05 | BETA | 10. | \$102 | 79.50 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 824. | FE | .05 | SAR | 6.35 |
| | | В | .44 | PB | 0 | NA | 624.40 |
| • | | CD | .006 | LÏ | .04 | \$04 | 2250. |
| | | · CA | 530.90 | MG | 122.80 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 4065. |
| | | CL | 106. | HG | 0 | KJEL | .10 |
| | | CR | .008 | MO | 0 | VA | . 02 |
| | | CO | 0 | NI | 0 | ZN | 1.74 |
| | | COND | 6200. | NO3 | 1.14 | PH | 7.50 |
| | | | | | | | |

| 19 | CASE | MO-DA-YR | | | • | | | |
|--|------|----------|------|--------|---|--------------|--------------|---------|
| NH3 | 19 | 10/13/89 | ALK | 540. | CU | 0 | P 0 4 | 78. |
| AS 277 | | | AL | . 0 | CN | 0 | K | 14.13 |
| BBA | | | NH3 | 0 | F | 0 | RESD | |
| BB | | | AS | .277 | ALFA | 7. | | |
| HCO3 659. FE | | | BA | . 03 | BETA | 6. | \$102 | 44.57 |
| HCO3 659, FE | | | 8E | 0 | | | | |
| B | | | HCO3 | 659. | FE | .11 | SAR | |
| CD 0 LI 05 S04 2650. CA 549.50 MG 131.80 SURF 0 CO3 0 MN 02 TOS 4550. CL 109. MG 0 KIEL 0 CR 0 MO 0 VA .03 CD 00 NII 0 ZN .18 COHD 6930. MO3 3.75 PH 7.00 20 04/02/90 ALK 661. CU 0 K 12.29 AB 0 CH 0 K 12.29 AB .02 BETA 5. S102 98.03 BE 0 OH 0 AB 0 AB 0 AB 0 AB 150.88 BE 0 OH 0 AB 0 AB 0 AB 150.88 BE 0 OH 0 AB 0 AB 0 CO AB 131.80 SURF 0 CO 0 LI 08 SO4 1880. CA 527.40 MG 131.80 SURF 0 CO3 0 MN 0 TOS 4264. CL 118. HG 0.00 K 12.79 AH3 .47 F 0 RESD 23.31 CO 0 AIR 0 CH 0 K 12.79 AH3 .47 F 0 RESD 25.352 BB 0 OH 0 AB 0 CO AB 0 C | | | В | .57 | | 0 | NA | |
| CA 549.50 NS 131.80 SURF 0 CO3 0 MN .02 TDS 4550. CL 109. H6 0 KJEL 0 CR 0 MO 0 VA .03 CO 0 NI 0 VA .03 CO 0 NI 0 VA .18 COHO 6930. MO3 3.75 PH 7.00 20 04/02/90 ALK 661. CU 0 FP04 25.20 AL 0 CH 0 K 12.29 ANS .255 ALFA 0 SE 0 BA .02 BETA 5. SI02 98.03 BE 0 OH 0 A6 0 HC03 806. FE .07 SAR 7.658 B .59 P8 0 NA 758.80 CD 0 LI .08 S04 1880. CA 527.40 M6 131.80 SURF 0 CO3 0 MN 0 TDS 4264. CL 118. H6 0.00 KJEL 0 CO 0 NI 0 VA .04 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 1 0 VA .03 | | | | 0 | | | | |
| C03 0 MN .02 TDS 4550. CL 109. | | | CA | 549.50 | | | | |
| CL 109. HG 0 KJEL 0 CR 0 MO 0 VA .03 CD 0 NII 0 ZN .18 COND 6930. NO3 3.75 PH 7.00 20 04/02/90 ALK 661. CU 0 PO4 25.20 AL 0 CH 0 K 12.29 AS .255 ALFA 0 SE 0 BA .02 BETA 5. SID2 98.03 BE 0 OH 0 AG 0 HC03 806. FE .07 SAR 7.658 B .S9 PB 0 HA 758.80 CD 0 LI .08 SO4 1880. CA 527.40 HG 131.80 SURF 0 CO 0 HI .10 CR 0 KJEL 0 CL 11B. HG 0.00 KJEL 0 CR 0 HO 0 VA .04 CD 0 NII 0 ZN .11 COND 4378. HO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 CR 0 HO 0 VA .04 CD 0 NII 0 ZN .11 COND 4378. HO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CH 0 K 12.79 AS .336 ALFA 5. SE 0 BR .37 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BR .37 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BR .04 BETA 0 SID2 93.60 BR 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 BR .07 PB 0 HA 707.20 CD .007 LI .10 SO4 SID2 93.60 AG 0 HA 707.20 CD .007 LI .10 SO4 2125. CD .007 L | | | | | | | | |
| CR 0 MO 0 VA .03 CD 0 NI 0 VA .18 CDMD 6930. MO3 3.75 PH 7.00 20 04/02/90 ALK 661. CU 0 P04 25.20 AL 0 CH 0 K 12.29 MH3 .06 F .22 RESD 23.94 AS .255 ALFA 0 SE 0 BA .02 BETA 5. SI02 98.03 BE 0 OH 0 A6 0 HC03 806. FE .07 SAR 7.658 B .59 PB 0 NA 758.80 CD 0 LI .08 S04 1880. CA 527.40 MG 131.80 SURF 0 CO 0 HI 0 VA .04 CL 118. HG 0.00 KJEL 0 CC 0 HI 0 VA .04 CC 0 O HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 HI 0 VA .04 CD 0 COND 4378. NO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 P04 84.50 AL .14 CH 0 K 12.79 AN .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BB .04 BETA 0 SI02 93.60 BB .04 BETA 0 SI02 93.60 BB .057 PB 0 NA 707.20 CD .007 LI .10 SO4 215. CA 516.20 MG 145.80 SURF 0 CO .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO .03 0 MN .02 IDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CD .007 LI .144 | | | CL | 109. | | | | |
| CO | | | | | | | | |
| COND 6930. MO3 3.75 PH 7.00 | | | | 0 | | | | |
| 20 | | | | | | | | |
| AL 0 CH 0 K 12.29 MH3 .06 F .22 RESD 23.94 AS .255 ALFA 0 SE 0 BA .02 BETA 5. SIO2 98.03 BE 0 OH 0 AG 0 HC03 806. FE .07 SAR 7.658 B .59 PB 0 HA 758.80 CD 0 LI .08 SD4 1880. CA 527.40 MG 131.80 SURF 0 CO 0 MN 0 TDS 4264. CL 118. HG 0.00 KJEL 0 CR 0 MO 0 VA .04 CO 0 MI 0 ZH .11 COND 4378. HO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CH 0 K 12.79 MH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SIO2 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 MA 707.20 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO 0 MI 0 O CO CO CO CO CO CO CO CO CO CO CO CO C | | | 555 | 2 | | 31,3 | •" | |
| AL 0 CH 0 K 12.29 MH3 .06 F .22 RESD 23.94 AS .255 ALFA 0 SE 0 BA .02 BETA 5. SIO2 98.03 BE 0 OH 0 AG 0 HC03 806. FE .07 SAR 7.658 B .59 PB 0 HA 758.80 CD 0 LI .08 SD4 1880. CA 527.40 MG 131.80 SURF 0 CO 0 MN 0 TDS 4264. CL 118. HG 0.00 KJEL 0 CR 0 MO 0 VA .04 CO 0 MI 0 ZH .11 COND 4378. HO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CH 0 K 12.79 MH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SIO2 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 MA 707.20 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO 0 MI 0 O CO CO CO CO CO CO CO CO CO CO CO CO C | 20 | 04/02/90 | ALK | 661. | CU | 0 | P04 | 25.20 |
| NH3 | | • • | | | | | | |
| AS .255 ALFA 0 SE 0 BA .02 BETA 5. SI02 98.03 BE 0 OH 0 AG 0 HC03 806. FE .07 SAR 7.658 B .59 PB 0 NA 758.80 CD 0 LI .08 SUFF 0 CO3 0 MM 0 TDS 4264. CL 118. HG 0.00 KJEL 0 CR 0 MD 0 VA .04 CD 0 HI 0 VA .11 COND 4378. HO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CH 0 K 12.79 AN .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 BB .67 PB 0 NA 707.20 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SUFF 0 CO3 0 MM 0 O VA .04 CD .07 LI .10 SO4 2125. CA 516.20 MG 145.80 SUFF 0 CO3 0 MM 0 O VA .04 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SUFF 0 CO3 0 MM .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CD .007 LI .10 SO4 2125. CR 0 MO 0 VA .02 CD .007 LI .110 SO4 2125. CR 0 MO 0 VA .02 CD .007 LI .111 | | | | .06 | | | | |
| BA | | | | | | | | |
| BE 0 | | | | | | | | |
| HC03 | | | | | | | | |
| B | | | | | | | | |
| CD 0 LI .08 S04 1880. CA 527.40 MG 131.80 SURF 0 C03 0 MN 0 TDS 4264. CL 118. HG 0.00 KJEL 0 CR 0 MO 0 VA .04 CD 0 NI 0 TO 7N .11 COND 4378. NO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CN 0 K 12.79 NH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 1 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 1 0 KJEL 1.71 | | | | | | | | |
| CA 527.40 MG 131.80 SURF 0 CO3 0 MN 0 TDS 4264. CL 118. HG 0.00 KJEL 0 CR 0 MO 0 VA .04 CO 0 HI 0 TO TN .11 COND 4378. NO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CN 0 K 12.79 NH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HCO3 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 0 NI 0 VA .02 CO 0 0 NI 0 VA .02 | | | | | | | | |
| CO3 | | | | | | | | |
| CL 118. HG 0.00 KJEL 0 CR 0 HO 0 VA .04 CO 0 NI 0 IN .11 COND 4378. NO3 3.20 PH 7.50 21 07/06/90 ALK 620. CU .05 PO4 84.50 AL .14 CN 0 K 12.79 NH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 SO4 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 VA .02 CO 0 NI 0 VA .02 | | | | | | | | |
| CR 0 | | | | | | | | |
| CO | | | | | | | | |
| COND 4378. NO3 3.20 PH 7.50 | | | | | | | | |
| 21 07/06/90 ALK 620. CU .05 P04 84.50 AL .14 CN 0 K 12.79 HH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 0H 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 M0 0 VA .02 CO 0 NI 0 VA .02 | | | | | | | | |
| AL 14 CN 0 K 12.79 NH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 TN 1.44 | | | OOND | 4070. | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 3.1 0 | <i>e</i> 11 | 7.50 |
| NH3 .47 F 0 RESD -25.352 AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 0H 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | 21 | 07/06/90 | ALK | 620. | cu | .05 | P04 | 84.50 |
| AS .336 ALFA 5. SE 0 BA .04 BETA 0 SI02 93.60 BE 0 OH 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 TN 1.44 | | | AL | .14 | CH | | K | 12.79 |
| BA .04 BETA 0 SI02 93.60 BE 0 0H 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | NH3 | .47 | F | 0 | RESD | -25.352 |
| BE 0 0H 0 AG 0 HC03 756. FE .12 SAR 7.081 B .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | AS | . 336 | ALFA | 5. | SE | 0 |
| HC03 756. FE .12 SAR 7.081 8 .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | - | | BA | .04 | BETA | 0 | \$102 | 93.60 |
| 8 .67 PB 0 NA 707.20 CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | BE | 0 | OH | 0 | A6 | 0 |
| CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 7N 1.44 | | • | HCO3 | 756. | FE | .12 | SAR | 7.081 |
| CD .007 LI .10 S04 2125. CA 516.20 MG 145.80 SURF 0 CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 7N 1.44 | | | 8 | .67 | | | | 707.20 |
| CO3 0 MN .02 TDS 3972. CL 121. HG 0 KJEL 1.71 CR 0 M0 0 VA .02 CO 0 NI 0 ZN 1.44 | | | CD | .007 | | .10 | 504 | 2125. |
| CL 121. HG 0 KJEL 1.71 CR 0 HO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | CA | 516.20 | MG | 145.80 | SURF | 0 |
| CL 121. HG 0 KJEL 1.71 CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | C03 | 0 | MN | .02 | TDS | 3972. |
| CR 0 MO 0 VA .02 CO 0 NI 0 ZN 1.44 | | | CL | 121. | | | KJEL | |
| CO O NI O ZN 1.44 | | | | | | | | |
| • | | | | | | 0 | | |
| | | | | 3330. | | 2.03 | _ | |

| CASE | MO-DA-YR | | | | · | | |
|------|----------|------|-------|------|------|--------|---------|
| 22 | 10/18/90 | ALK | 613. | CU | 0 | P04 | 71. |
| | | AL | .09 | CN | 0 | K | 13.92 |
| | | NH3 | .05 | F | .06 | RESD | -15.186 |
| | | AS | .46 | ALFA | | SE | 0 |
| | | BA | .033 | BETA | | \$102 | 38.07 |
| | | BE | .003 | DH | 0 | AG | 0 |
| | | HCO3 | 748. | FE | .19 | SAR | .76 |
| | | В | .55 | PB | .005 | NA | 665.50 |
| | | CD | 0 | LI | .09 | SD4 | 1974. |
| | | CA | 354. | MG | 119. | SURF | .10 |
| | • | C03 | 0 | MN | 0 | TDS | 4098. |
| | | CL | 110. | HG | 0 | · KJEL | .06 |
| | | CR | 0 . | MO | 0 | VA | .02 |
| | | CO | 0 | NI | 0 | ZN | 2.12 |
| | | COND | 3440. | NO3 | 3.85 | PH | 6.80 |

PEI #3 WELL - CHEMICAL ANALYSES

CR

CO

COND

| AVERAGES | 06/14/ | 84 TO 01/09/91 | | | | |
|----------|--------|----------------|------|--------|------|---------|
| | ALK | 841.3 | cu | .022 | P04 | .08 |
| | AL | .011 | CN | 0 | K | 14.645 |
| | NH3 | .161 | F | .106 | RESD | -10.195 |
| | AS | .186 | ALFA | 1.7 | SE | .002 |
| | BA | .046 | BETA | 5.8 | S102 | 73.738 |
| | 8E | .00 | OH | 0 | AG | .00 |
| | HCO3 | 1026.3 | FE | . 096 | SAR | 6.644 |
| | B | . 494 | PB | .01 | NA | 658.23 |
| | CD | .004 | LI | .048 | \$04 | 2036. |
| | CA | 500.26 | MG | 110.88 | SURF | . 261 |
| | CO3 | 0. | MN | .035 | TDS | 4016. |
| | CL | 96.22 | HG | 0.00 | KJEL | .305 |

ΜO

NI

NO3

.003

.011

2.053

۷A

ZN

PH

.018 .575

7.16

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

.006

.004

5772.

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|-------|---|------|-------|----------|-----------|
| 1 | 06/14/84 | ALK | 154. | | CU | .006 | P04 | .08 |
| | | AL | .006 | | CN | · 0 | K | 9.50 |
| | | NH3 | .17 | | F | .31 | RESD | .08 |
| | • | AS | 0 | - | ALFA | 0 | ` SE | 0 - |
| | | BA | .22 | | BETA | 11. | SI02 | 21. |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 187.8 | | FE | .13 | SAR | 1.70 |
| | | 8 | .11 | | P8 | . 005 | NA | 48 |
| | | CD | 0 | | LI | .03 | \$04 | 40. |
| | | CA | 20. | | MG | 24.30 | SURF | 0 |
| | | CD3 | 0 | | MN | 0 | TDS | 310. |
| | - | CŁ | 53.90 | | HG | 0 | KJEL | .50 |
| | | CR | 0 | | MO | .02 | VA | .06 |
| | | CO | .03 | | NI | .01 | ZN | .044 |
| | | COND | 450. | | NO3 | . 45 | PH | 7.90 |
| 2 | 08/22/84 | ALK | 205. | | CU | .022 | P04 | . 20 |
| - | 00/22/04 | AL | .04 | | CN . | 0 | K | 7.95 |
| | | NH3 | .10 | | F | .17 | RESD | -2.848 |
| | | AS | .008 | | ALFA | 4. | SE | 0 |
| | | BA | .14 | | BETA | 5. | SI02 | 23.21 |
| | | BE | 0 | | OH | | AG | 0 |
| | | HCO3 | 250. | | FE | .10 | SAR | 1.369 |
| | | В | .365 | | PB | .04 | NA NA | 58.70 |
| | | CO | 0 | | LI | .038 | \$04 | 113. |
| | | CA | 70. | | NG | 42. | SURF | |
| | | C03 | 0 | | MN | .01 | TDS | 0 530. |
| | | CL | 109. | | HG | 0 | KJEL | .14 |
| | | CR | 0 | | HO | Ö | VA | 0 |
| | | CO | 0 | | NI | .03 | ZN | .041 |
| | | COND | 800. | | NO3 | 1.64 | PH | 7.40 |
| | | COND | | | 1100 | 1.04 | FII | 7.40 |
| 3 | 04/18/85 | ALK | 306. | | CU | .05 | P04 | .06 |
| | | AL | . 09 | | CN | 0 | K | 8.10 |
| | | NH3 | 2. | • | F | .19 | RESD | -1.510 |
| | | AS | 0 | | ALFA | 0 | SE. | 0 |
| | | ·BA | .06 | | BETA | 9. | \$102 | 21.03 |
| | | BE | 0 | | OH | 0 | · AG | 0 |
| | | HC03 | 373. | | FE | .06 | SAR | 1.404 |
| | | 8 | .37 | | PB | .016 | NA | 63 |
| | | CD | 0 | • | LI | .035 | S04 | 104. |
| | | CA | 96.63 | · | MG | 34.06 | SURF | 0 |
| | | CO3 | 0 | | HH | . 0 | TDS | 575. |
| | | CL | 71. | | HG | 0 | KJEL | 3.60 |
| | | CR | 0 | | MO , | 0 | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .038 |
| | | COND | 880. | | NO3 | 2.40 | PH | 7.30 |

| CASE | MO-DA-YR | | | • | | | |
|------|------------|-------|----------|----------|-------|----------|--------|
| 4 | 06/17/85 | ALK | 327. | cu | 0 | P04 | 1. |
| | | AL | 0 | CN | 0 | K | 8.16 |
| | | NH3 | .08 | F | .19 | RESD | -0.288 |
| | | AS | 0 | ALFA | 25. | SE | 0 |
| | | BA | .15 | BETA | 15. | \$102 | 24.50 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 399. | FE | 0 | SAR | 2.001 |
| | | 8 | . 30 | 98 | .004 | NA | 85 |
| | | CD | 0 | LI | .039 | 504 | 93. |
| | | CA | 78.40 | MG | 35.50 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 595. |
| | | CL | 90.60 | HG | 0 | KJEL | .12 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | Ö | NI | Ō | ZN | Ō |
| | | COND | 910. | NO3 | 1.92 | PH | 7.70 |
| | | 00110 | 710. | | 1.72 | | 7• |
| 5 | 08/19/85 | ALK | 329. | cu | 0 | P04 | . 82 |
| | | AL | 0 | CN | 0 | K | 5.10 |
| | | NH3 | .05 | F | .19 | RESD | -0.225 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | .13 | BETA | 5. | \$102 | 22.25 |
| | | 88 | 0 | OH | . 0 | AG | 0. |
| | | HCO3 | 401. | FE | Q | SAR | 1.604 |
| | | 8 | .19 | PB | .013 | NA | 68 |
| | | CD | 0 | LI | .034 | · S04 | 80. |
| | | CA | 91.20 | MG | 27.36 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | IDS | 524. |
| | | CL | 67.60 | H6 | 0 | KJEL | .10 |
| | | CR | 07.60 | MO | 0 | VA | 0 |
| | | CO | 0 | NI NI | 0 | ZN | .022 |
| | | COND | 810. | NO3 | 1.81 | PH PH | 7.80 |
| | | CUND | 010. | RUS | | | 7.0V |
| 6 | 11/20/85 | ALK | 333. | CU | 0 | PD4 | 14.80 |
| • | 11, 10, 00 | AL | 0 | CN | Ö | K | 7.30 |
| | | NH3 | 0 | F | .20 | RESD | -0.517 |
| | | AS | 0 | ALFA | 0 | SE | . 0 |
| | • | BA | .14 | BETA | 5. | SI02 | 23.50 |
| | | BE | 0 | . OH | 0 | AG | 0 |
| | | HCO3 | 406. | FE | .03 | SAR | 1.24 |
| | | 8 | .26 | PB | .001 | NA NA | 54 |
| | | CD | 0 | LI | .036 | 504 | 61. |
| | | | | MC FI | | SURF | 1.45 |
| | | CA | 96. 0 | | 29. | TDS | 534. |
| | | CO3 | | MN | 0 | KJEL | |
| | | CL | 68.10 | HG | 0 | | .08 |
| , . | | CR | 0 | , MO | 0 | VA | .013 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 830. | NO3 | 1.92 | PH | 7.80 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|--------|-------|--------------|--------|
| 7 | 03/13/86 | ALK | 324. | cu | 0 | P04 | .06 |
| | | AL | 0 | CN | 0 | K | 6.94 |
| | | NH3 | 0 | F | .18 | RESD | -0.876 |
| | | AS | 0 | ALFA | 0 | SE | .002 |
| | - | BA | .14 | , BETA | 4. | SI02 | 23.30 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 395. | FE | 0 | SAR | 1.334 |
| | | В | . 25 | PB | 0 | NA | 58.80 |
| | • | CD | 0 | LI | .036 | 504 | 77. |
| | | CA | 89.20 | MG | 35.30 | SURF | . 0 |
| | | C03 | 0 | MN | 0 | TDS | 536. |
| | | CL | 79.30 | HG | 0 | KJEL | .10 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 880. | NO3 | 1.66 | PH | 7.84 |
| | • | | | | | | |
| 8 | 05/29/86 | ALK | 289. | cu | 0 | P 0 4 | .07 |
| | | AL | 0 | CN | 0 | K | 6.23 |
| | | NH3 | .08 | F | .22 | RESD | -1.170 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | 8A | .12 | 8ETA | 11. | \$102 | 23.34 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | • | HCO3 | 353. | FE | ۵ | SAR | 1.329 |
| | | В | .22 | PB | .006 | NA | 57 |
| | | CD | 0 | LI | .035 | \$04 | 84. |
| | | CA | 90.40 | NG | 29.80 | SURF | 0 |
| | | C03 | 0 | MN | .02 | TDS | 534. |
| | | CL | 77.10 | HG | 0 | KJEL | .10 |
| | | CR | 0 | HO | 0 | VA | 0 |
| | | CO | Ö | NI | 0 | ZN | .009 |
| | • | COND | 820. | NO3 | 1.53 | PH | 7.95 |
| | | | | | | | |
| 9 | 07/17/86 | ALK | 302. | CU | 0 | P04 | .11 |
| | | AL | 0 | CH | 0 | K | 7.69 |
| | | NH3 | .19 | F | .19 | RESD | -0.712 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .12 | BETA | 15. | S102 | 24.56 |
| | | 38 | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 368.4 | FE | 0 | SAR | 1.368 |
| | | 8 | 214 | PB | 0 | NA | 56.50 |
| | | CD | 0 | LI | .035 | \$04 | 71. |
| | | CA | 80.80 | HG | 33.10 | SURF | 0 |
| | | C03 | 0 | MM | 0 | TDS | 520. |
| | | CŁ | 72. | HG | 0 | KJEL | .25 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | • | CO | 0 | NI | . 0 | ZN | .022 |
| | | COND | 790. | ND3 | 1.30 | PH | 7.90 |

| CASE | MO-DA-YR | | | • | | | | |
|------|----------|------|------------|----------|------------|---|-----------|----------|
| 10 | 10/14/86 | ALX | 318. | CU | 0 | | P04 | 1.48 |
| | | AL | 0 | CN | 0 | | K | 8.10 |
| | | NH3 | .41 | F | .17 | | RESD | -0.477 |
| | | AS | 0 | ALF | | | SE | 0 |
| | | BA | .15 | BET | | • | \$102 | 25.40 |
| | | BE | 0 | OH | 0 | | AG | 0 |
| | | HC03 | 388. | FE | .03 | | SAR | 1.195 |
| | | 8 | .17 | PB | 0 | | NA | 50.80 |
| | | CD | 0 | LI | .037 | | \$04 | 38. |
| | | CA | 89.60 | MG | 28.80 | | SURF | 0 |
| | | C03 | 0 | MN | 0 | | TDS | 490. |
| | | CL | 76.90 | HG | Ŏ | | KJEL | .85 |
| | | CR | 0 | MO | 0 | | VA | 0 |
| | | CO | .02 | NI | 0 | | ZN | 0 |
| | | COND | 760. | NO3 | 2.11 | | PH | 8.00 |
| | | COND | 700. | nus | 2.11 | | rn | 5.00 |
| 11 | 02/13/87 | ALK | 324. | CU | 0 | | P04 | .11 |
| | | AL | 0 | CN | 0 | | K | 7.04 |
| | • | NH3 | .08 | F | .22 | | RESD | -0.285 |
| | | AS | 0 | ALFA | a 0 | | SE | 0 |
| | | BA | .14 | BETA | A 0 | | \$102 | 24.90 |
| | | BE | 0 | OH | . 0 | | AG | 0 |
| | | HCO3 | 395.2 | FE | 04م | | SAR | 1.389 |
| | | 8 | .26 | PB | 0 5 | | NA | 56.20 |
| | | CD | 0 | LI | .03 | | S04 | 74. |
| | | CA | 80. | Ме | 26.80 | | SURF | 0 |
| | | C03 | 0 | MN | 0 | | TDS | 469. |
| | | CL | 30. | HG | 0 | | KJEL | .11 |
| | | CR | 0 | MO | 0 | | VA | 0 |
| | | CO | Ŏ | NI | 0 | | ZN | .014 |
| | | COND | 725. | NO3 | 2.50 | | PH | 8.00 |
| 12 | 06/22/87 | ALK | 315. | CU | 0 | | P04 | .21 |
| ** | 00/11/0/ | AL | .05 | CN | 0 | | K K | 6.72 |
| | | NH3 | .04 | F | .20 | | RESD | -0.660 |
| | | AS | 0 | ALFA | | • | SE | 0.500 |
| | | BA | .13 | BETA | | | \$102 | 27.47 |
| | | BE | 0 | OH | , J. 0 | | AG | 0 |
| | | HCO3 | 384. | FE | 0 | | SAR | 1.155 |
| | | 8 | .23 | PB | 0 | | | |
| | | CD | . 23 0 | LI | | | NA CO4 | 49.55 |
| | | CA | | | .02 | | SO4 | 58. A |
| | | C03 | 98.40 0 | MG Mu | 24.90 | | SURF | 400 |
| | | | | MN He | 0 | | TDS | 499. |
| | | CŁ | 64. | HG | 0 | | KJEL | .08 |
| , | | CR | .0 | MO | 0 | | VA | 0 |
| • | | COAD | 775 | NI | .02 | | ZN | .055 |
| | | COND | 775. | NO3 | 1.62 | | PH | 7.80 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|-------|-------|------------|-------|--------------|--------|
| | • | | | | | | |
| 13 | 08/27/87 | ALK | 314. | CU | 0 | P04 | .13 |
| | | AL | 0 | CN | 0 | K | 6.66 |
| | - | NH3 | .06 | · F | .19 | RESD | -0.211 |
| | | AS | . 0 | ALFA | 0 | SE | 0 |
| | | BA | .11 | BETA | 7. | 3102 | 24.86 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 383. | FE | 0 | SAR | 1.328 |
| | | 8 | . 25 | PB | 0 | NA | 55 |
| | | CD | 0 | · LI | .04 | S 0 4 | 55. |
| | • | CA | 79.50 | MG | 30.70 | SURF | 0 |
| | | CO3 · | 0 | MN | 0 | TDS | 488. |
| | | CL | 61.50 | HG | 0 . | KJEL | .10 |
| | | CR | 0 | HO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | 0 |
| | | COND | 750. | NO3 | 2.01 | PH | 7.40 |
| | | | | | 22 | | |
| 14 | 11/11/87 | ALK | 316. | CU | 0 | P04 | .13 |
| | | AL | 0 | CN | 0 | K | 7.35 |
| | | NH3 | . 06 | F | .20 | RESD | -0.640 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .12 | BETA | 0 | \$102 | 27.59 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 386. | FE | 0. | SAR | 1.125 |
| | | В | .16 | PB | 0 ~. | NA | 48.30 |
| | | CD | 0 | LI | .03 | S04 | 59. |
| | | CA | 86.05 | MG | 32.53 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 499. |
| | | CL | 62. | H6 | 0 | KJEL | .10 |
| | | CR | 0 | HO. | 0 | VA | 0 |
| | | CO | . 0 | , NO NI | 0 | ZN | .02 |
| | | COND | 780. | NO3 | 2.80 | 24 PH | 8.05 |
| • | | CUND | 700. | nus | 2.00 | rn | 6.03 |
| 15 | 03/30/88 | ALK | 321. | CU | 0 | P04 | . 0 |
| | | AL | 0 | CN | 0 | K | 6.83 |
| | | NH3 | 0 | F | .19 | RESD | -0.260 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .14 | BETA | 7. | \$102 | 27. |
| | | BE | 0 | OH | 0 | AG | 0 |
| • | | HCO3 | 392. | 'FE | 0 | SAR | 1.14 |
| | | В | .19 | . PB | 0 | NA | 47.96 |
| | | CD | 0 | LI | .02 | S04 | 43. |
| | | CA | 108. | MG | 15.80 | SURF | 0 |
| | | CO3 | 0 | HN | 0 | TDS | 496. |
| | | CL | 61. | HG | 0 | KJEL | 0 |
| | | CR | .0 | . MO | 0 | VA | .025 |
| • | | CO | . 0 | NI | 0 | ZN | 0 |
| | | COND | 750. | NO3 | 1.49 | PH | 7.60 |

| CASE | MO-DA-YR | | | • • | | | |
|------|----------|------|----------------|--------|-------|------------|--------|
| 16 | 06/13/88 | ALK | 302. | CU | 0 | P04 | .10 |
| | | AL | .04 | CN | 0 | K | 6.73 |
| | | NH3 | .10 | F | .17 | RESD | -0.344 |
| | • | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .14 | BETA | 0 | \$102 | 26.69 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 368. | FE | .08 | SAR | 1.145 |
| | | 8 | .16 | P8 | 0 | NA | 47 |
| | • | CD | 0 | LÏ | .03 | S04 | 44. |
| | | CA | 112. | MG | 9.60 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 471. |
| | | CL | 61.50 | HG | 0 | KJEL | .10 |
| | | CR | . 004 | MO | .02 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .01 |
| | | COND | 750. | NO3 | 1.61 | PH | 8.00 |
| | | | | | | | |
| 17 | 03/23/89 | ALK | 298. | CU | 0 | P04 | .13 |
| | | AL | 0 | CN | 0 | K | 6.89 |
| | | NH3 | 0 | F | .21 | RESD | -3.477 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .13 | BETA | 0 | \$102 | 26.71 |
| | | 38 | 0 | НО | . 0 | AG | 0 |
| | | HCO3 | 364. | FE | Q. | SAR | . 854 |
| | | 8 | .14 | P8 | 0 ~ | NA | 42.70 |
| | | CD | 0 | LI | .03 | S04 | 160. |
| | | CA | 128. | HG | 37.20 | SURF | 0 |
| | | C03 | 0 | MH | 0 | TDS | 620. |
| | | CL | 67.50 | HG | 0 | KJEL | 0 |
| | | CR | 0 | MO | Ō | VA | Ö |
| | | CO | 0 | NI | 0 | ZH | .01 |
| | | COND | 950. | ND3 | 1.60 | PH | 7.60 |
| • | | | | | | | |
| 18 | 06/05/89 | ALK | 303. | CU | 0 | P04 | .08 |
| | | AL | 0 | CN | 0 | K | 6.63 |
| | | NH3 | .07 | F | .17 | RESD | -1.022 |
| | | AS . | . 0 | ALFA | 5. | \$E | Ò |
| | | BA | .13 | BETA | 6. | \$102 | 25.06 |
| | | BE | 0 | DH | 0 | AG | 0 |
| | | HCO3 | 370. | FE | .04 | SAR | 1.045 |
| | | В | .11 | PB | 0 | NA | 45.26 |
| | | CD | 0 | LI | .04 | S04 | 53. |
| | | CA | 87.03 | MG · | 33.40 | SURF | 0 |
| | | CO3 | 0 | MN | .02 | TDS | 477. |
| | | CL | 66. | HG | 0 | KJEL | .10 |
| | | CR . | 0 _. | MO | . 0 . | VA | 0 |
| | | CO | 0 | NI | 0 . | ZN | 0 |
| | | COND | 756. | NO3 | 1.73 | PH | 7.70 |

| | | | | | - | | | | |
|------|----------|------------------|---|---|---------------|---------------|---|------------------|-----------------------|
| CASE | MO-DA-YR | | | | | | | | |
| 19 | 09/11/89 | ALK | 291. | | cu | 0 | | P04 | .13 |
| | .,,, | AL | 0 | | CN | 0 | | K | 6.66 |
| | | NH3 | Ŏ | | F | .22 | | RESD | -1.030 |
| | | AS | Ö | | ALFA | 0 | | SE | 0 |
| | | BA | .13 | | BETA | 7. | | SIO2 | 27.43 |
| | | | | | | 0 | | | 27.40 |
| | | BE | 0 | | OH | | | AG | 0 |
| | | HC03 | 355. | | FE | . 05 | | SAR | 1.03 |
| | | 8 | .15 | | P8 | 0 | | NA | 44.01 |
| | | CD | 0 | | LI | .04 | | S04 | 68. |
| | | CA | 83.67 | | MG | 32.62 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | TDS | 477. |
| | | CL | 57. | | HG | 0 | • | KJEL | 0 |
| | | CR | .004 | | MO | 0 | | ٧A | 0 |
| | | CO | 0 | | NI | 0 | | ZN | .14 |
| | | COND | 712. | | NO3 | 1.59 | | PH | 7.80 |
| 20 | 10/13/89 | ALK AL NH3 | 316. 0 .91 | · | CU CN F | 0 0 .17 | | PO4 K Resd | .05 7.08 -0.584 |
| | | AS | 0 . | | ALFA | 3. | | SE | 0 |
| | | BA | .13 | | BETA | 8. | | SI02 | 22.38 |
| | | BE | 0 | | OH | . 0 | | AG | 0 |
| | | HCO3 | 386. | | FE | 0. | | SAR | .996 |
| | | 8 | .16 | | PB | 0 3. | | NA | 42.59 |
| | | CD | 0 | | LI | .03 | • | S04 | 47. |
| | | CA | 84.34 | | MG | 32.89 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | • | TDS | 516. |
| | | CL | 58. | | HG | Ŏ | | KJEL | 1.12 |
| | | | | | | | | | |
| | | CR | 0 | | MO | 0 | • | VA | 0 |
| | | CO | .02 | | NI | 0 . | | ZN . | .01 |
| | • | COND | 715. | | NO3 | 1.37 | | PH | 7.70 |
| 21 | 07/06/90 | ALK | 310. | • | CU | 0 | | P04 | .17 |
| | | AL | 0 | | CN | 0 | | K | 6.65 |
| | | NH3 | . 21 | | F | .19 | | RESD | -0.517 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .12 | | 8ETA | 0 | | SI02 | 25.04 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 378. | | FE | 0 | | SAR | 1.034 |
| | | В | .14 | | PB | 0 | | NA | 43.57 |
| | | CD | 0 | • | LI | .03 | | S04 | 53. |
| | | CA | 81.91 | | MG | 31.96 | | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | | TDS | 588. |
| | | CL | 68. | | HG | 0 | | KJEL | 1.77 |
| | | CŖ | 0 | | MO | . 0 | | VA | .01 |
| | | CO | 0 | • | HI | 0 | | ZN | .03 |
| | | COND | 630. | | NO3 | 1.49 | | PH | 7.57 |
| | | VOID | · • • • • • • • • • • • • • • • • • • • | | 1100 | 4.7/ | | | 7.37 |

| CASE | MO-DA-YR | | | | | | |
|------|----------|------|-------|--------------|------|---------------|--------|
| 22 | 10/18/90 | ALK | 311. | CU | 0 | P04 | .12 |
| | | AL | .18 | CN | 0 | K | 6.19 |
| | | NH3 | .04 | F | .16 | RESD | -0.977 |
| | | AS | .005 | ALF A | | SE | 0 |
| | | BA | .13 | BETA | | SI 0 2 | 30.06 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 379. | FE | .15 | SAR | .60 |
| | | В | .20 | . PB | .002 | NA | 42.53 |
| | | CD | 0 | LI | .05 | S04 | 48. |
| | | CA | 88.09 | MG | 34. | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 548. |
| | | CL | 60. | HG | 0 | KJEL | .02 |
| | | CR | 0 | M0 | 0 | VA | 0 |
| | | CB | 0 | NI | 0 | ZN | .04 |
| | | COND | 637. | NO3 | 1.36 | PH | 7.70 |

PEI #4 WELL - CHENICAL ANALYSES

| AVERAGES | 06/14/8 | 84 TO 01/09/91 | · | | | |
|----------|---------|----------------|------|--------|-------|--------|
| | ALK | 300.4 | CU | .004 | P04 | .911 |
| | AL | .018 | CN | 0 | Х. | 7.114 |
| | NH3 | .211 | F | .195 | RESD | -0.843 |
| | AS | .001 | ALFA | 1.8 | SE | .00 |
| | BA | .133 | BETA | 6. | \$102 | 24.876 |
| | 8E | 0 . | OH | 0 | AG | 0 |
| | HCO3 | 366.4 | FE | .032 | SAR | 1.245 |
| | В | . 209 | PB \ | .004 | NA | 52.93 |
| | CD | 0 | LI | .034 | S04 | 69. |
| | CA | 87.237 | MG | 30.074 | SURF | .066 |
| | CO3 | 0 | MN | .002 | TOS | 513. |
| | CL | 67.36 | HG | 0 | KJEL | . 425 |
| | CR | .00 | MO | .002 | VA | .005 |
| | CO | .003 | NI | .003 | ZN | .023 |
| | COND | 766. | NO3 | 1.723 | PH | 7.75 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|-------|-------|------------|--------|
| 1 | 06/14/84 | ALK | 134. | CU | .016 | P04 | .15 |
| | | AL | .002 | CN | 0 | . K | 2.20 |
| | | NH3 | . 20 | F | .68 | RESD | 1.76 |
| | | AS | 0 | ALFA | 8. | SE | 0 |
| | | BA | .40 | 8ETA | 8. | SI02 | 29. |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 163.4 | FE | .10 | SAR | . 59 |
| | | 8 | .06 | PB | 0 | NA | 20.40 |
| | | CD | .004 | LI | 0 | \$04 | 38. |
| | | CA | 64. | MG | 15.10 | SURF | 0 |
| | i | CD3 | 0 | MN | .01 | TDS | 290. |
| | | CL | 64. | He | 0 | KJEL | .60 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | COND | 0 | NI | .10 | ZN | .043 |
| | | COND | 460. | · NO3 | 1.74 | PH | 7.40 |
| 2 | 08/22/84 | ALK | 125. | CU | .053 | PO4 | 0 |
| • | ,, | AL | .07 | CN | 0 | K | 1.92 |
| | | NH3 | 0 | F | .25 | RESD | -1.590 |
| | | AS | .002 | ALFA | 0 | SE | 0 |
| | | BA | . 05 | BETA | 0 | SI02 | 25.41 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 152. | FE | .08 | SAR | 4.203 |
| | | В | .161 | P8 | .04 | NA | 38 |
| | | CD | 0 | LI | .008 | 504 | 27. |
| | | CA | 60. | MG | 13.20 | SURF | 0 |
| | | C03 | 0 | MN | .01 | TDS | 631. |
| | | CL | 74.90 | HG | 0 | KJEL | .10 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | .02 | ZN | .036 |
| | | COND | 980. | NO3 | .65 | PH | 7.30 |
| 3 | 06/17/85 | ALK | 124. | cu | 0 | P04 | .14 |
| | , | AL | .15 | CN | 0 | K | 2.12 |
| | | NH3 | .08 | F | .36 | RESD | -0.989 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | • | BA | .05 | BETA | 8. | \$102 | 27.02 |
| | | 8E | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 151. | FE | .05 | SAR | .684 |
| | | В | .11 | PB | .004 | NA | 20.70 |
| | | CD | 0 | LI | .008 | \$04 | 20. |
| | | CA | 53.60 | MG | 9.60 | SURF | 0 |
| | | CO3 | 0 | MN | .03 | TDS | 245. |
| | | CL | 51.50 | HG | 0 | KJEL | 0 |
| | | CR | . 0 | MO | .01 | , VA , | 0 |
| | | CO | 0 | NI | 0 | ZN | .048 |
| | | COND | 380. | NO3 | 2.22 | · PH | 7.35 |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|--------------|-------|----------------|-------|--------|
| 4 | 08/19/85 | ALK | 121. | cu | 0 | P04 | .06 |
| | | AL | .28 | . CN | 0 | ĸ | 2.10 |
| | | NH3 | . 05 | F | . 30 | RESD | -0.878 |
| | | AS | .003 | ALFA | 0 | SE | 0 |
| | | BA | .04 | BETA | 0 | \$102 | 25.82 |
| | | BE | .002 | OH | 0 | AG | 0 |
| | | HCO3 | 148. | FE | .19 | SAR | 1.049 |
| | | В | .04 | PB | 0 | NA | 31 |
| | | CD | 0 | LI | .008 | S04 | 34. |
| | | CA | 50.40 | MG | . 9, 60 | SURF | 0 |
| | | C03 | 0 | mn , | 0 | TDS | 284. |
| | | CL | 53.40 | HG | 0 | KJEL | .09 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | · NI | 0 | ZN | 0 |
| | | COND | 434. | NO3 | 1.92 | PH | 7.60 |
| | | | | | | , | |
| 5 | 03/13/86 | ALK | 178. | CU | 0 | P04 | .16 |
| | p | AL | .19 | CN | 0 | K | 2.07 |
| | | NH3 | 0 | F | .25 | RESD | 1.02 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 0 | SIO2 | 29.17 |
| | | ΒE | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 217. | FE | 0 2 | SAR | .814 |
| | | 8 | .15 | PB | 0 ~ | NA | 28.30 |
| | • | CD | 0 | LI | .012 | S04 | 32. |
| | | CA | 70. | MG | 13.20 | SURF | 0 |
| | | CO3 | 0 | MN | .02 | TDS | 322. |
| | | ĊL | 60.70 | HG | 0 | KJEL | .13 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 - | NI | 0 | ZN | .148 |
| | | COND | 495. | MO3 . | 1.97 | PH | 7.63 |
| | | | | | | | |
| 6 | 05/29/86 | ALK | 124. | CU | 0 | P04 | .08 |
| | | AL | 0 | CN | .036 | K | 1.73 |
| | | NH3 | .03 | F | .31 | RESD | -1.030 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | . 04 | BETA | 15. | \$102 | 27.62 |
| | | BE | 0 | OH | . 0 . | AG | 0 |
| | | HCO3 | 151. | FE | .03 | SAR | .661 |
| | | 8 | .09 | PB | 0 | NA | 20.12 |
| | | CD | 0 | LI | .011 | \$04 | 28. |
| | | CA | 54. | MG | 9.80 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 245. |
| | | CL | 47.90 | HG | 0 | KJEL | .05 |
| | | CR | 0 | MO | 0 | VA | .005 |
| | | CD | 0 | NI | .05 | ZN | .196 |
| | | COND | 380. | NO3 | 2.08 | PH | 7.50 |
| | | | - | | - • | ÷ ** | |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|--------|------------------|------------|------------------|
| 7 | 07/17/86 | ALX | 122. | cu | .03 | P04 | .39 |
| | | AL | .26 | CN | 0 | K | 2.40 |
| | | NH3 | .24 | F | .34 | RESD | -0.946 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | . 05 | 8ETA | 0 | \$102 | 29.01 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 148.8 | FE | . 23 | SAR | .679 |
| | | В | .088 | Р8 | .003 | NA | 20.30 |
| | | CD | 0 | LI | .01 | \$04 | 18. |
| | | CA | 51.20 | MG | 10.10 | SURF | 0 |
| | | C03 | 0 | MN | .02 | TDS | 255. |
| | | CL | 51.20 | HG | 0 | KJEL | .29 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .672 |
| | | COND | 380. | NO3 | 1.30 | PH | 7.30 |
| | | | | | | | |
| 8 | 10/14/86 | ALK | 120. | CU | 0 | P04 | .12 |
| | | AL | 0 | CN | 0 | K | 2.30 |
| | | NH3 | . 45 | F | . 28 | RESD | -0.945 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | . 04 | . BETA | 5. | SI02 | 26.60 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 146.4 | FE | .07 | SAR | . 636 |
| | | 8 | .12 | PB | .0 <u>7</u> 0 | NA | 18.90 |
| | | CD | 0 | LI | .006 | S04 | 26. |
| | | CA | 50.40 | MG | 10.10 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 221. |
| • | | CL | 48. | HG | 0 | KJEL | .65 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | .02 | NI | 0 | ZN | .022 |
| | | COND | 350. | NO3 | 2.19 | PH | 7.80 |
| | | | | | | | |
| 9 | 02/13/87 | ALK | 126. | CU | 0 | P04 | .13 |
| | | AL | .14 | CN | 0 | K | 2.06 |
| | | rh3 | . 05 | F | .40 | RESD | -4.888 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .06 | BETA | 0 | \$102 | 27.92 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 153.7 | FE | .13 | SAR | .509 |
| | | 8 | .05 | 98 | 0 | NA | 22.50 |
| | | CD | 0 | LI | 0 | S04 | 24. |
| | | CA | 50.40 | MG | 5.90 | SURF | 0 |
| | | €03 | 0 | MN | .02 | TDS | 415. |
| | | CL | 18.50 | HG | 0 | KJEL | .10 ⁻ |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .086 |
| | | COND | 640. | NO3 | 1.31 | PH | 7.80 |
| | | | | | | | |

| CASE | MO-DA-YR | | | | - | | • | |
|------|----------|------|-------|---|------|-------|---------------------------------------|--------|
| 10 | 06/22/87 | ALK | 127. | | CU | 0 | P04 | .36 |
| 10 | 00/22/01 | AL | .16 | | CN | .021 | , , , , , , , , , , , , , , , , , , , | 2.19 |
| - | | NH3 | .05 | • | F | .29 | RESD | -1.400 |
| | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | .05 | | BETA | 5. | \$102 | 31.67 |
| | | 88 | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 155. | | FE | .15 | SAR | .65 |
| | | 8 | .08 | | PB | 0 | NA | 20.99 |
| | | CD | 0 | | LI | 0 | \$0 4 | 23. |
| | , | CA | 69.60 | | MG | 5.70 | SURF | 0 |
| | | CO3 | 0 | | MN | .02 | TDS | 368. |
| | | CL | 63. | | H6 | 0 | KJEL | 0 |
| | | CR | 03. | • | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | .02 | ZN | .041 |
| | | COND | 420. | | NO3 | 1.91 | PH | 7.60 |
| | | COND | 420. | | NUO | | rn | 7.60 |
| | | | | | | | | |
| 11 | 08/27/87 | ALK | 127. | | CU | 0 | P04 | .13 |
| | | AL | . 27 | | CN | 0 | K | 1.77 |
| | | NH3 | . 07 | i | F | . 30 | RESD | . 876 |
| | | AS | 0 | | ALFA | 12. | \$E | 0 |
| | | 8A | .05 | | BETA | 14. | \$102 | 29.66 |
| | | 8É | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 155. | | FÉ | .19 | SAR | .915 |
| | | В | .09 | | PB | .008 | NA | 27.50 |
| | | CD | 0 | | ίΙ | 0 | S04 | 27. |
| | | CA | 47.95 | | MG | 12.46 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 268. |
| | | CL | 57.50 | | HG | Ō | KJEL | .15 |
| | | CR | 0 | | MO | Ö | VA | 0 |
| | | CO | Ŏ | | NI | 0 | ZH | .06 |
| | | COND | 395. | | NO3 | 2.29 | PH | 7.20 |
| | | | ٠ | | | | | |
| 12 | 11/11/87 | ALK | 127. | | CU | 0 | P04 | .11 |
| | | AL | . 52 | • | CN | 0 | K | 2.57 |
| | | NH3 | .10 | | F | . 36 | RESD | -1.141 |
| | | AS | 0 | | ALFA | 0 | SE | . 0 |
| | | BA | . 05 | | BETA | 0 | -\$102 | 31.75 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HC03 | 155. | 1 | FE | .16 | SAR | . 683 |
| | | В | .04 | | PB | 0 | NA | 21.30 |
| • | | CD | 0 | | ŁI | 0 | S04 | 60. |
| • | | CA | 52.28 | | MG | 13.06 | SURF | 0 |
| | | CO3 | .0 | | MN | .02 | TDS | 268. |
| | | CL | 27. | | HG | 0 | KJEL | .15 |
| | | CR | .004 | | MO | 0 | VA | 0 |
| | | CO | 0 | | NI | .0 | ZN | .11 |
| | | COND | 400. | | NO3 | 2.60 | PH | 7.30 |

| | | | | • | | | |
|------|----------|---|-------|---|------|----------|--------|
| CASE | MO-DA-YR | | | | | | , |
| 13 | 03/30/88 | ALK | 64. | CU | 0 | P04 | .10 |
| | | AL | .56 | CN | 0 | K | 1.93 |
| | | NH3 | . 28 | F | . 34 | RESD | -1.424 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 4. | \$102 | 37.44 |
| | | BE | 0 | ОН | .0 | AG | 0 |
| | | HCO3 | 200. | FE | .26 | SAR | . 687 |
| | | 8 | .06 | PB | 0 | NA | 24.22 |
| | | CD | 0 | LI | 0 | S04 | 55. |
| | | CA | 93.60 | MG | .40 | SURF | 0 |
| | | CO3 | 0 | HN | .03 | TDS | 336. |
| | • | CL | 51.30 | HG | 0 | KJEL | .35 |
| | | CR | 0 | MO | 0 | VA | .022 |
| | | CO | 0 | NI | 0 | ZH | .17 |
| | | COND | 500. | NO3 | 1.79 | PH | 7.40 |
| | | • | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 4.17 | .,, | |
| | • | • | | • | | | |
| 14 | 06/13/88 | ALK | 172. | cu | 0 | P04 | .15 |
| | , , | AL | .21 | CN | 0 | K | 2.19 |
| | | NH3 | .10 | F | .31 | RESD | -1.261 |
| | | AS | . 0 | ALFA | 0 | SE | 0 |
| | | BA | .07 | BETA | 0 | \$102 | 33.68 |
| | | BE | 0 | ОН | . 0 | AG | 0 |
| | | HC03 | 210. | FE | .26 | SAR | .605 |
| | | В | .05 | PB | 0 | NA | 21.33 |
| | | CD | 0 | LI | 0 | S04 | 27. |
| | | CA | 92.80 | MG | .90 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 321. |
| | | CL | 56. | HG | Ŏ | KJEL | .20 |
| | | CR | 0 | MO | 0 | VA | .01 |
| | | CO | 0 | NI | 0 | | .11 |
| | | COND | 480. | NO3 | 1.79 | ZN Ph | 7.80 |
| | | COND | 400. | nus | 1.77 | rn | 7.00 |
| | ٢ | | | | | | |
| 15 | 10/07/88 | ALK | 168. | CU . | 0 . | P04 | .24 |
| | | AL | .16 | CN | 0 _ | X | 1.71 |
| | | NH3 | .15 | F | .48 | RESD | -1.821 |
| | | AS | .006 | ALFA | 4. | SE | 0 |
| | | BA | .09 | BETA | 4. | \$102 | 33.10 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 205. | FE | .168 | SAR | .596 |
| | , | В | .17 | PB | .007 | NA | 22.04 |
| | | CD | .002 | LI | 0 | S04 | 27. |
| | | CA | 91.60 | MG | 7.44 | SURF | 0 |
| | • | C03 | 0 | MN | .11 | TDS | 325. |
| | | CL | 75. | HG | 0 . | KJEL | 0 |
| | | CR | .023 | MÖ | ,0 | . VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .19 |
| | | COND | 500. | · NO3 | 1.27 | PH | 7.90 |

| CASE | MO-DA-YR | | | - | | | |
|------|----------|------|---------------|-----------|-------|----------|--------|
| 16 | 03/23/89 | ALK | 220. | cu | 0 | PD4 | 1.06 |
| | | AL | . 07 | CN | 0 | K | 2.67 |
| | | NH3 | .23 | F | .21 | RESD | -1.269 |
| | | AS | 0 | ALFA | 10. | SE | 0 |
| | | BA | .09 | BETA | 4. | \$102 | 38.11 |
| | | 38 | 0 | OH | 0 | AG | 0 |
| | | HC03 | 268. | FE | .07 | SAR | . 638 |
| | | 8 | .05 | PB | 0 | NA | 24.70 |
| | | CD | 0 | LI | .02 | S04 | 44. |
| | | CA | 105.60 | MG | 4.80 | SURF | 0 |
| | | C03 | 0 | . MN | 0 | TDS | 424. |
| | | CF | 58. | HG | 0 | KJEL | .50 |
| | | CR | .004 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZŇ | . 26 |
| | | COND | . 590. | NO3 | 1.93 | PH | 7.20 |
| 17 | 06/05/89 | ALK | 160. | cu | 0 | P04 | . 25 |
| 17 | 00/03/03 | AL | .08 | CN | 0 | K | 2.50 |
| | | NH3 | .41 | · F | .26 | RESD | -1.303 |
| | | AS | 0 | , Alfa | 7. | SE | 0 |
| | | BA | .07 | BETA | 7. | \$102 | 35.76 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 195. | FE | .09 | SAR | 6.626 |
| | | В | .02 | PB | 0 | NA NA | 22.84 |
| | | CD | 0 | LI | .02 | SD4 | 28. |
| | | CA | 64.10 | MG | 15.83 | SURF | 0 |
| | | CO3 | 0 | NN | 0 | TDS | 295. |
| | | CL | 60. | He | Ŏ | KJEL | .55 |
| | | CR | 0 | MO | Ŏ | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .42 |
| | | COND | 460. | H03 | 2.70 | PH | 7.10 |
| | | | | | | | |
| 18 | 09/11/89 | ALK | 144. | CU | 0 | P04 | .49 |
| | | AL | .09 | CN | 0 | K | 2.34 |
| | | NH3 | .11 | F | .16 | RESD | -1.650 |
| | | AS | .004 | alfa | 0 | SE | 0 |
| | | BA | .07 | BETA | 4. | \$102 | 37.34 |
| | | BE | 0 | НО | 0 | AG | 0 |
| | | HCO3 | 176. | FE | .05 | SAR | .68 |
| | | 8 | .09 | PB | 0 | NA | 23.53 |
| | | CD | 0 | LI | 0 | \$04 | 39. |
| | | CA | 64.53 | NG | 16.08 | SURF | 0 |
| | | C03 | 0 | HN | 0 | TDS | 342. |
| | | CL | 63, | HG | 0 | KJEL | .14 |
| | | CR | .006 | MO | 0 | VA | 0 |
| | • | CO | 0 | NI | 0 | ZN | . 08 |
| | | COND | 489. | NO3 | 2.18 | PH | 7.30 |

| | | | | | • | | | | |
|------|----------|----------|-------|---|---------------|-------|-----|-------------|-------------|
| CASE | MO-DA-YR | | | | | | | | |
| 19 | 10/13/89 | ALK | 179. | ſ | วบ | 0 | | P04 | 1.03 |
| 17 | 10/13/07 | AL | 0 | | CN | 0 | | K | 2.86 |
| | | NH3 | .28 | | F | .16 | | RESD | |
| | | AS | 0 | | | 0 | | | -2.052 0 |
| | | | .09 | | ALFA | | | SE | |
| | | BA Dr | | | BETA | 4. | · · | SI02 | 18.86 |
| | | BE | 0 | |)H | 0 | | AG | 0 |
| | | HCO3 | 218. | | E | 0 | | SAR | .679 |
| | | В | .06 | | PB . | 0 | | NA 224 | 26.20 |
| | | CD | 0 | | .I | 0 | | 504 | 74. |
| | | CA | 79.74 | | 16 | 20.04 | | SURF | 0 |
| | | CO3 | 0 | | 1N | 0 | | TDS | 388. |
| | | CL | 64. | | 16 | 0 | | KJEL | . 35 |
| | | CR | 0 | | 10 | 0 | | VA | 0 |
| | | CO | .02 | | ŧΙ | 0 | - | ZN | .06 |
| | | COND | 585. | H | 103 | 2.16 | | PH | 7.00 |
| | | | | · | | | | | |
| 20 | 07/06/90 | ALK | 188. | | CU | 0 | | P04 | . 69 |
| | | AL | 1.81 | (| CN | 0 | | K | 2.69 |
| | | NH3 | . 43 | F | F | . 42 | | RESD | -1.729 |
| | | AS | . 0 | 4 | ALFA | 0 . | | SE | 0 |
| | | BA | .10 | 8 | BETA | 0 | | SI02 | 5.09 |
| | | 8E | 0 | |)H | . 0 . | - | AG | 0 |
| | | HC03 | 229. | | E | .19 | | SAR | . 693 |
| | | 8 | .04 | | 98 | .011 | | NA | 26.38 |
| | | CD | .003 | | .I | .02 | • | S04 | 36. |
| | | CA | 66.92 | | 16 | 26.09 | | SURF | 0 . |
| | | C03 | 0 | | 111 | .11 | | TDS | 426. |
| | | CL | 56.90 | | 16 | .0004 | | KJEL | .91 |
| | | CR | .03 | | 10 | 0 | | VA | 0 |
| | | CO | 0 | | II | 0 - | | ZN | .63 |
| | | COND | 467. | | 103 | 1.77 | | PH | 6.84 |
| | | | | | | | | | |
| 21 | 10/18/90 | ALK | 190. | C | U | 0 | | P04 | .69 |
| | | AL | . 24 | C | CN | 0 | | X | 2.97 |
| | | NH3 | . 32 | F | : | .75 | | RESD | -0.603 |
| | | AS | .016 | A | ALFA | | | SE | 0 |
| | | BA | .09 | 8 | ETA | | | SI02 | 65.61 |
| | | BE | .001 | 0 |)H | 0 | | AG | 0 |
| , | | HCO3 | 232. | | Ε | .13 | | SAR | .91 |
| | | В | .13 | | 8 | .003 | | NA | 27.72 |
| | | CD | .008 | | .I | .02 | | S04 | 39. |
| | | CA | 62.88 | | 16 | 15.55 | | SURF | .03 |
| | | CO3 | 0 | | 1H | .06 | | IDS | 424. |
| | | CL | 58. | | IG | 0 | | KJEL | .06 |
| | | CR | 0 | | 10 | 0 | • | VA | 0 |
| | | CO | . 0 | | II | 0 | | ZN | 1.06 |
| | | COND | 471. | | 103 | 1.89 | | PH | 7.10 |
| | | | | " | . | : | | | |

PEI #5 WELL - CHEMICAL ANALYSES

| AVERAGES | 06/14/8 | 14 TO | 01/09/91 | | | | |
|----------|---------|-------|----------|------|--------|-------|--------|
| | ALK | 144.8 | | cu | .005 | P04 | 311 |
| | AL | .25 | 1 | CN | .003 | K | 2.252 |
| | NH3 | .17 | 3 | , F | . 343 | RESD | -1.108 |
| | AS | .00 | | ALFA | 2.7 | SE . | 0 |
| | BA | .08 | | BETA | 4.1 | \$102 | 30.745 |
| | BE | .00 | | OH | 0 | AG | 0 |
| | HC03 | 182.3 | | FE | .129 | SAR | 1.152 |
| | В | .08 | 3 | PB | .004 | NA | 24.24 |
| | CD | .00 | | LI | .007 | \$04 | 35. |
| | CA | 66.45 | | MG | 11.188 | SURF | .001 |
| | CO3 | 0 | • | MN | .022 | TDS | 338. |
| | CL | 55.23 | | HG | 0.00 | KJEL | .256 |
| | CR | .00 | | MO | .00 | VA | .002 |
| | CO | .00 | | NI | .009 | ZH | .212 |
| | COND | 488. | • | NO3 | 1.889 | PH | 7.40 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UNHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER

| CASE | MO-DA-YR | | | • | | | | |
|------|----------|-----------|--------|--------------|---------------|---|-------------|--------|
| 1 | 06/14/84 | ALK | 293. | CU | .016 | | P04 | .04 |
| | | AL | .01 | CN | 0 | | K | 5.80 |
| | | NH3 | .24 | F | .40 | | RESD | .09 |
| | | AS | 0 | ALF A | 0 | | SE | 0 |
| | | BA | .35 | BETA | 5. | | S102 | 23.50 |
| | | BΕ | 0 | HO | 0 | | A6 | 0 |
| | | HC03 | 357.4 | FE | .12 | | SAR | 1.21 |
| | | 8 . | . 02 | PB | .044 | | NA | 48.30 |
| | | CD | .007 | ŁI | .03 | | S 04 | 43. |
| | | CA | 74. | MG | 27.50 | | SURF | 0 |
| | | C03 | 0 | HN | .01 | | TDS | 430. |
| | | CL | 48.20 | HG | 0 | | KJEL | .85 |
| | | CR | 0 | MO | 0 | | VA | .05 |
| | | CO | 0 | NI | .04 | | ZN | .108 |
| | , | COND | 680. | NO3 | 1.23 | | PH | 7.35 |
| | | | | | | | | |
| 2 | 08/22/84 | ALK | 340. | CU | .018 | • | P04 | 0 |
| | | AL | .07 | CN | .005 | | K | 6.75 |
| | | NH3 | . 20 | F | .17 | | RESD | -1.440 |
| | | AS | .003 | ALFA | 0 | | SE | 0 |
| | | BA | .16 | BETA | 3. | | \$102 | 23.57 |
| | | BE | 0 | OH | . 0 | | AG | 0 |
| | | HCO3 | 415. | FE | $\mathbf{M1}$ | | SAR | 1.234 |
| | | 8 | .04 | PB | .05 | | NA | 57.60 |
| | | CD | 0 | LI | .037 | • | S04 | 98. |
| | | CA | 100. | MG | 39.60 | | SURF | 0 |
| | | CO3 | o · | MN | 0 | | TDS | 608. |
| | | CL | 69. | HG | 0 | | KJEL | .35 |
| | | CR | 0 | MO | 0 | j | VA | 0 |
| | | CO | 0 | HI | .03 | | ZH | .052 |
| | • | COND | 880. | NO3 | .67 | | PH | 7.30 |
| | | | | | | | | |
| 3 | 04/18/85 | ALK | 341. | CU | .03 | | P04 | .12 |
| | | AL | .06 | CN | 0 | • | K | 7.20 |
| | | NH3 | 0 | F | .19 | | RESD | -1.160 |
| | | AS | 0 | ALFA | 0 | • | SE | 0 |
| | | BA | 0 | BETA | 5. | | SI02 | 21.22 |
| | | BE | 0 | OH | 0. | | AG | 0 |
| | | HCO3 | 416. | FE | .02 | | SAR | 1.285 |
| | | В | .41 | PB | .02 | | NA | 59 |
| | | CD | 0 | LI | .034 | | S04 | 88. |
| | | CA | 100.58 | MG | 36. | | SURF | 0 |
| | | CO3 | 0 | MN | 0 | | TDS | 571. |
| | | CL | 69. | HG | 0 | | KJEL | .35 |
| | | CR | 0 | MO | 0 | | VA | .002 |
| | | CO | 0 | NI | .02 | | ZN | .022 |
| | | COND | 885. | NO3 | 2.50 | | PH | 7.50 |
| | | | | | | | - •• | |

| CASE | MO-DA-YR | | | • | | | |
|------|----------|------|-------|------|------------|-------|--------|
| 4 | 06/17/85 | ALK | 336. | CU | 0 | P04 | .05 |
| | • | AL | 0 - | CN | 0 | K | 7.04 |
| | | NH3 | .05 | F | . 22 | RESD | .248 |
| | | AS | .002 | ALFA | 7. | SE | 0 |
| | | BA | .14 | 8ETA | 16. | \$102 | 23.13 |
| | | BE | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 410. | FE | 0 | SAR | 1.572 |
| | | В | .30 | . PB | .004 | NA | 65 |
| | | CD | 0 | LI | .036 | S04 | 49. |
| | | CA | 77.20 | MG | 31.90 | SURF | 0 |
| | | CO3 | 0 | · MN | 0 | TDS | 510. |
| | | CL | 68.20 | HG | 0 | KJEL | .10 |
| | | CR | 0 | MO | 0 | VA | .003 |
| | | CO | Ò | NI | 0 | ZN | . 034 |
| | | COND | 790. | NO3 | 2.27 | PH | 7.65 |
| | · | | | | 5 . | | |
| 5 | 08/19/85 | ALK | 327. | CU | 0 | PO4 | .08 |
| | • • | AL | 0 | CN | 0 | K | 6.90 |
| | • | HH3 | .05 | F | .20 | RESD | -0.019 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .13 | BETA | 8. | \$102 | 24.59 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 399. | FE | .05 | SAR | 1.393 |
| | | В | .24 | PB | 0 % | NA | 58 |
| | | CD | 0 | LI | . 034 | ` S04 | 47. |
| | | CA | 89.60 | MG | 25.44 | SURF | 0 |
| | | C03 | 0 | нн | 0 | TDS | 488. |
| | | CL | 62.10 | HG | 0 | KJEL | .07 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | Ō | NI | 0 | ZN | .016 |
| | | COND | 750. | NO3 | 1.96 | PH | 7.75 |
| | | | | | | | |
| 6 | 11/20/85 | ALK | 331. | cu | 0 | P04 | .06 |
| | | AL | .02 | CN | 0 | X | 7.09 |
| | • | NH3 | 0 | F | .21 | RESD | -0.489 |
| | | AS | 0 | ALFA | _0 _ | SE | 0 |
| | | BA | .14 | BETA | 5. | \$102 | 24.30 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HC03 | 404. | FE | .03 | SAR | 1.109 |
| | | В | . 24 | PB | .008 | . NA | 48.10 |
| | | CD | 0 | LI | .036 | \$04 | 45. |
| | | CA | 90. | MG | 31.90 | SURF | 0 |
| | | CO3 | 0 | . MN | 0 1 | TDS | 518. |
| | | CL | 61.60 | HG | 0 | KJEŁ | .08 |
| | • | CR | .002 | MO | 0 | . VA | .014 |
| | | CO | 0 | NI | . 0 | ZN | 0 |
| | | COND | 775. | NO3 | 2.13 | PH | 7.85 |

| | | | | • | | | |
|------|----------|-------|-------|-------------|-------|-------------|--------|
| CASE | MO-DA-YR | | | • | | | |
| 7 | 03/13/86 | ALK | 320. | CU | .02 | P04 | .10 |
| | , , | AL | .12 | CH | 0 | K | 6.74 |
| | | NH3 | .07 | F | .19 | RESD | -0.484 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | • | BA | .15 | BETA | 0 | 5102 | 24.28 |
| | | BE | 0 | OH | 0 . | AG | 0 |
| | | HCO3 | 390. | FE . | .17 | SAR | 1.262 |
| | | В | .27 | PB | .007 | NA NA | 53.82 |
| | | CD | 0 | ĹĬ | .038 | S04 | 47. |
| | | CA | 87.60 | MG | 30.50 | SURF | 0 |
| | | CO3 | 0 | | | | 498. |
| | | | | MM | 0 | IDS | |
| | | CL | 63.50 | HG | 0 | KJEL | .10 |
| | | CR | .01 | H0 | 0 | VA Til | 0 |
| | | CO | 0 | NI | 0 | ZN | .049 |
| | | COND | 851. | NO3 | 2.09 | PH | 7.82 |
| | | | | | | | |
| 8 | 05/29/86 | ALK | 285. | CU | 0 | P04 | .04 |
| - | | AL | 0 | CN | 0 | K | 5.33 |
| | | NH3 | .08 | F | .22 | RESD | -0.420 |
| | | AS | 0 | ALFA | 0 | \$E | 0 |
| | | BA | .12 | . BETA | 6. | \$102 | 22.51 |
| | | BE | 0 | OH | . 0 | AG | 0 |
| | | HCO3 | 348. | FE | 0. | SAR | 1.019 |
| • | | В | .19 | PB | .012 | NA · | 41.04 |
| • | | CÐ | 0 | LI | .039 | S04 | 51. |
| | | CA | 80.40 | MG | 25.70 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 430. |
| | | CL | 49.30 | HG | 0 | KJEL | .12 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI | 0 | ZN | .021 |
| | | COND | 799. | NO3 | 1.09 | PH | 7.90 |
| | | | | | • | | |
| 9 | 07/17/86 | ALK | 318. | CU | 0 | P0 4 | .08 |
| | | AL | 0 | CN | 0 | K | 7.26 |
| | | NH3 | .09 | F | .20 | RESD | -0.595 |
| | | AS | o ´ | ALFA | 9. | SE | 0 |
| | | BA | .12 | BETA | 10. | \$102 | 25.01 |
| | | BE | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 388. | FE | 0 | SAR | 1.166 |
| | | 8 | .231 | P8 | 0 | NA | 49.99 |
| | | CD | 0 | LI | .036 | \$04 | 34. |
| | | CA | 87.20 | HG | 31.70 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 495. |
| | | CL | 76. | HG | Ö | KJEL | .14 |
| | | CR | 0 | MO | 0 | VA | 0 |
| • | | CO | 0 | NI | Ŏ | ZN | .054 |
| | | COND | 760. | N03 | 1.55 | PH | 8.00 |
| | | VVIID | | noo | 1.33 | CH | U. VV |

| | | | | | • | | | | |
|------|----------|-----------|-------------|---|-----------|-----------|---|-----------|-------------|
| CASE | MD-DA-YR | | | | - | | | | |
| 10 | 10/14/86 | ALK | 324. | | CU | 0 | | P04 | .10 |
| | ,, | AL | 0 | | CN | Ö | | ĸ | 7.70 |
| | | · NH3 | .44 | | F | .19 | | RESD | -0.322 |
| | | AS | 0 | | ALFA | 0 | | SE | 0 |
| | | BA | .14 | | BETA | 7. | | \$102 | 24.70 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | HC03 | 395.3 | | FE | Ö | | SAR | 1.148 |
| | | В | .28 | | PB | 0 | | NA | 48.70 |
| | | CD | 0 | | LI | .033 | | \$04 | 35. |
| | | CA | 91.20 | | MG | 27.40 | | SURF | 0 |
| | | C03 | 0 | | MH | 0 | | TDS | 482. |
| | | CL | 70.20 | | HG | 0 | | KJEL | .85 |
| • | | CR | .003 | | MO | Ö | | VA | 0 |
| | | CO | | ; | HI | Ö | | ZN | .019 |
| | | COND | 750. | | NO3 | 2.21 | | PH | 8.20 |
| | | V42 | 7501 | | 1100 | | | • •• | |
| 11 | 02/13/87 | ALK | 336. | | CU . | 0 | | P04 | .13 |
| 11 | VL/13/07 | AL | 0 | | CN | 0 | | K | 6.55 |
| | | NH3 | .11 | | F . | .23 | | | |
| | | AS | 0 | | | | | RESD | -0.135 0 |
| | | | | | ALFA | 0 | | SE | |
| | | BA | .14 | | BETA | 5. | | SI02 | 24.50 |
| | | 8E | 0 | | OH | . 0 | | AG | 0 |
| | | HC03 | 409.9 | | FE | .02 | | SAR | 1.558 |
| | | В | .24 | | PB | 0 | | NA . | 65 |
| | | CD | 0 | | LI | .024 | | S04 | 57. |
| | | CA | 72. | | MG | 36.40 | | SURF | 0 |
| | | C03 | 0 | | MM | 0 | | TDS | 503. |
| | | CL | 65.90 | | HG | 0 | · | KJEL | .15 |
| | | CR | 0 | | MO | 0 | | VA | 0 |
| | | CO | 0 | | NI | 0 | | - ZN | .029 |
| | | COND | 775. | | NO3 | 1.61 | | PH | 8.20 |
| 12 | 06/22/87 | ALX | 312. | | CU | 0 | | P04 | .11 |
| •• | AALTELOI | AL | .03 | | CN | . 023 | | K | 6.37 |
| | | NH3 | .04 | | F | .20 | | RESD | -0.641 |
| | | AS | .002 | | r Alfa | 0 | | SE | 0.041 |
| | | BA | .13 | | BETA | 5. | | SI02 ' | 27.55 |
| | | BE | 0 | | OH | 0 | | AG | 0 |
| | | | | | | | | | 1.077 |
| | | HCO3 B | 381. .22 | | FE PB | . 04 0 | | SAR | |
| | | | 0 | | | | | NA SD4 | 45.98 |
| | | CD | - | | £I. | .02 | | SD4 | 46. |
| | | CA | 112. | | MG | 15.80 | | SURF | 0. |
| | | C03 | 0 | | HN | 0 | | TDS | 488. |
| | | CL | 62. | | HS | 0 | | KJEL | .06 |
| | | CR | 0 | | MO | 0 | | . VA | 0 |
| | | CO | 0 | | NI | .04 | | ZN | .07 |
| | | COND | 750. | | H03 | - 1.77 | | PH | 7.80 |

| CASE | MO-DA-YR | | | | - | | | |
|------|----------|------|--------|---|------|----------|-------|--------|
| | | | | | | | | |
| 13 | 08/27/87 | ALK | 311. | | CU | 0. | P04 | .09 |
| | | AL | 0 | | CN | 0 | K | 6.26 |
| | | NH3 | .05 | | F | .18 | RESD | .152 |
| - | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | .11 | | BETA | 13. | \$102 | 25.65 |
| | | 38 | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 379. | | FE | .09 | SAR | 1.201 |
| | | В | .24 | | P8 | 0 | NA | 52 |
| | | CD | 0 | | ĻΙ | .04 | \$04 | 48. |
| | | CA | 77.79 | | MG | 30.23 | SURF | 0 |
| | | CO3 | 0 | | MN | 0 | TDS | 470. |
| | | CL | 62. | | HG | 0 | KJEL | .10 |
| | | CR | . 0 | | MO | 0 | · VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .02 |
| | | COND | 750. | | NO3 | 2.13 | PH | 7.20 |
| | | | | | | | | |
| 14 | 11/11/87 | ALK | 316. | • | CU | 0 | P04 | .12 |
| | ,, | AL | 0 | | CN | 0 | K | 7.49 |
| | | NH3 | .10 | | F | .18 | RESD | -0.786 |
| | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | .12 | | BETA | 8. | \$102 | 27.41 |
| | | 8E | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 386. | | FE | | SAR | 1.062 |
| | | 8 | .16 | | PB | .02 0 | NA | 46.11 |
| | | CD | 0 | | LI | .03 | S04 | 56. |
| | | CA | 86.32 | | MG | 34.15 | SURF | 0 |
| | | CO3 | 00.32 | | MN | 0 | . TDS | 480. |
| | | CL | 58.50 | | HG | 0 | KJEL | 12 |
| | | CR | 0 | | MO | Ŏ | VA | 0 |
| | | | .007 | | NI | 0 | ZN | .03 |
| | | COND | | | | | PH | 7.80 |
| | | COND | 750. | | NO3 | 2.20 | rn | 7.00 |
| 15 | 03/30/88 | ALK | 313. | | CU | 0 | PO4 | .05 |
| | ,, | AL | 0 | | CN | 0 | K | 6.72 |
| | | NH3 | .09 | | F | .18 | RESD | -0.864 |
| | | AS | 0 | | ALFA | 0 | SE | 0 |
| | | BA | .14 | | 8ETA | 7. | \$102 | 26.38 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 382. | | FE | 0 | SAR | 1.10 |
| | | 8 | .18 | | PB | 0 | NA | 47.74 |
| | | CD | 0 | | LĪ | .02 | S04 | 60. |
| | | CA | 121.60 | | MĠ | 12.90 | SURF | 0 |
| | • | CO3 | 0 | | MN | 0 | TDS | 510. |
| | | CL | 61. | | HG | 0 | KJEL | .10 |
| | | CR | .005 | | MO | Ô | VA | . 025 |
| | - • | CO | 0 | | NI | 0 | ZN | .03 |
| | | COND | 780. | | NO3 | 1.72 | PH | 7.60 |
| | | COND | /OV. | | 1103 | 1.14 | rn | 7.00 |

| CASE | MO-DA-YR | | | | • | | | |
|------|----------|-----------|---------------|---|----------|-------|----------------------|--------|
| 16 | 06/13/88 | At W | 310. | | | ۸ | P04 | 11 |
| 10 | 00/13/00 | ALK AL | .02 | | CU CN | 0 | 70 4 K | .11 |
| | | NH3 | ۷۸ | | F | .18 | RESD | -0.747 |
| | | AS | .60 , | | ALFA | 0 | SE SE | 0.747 |
| | | BA | .14 | | BETA | 0 | SI02 | 26.34 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 37 8 . | • | FE | 0 | SAR | 1.007 |
| | | В | .14 | | PB | 0 | NA NA | 43.15 |
| | | CD | 0 | | LI | .04 | 504 | 48. |
| | | CA | 139.20 | | MG | 25. | SURF | 0 |
| | | C03 | 0 | | MN | 0 | IDS | 499. |
| | | CL | 60. | | HG | 0 | KJEL | .08 |
| | | CR | 0 | | MO | Ö | VA | .01 |
| | | CO | 0 | | NI | 0 - | ZN | .01 |
| | | COND | 765. | | H03 | 1.71 | PH | 8.00 |
| | | COND | 705. | | NUS | 1.71 | rn | 0.00 |
| 17 | 10/07/88 | ALK | 315. | | CU | 0 | P04 | .12 |
| • . | 10/01/00 | AL | 0 | | CN | Ö | K | 6.73 |
| • | | NH3 | .09 | | F | . 23 | RESD | -0.809 |
| | | AS | 0 | | Alfa | 0 | SE | 0 |
| | | BA | .14 | | BETA | Ö | \$102 | 25.34 |
| | | BE | 0 | | OH | . 0 | AG | 0 |
| | | HCO3 | 384. | | FE | .07 | SAR | .937 |
| | | В | .14 | | PB | 0 | . NA | 40.59 |
| | | CD | 0 | | LI | .04 | S04 | 46. |
| | | CA | 72.80 | | MG | 42.24 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 459. |
| | • | CL | 57. | | HG | Ö | KJEL | .10 |
| | | CR | 0 | | MO | 0. | VA | 0 |
| | | CO | 0 | | NI | 0 | ZN | .06 |
| | | COND | 720. | | NO3 | 1.10 | PH | 8.20 |
| | | •=• | | | | | | |
| 18 | 03/23/89 | ALK | 304. | | cu | 0 | PD4 | .20 |
| | | AL | 0 | | CN | 0 | K | 6.53 |
| | | NH3 | 0 | | F | .22 | RESD | -3.067 |
| | | AS | 0 | | ALFA | 12. | SE | 0 |
| | | BA | .14 | | BETA | 5. | \$102 | 25.62 |
| | | BE | 0 | | OH | 0 | AG | 0 |
| | | HCO3 | 371. | | FE | 0 | SAR | .896 |
| | | 8 | .13 | | PB · | 0 | NA | 44.04 |
| | | CD | 0 | | LI | .04 | S04 | 150. |
| | | CA | 128. | | MG | 33.60 | SURF | 0 |
| | | C03 | 0 | | MN | 0 | TDS | 620. |
| | | CL | 67.50 | | HG | 0 | KJEL | 0 |
| | | CR | .003 | | MO | . 0 | VA | 0 - |
| | • | CO | 0 | • | NI | 0 | ZN | .03 |
| | | COND | 950. | | NO3 | 1.84 | PH | 7.70 |
| | | - | - | | | | | |

| CARE | MO-DA-VO | | | - | | | |
|------|----------|------|-----------|----------|-------|---------------|--------|
| CASE | MO-DA-YR | | | | | | |
| 19 | 06/05/89 | ALK | 244. | CU | 0 | P04 | .10 |
| | | AL | 0 | CN | 0 | · K | 6.69 |
| | | NH3 | .04 | F | .18 | RESD | -2,115 |
| | | AS | 0 | ALFA | 6. | SE | 0 |
| | | BA | .13 | BETA | 9. | SI 0 2 | 25.02 |
| | | 8E | 0 | OK | 0 | AG | 0 |
| | | HCO3 | 297. | FE | .04 | SAR | 1.029 |
| | | В | .11 | PB | 0 | NA | 44.27 |
| | | CD | 0 | LI | .04 | S04 | 109. |
| | | CA | 85.41 | MG | 33.24 | SURF | 0 |
| | | CO3 | 0 | MN | .02 | TDS | 495. |
| | | CL | 64. | HG | . 0 . | KJEL | .08 |
| | | CR | 0 | MO | 0 | VA | 0 |
| | | CO | 0 | NI NI | Ö | ZN | ŏ |
| | | COND | 765. | H03 | 1.95 | PH | 7.30 |
| | | COND | 103. | nus | 1.73 | rn | 7.30 |
| | | | | | | | |
| 20 | 09/11/89 | ALK | 295. | CU | 0 | P04 | .13 |
| 20 | V7/11/07 | AL | 293. 0 | CN | 0 | , P04 K | 6.65 |
| | | | | F | | RESD | -0.840 |
| | | NH3 | 0 0 | | .18 | | 0.640 |
| | | AS | | . ALFA | 0 | SE | |
| | | BA | .13 | BETA | 5. | \$102 | 26.81 |
| | | BE | 0 | OH | . 0 | A6 | 0 |
| | | HCO3 | 360. | FE | 0. | SAR | 1.03 |
| | • | B | .17 | PB | 0 | NA | 43.37 |
| | | CD | . 0 | LI | .04 | \$04 | 58. |
| | | CA | 82.88 | MG | 31.73 | SURF | 0 |
| | | C03 | 0 | MN | 0 | TDS | 467. |
| | | CL | 56. | HG | 0 | KJEĿ | 0 |
| | | CR | 0 | MO | 0 | . VA | 0 |
| | | CO | 0 | NI | 0 | · ZN | .01 |
| | | COND | 714. | H03 | 1.54 | PH | 7.80 |
| | | | | | | | |
| 21 | 10/13/89 | ALK | 312. | CU | 0 | P04 | .15 |
| | | AL | 0 | CH | 0 | K | 7. |
| | | NH3 | .10 | F | .23 | RESD | -0.810 |
| | | AS | 0 | ALFA | 4. | SE | 0 |
| | | BA | .13 | BETA | 12. | \$102 | 22.54 |
| | | 8E | 0 | OH | 0 | AG | 0 |
| | | HCO3 | 381. | FE | .06 | SAR | .982 |
| | | 8 | .14 | PB | 0 | NA | 42.42 |
| | • | CD | 0 | LI | .04 | S04 | 50. |
| | | CA | 85.44 | MG | 33.98 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 540. |
| | | CL | 57. | HG | 0 | KJEL | .25 |
| | | CR | 0 | MO | 0 | VA | .01 |
| | | CO | .02 | IH | Ö | ZN | .05 |
| | | COND | 804. | NO3 | 1.56 | PH | 7.70 |
| | | | | 1199 | | * * * * . | |

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|------|----------|--------------|-------|------|-------|------------|--------|
| CASE | MO-DA-YR | | | | | | |
| 22 | 07/06/90 | ALK | 313. | CU | 0 | PO4 | .23 |
| | | AL | 0 | CN · | 0 | K | 6.27 |
| | | NH3 | .19 | F | .20 | RESD | -0.367 |
| | | AS | 0 | ALFA | 0 | SE | 0 |
| | | BA | .12 | BETA | 4. | SIO2 | 25.19 |
| | | 38 | 0 | ОН | 0 | AG | 0 |
| | | HCO3 | 382. | FE | .05 | SAR | 1.056 |
| | | В | .15 | PB | 0 | NA | 44.21 |
| | | CD | 0 | LI | .04 | S04 | 58. |
| | | CA | 82.74 | MG | 30.43 | SURF | 0 |
| | | CO3 | 0 | MN | 0 | TDS | 550. |
| | | CL | 68.50 | HG | 0 | KJEL | .61 |
| | | CR | 0 | MO | 0 | VA | 0 - |
| | | CO | 0 | NI | 0 | ZN | .06 |
| | | COND | 653. | NO3 | 1.63 | PH | 7.54 |
| | | | | | | | |
| 23 | 10/18/90 | ALK | 306. | CU | .03 | P04 | . 26 |
| | | AL | .09 | CN | 0 | · K | 7.59 |
| | | NH3 | .08 | F | .22 | RESD | . 12 |
| | | AS | .004 | ALFA | | SE | 0 |
| | | BA | .133 | BETA | | \$102 | 67.30 |
| | | BE | .002 | OH | . 0 | AG | 0 |
| | | HCO3 | 375. | FE | .08 | SAR | .77 |
| | | В | .15 | P8 | .007 | NA | 39.44 |
| | | CD | 0 | LI | .04 | S04 | 41. |
| | | CA | 73.14 | MG | 28.34 | SURF | 0 |
| | | C O 3 | 0 | MN | . 0 | TDS | 520. |
| | | CL | 58.50 | HG | 0 | KJEL | .04 |
| | | CR | 0 | MO | 0 | ٧A | 0 |
| | : | CO | 0 | NI | 0 | ZN | . 25 |
| | | COND | 643. | NO3 | 1.56 | PH | 7.70 |
| | | | | | | | |

PEI #6 WELL - CHEMICAL ANALYSES

| AVERAGES | 06/14/8 | 34 TO 01/09/91 | | | | |
|----------|---------|----------------|------|--------|-------|--------|
| | ALK | 313.1 | CU | .005 | P04 | .107 |
| | AL | .018 | CH | .001 | K | 6.751 |
| | NH3 | .118 | F | .209 | RESD | -0.674 |
| | AS | .00 | ALFA | 1.7 | SE | 0 |
| | BA | .137 | BETA | 6.3 | \$102 | 26.629 |
| | BE . | .00 | OH | 0 | AG | 0 |
| | HC03 | 382.1 | FE | .042 | SAR | 1.135 |
| | В | .191 | PB | .007 | NA | 49.04 |
| | CD . | .00 | LI | .035 | S04 | 59. |
| | CA | 91.178 | MG | 30.247 | SURF | 0 |
| | C03 | 0 | MN | .001 | TDS | 506. |
| | CL | 62.39 | HG | 0 | KJEL | .204 |
| | CR | .001 | МO | 0 | VA | .005 |
| | CO | .001 | NI | .006 | ZN | .045 |
| | COND | 771. | NO3 | 1.74 | PH | 7.73 |

ALFA AND BETA IN PICOCURIES PER LITER

CONDUCTIVITY IN UMHOS PER CENTIMETER

RESD AND SAR ARE CALCULATED

REMAINDER IN MILLIGRAMS PER LITER